CITY OF HAVERHILL

CITY COUNCIL AGENDA

Tuesday, August 24, 2021 at 7:00 PM

Theodore A. Pelosi, Jr. Council Chambers, 4 Summer st, Room 202 In-Person/Remote Meeting

This meeting/hearing of Haverhill City Council will be held in-person at the location provided on this notice. Members of the public are welcome to attend this in-person meeting. Please note that while an option for remote attendance and/or participation is being provided as a courtesy to the public, the meeting/hearing will not be suspended or terminated if technological problems interrupt the virtual broadcast, unless otherwise required by law. Members of the public with particular interest in any specific item on this agenda should make plans for in-person vs. virtual attendance accordingly.

- 1. OPENING PRAYER
- 2. PLEDGE OF ALLEGIANCE
- 3. APPROVAL OF MINUTES OF PRIOR MEETING
- 4. ASSIGNMENT OF THE MINUTES REVIEW FOR THE NEXT MEETING
- 5. COMMUNICATIONS FROM THE MAYOR:
- 6. COMMUNICATIONS FROM COUNCILLORS TO INTRODUCE AN INDIVIDUAL(S) TO ADDRESS THE COUNCIL:
- 7. Public Participation- Requests under Council Rule 28
- 8. COMMUNICATIONS AND REPORTS FROM CITY OFFICERS AND EMPLOYEES:
 - 8.1.Communication from Linda Koutoulas, City Clerk, announcing early voting before our preliminary election being held on September 14, 2021; to be held in person in City Hall basement (former RMV location) from Tuesday, September 7th through Friday, September 10th, from 8-4 and on Thursday, September 9th, from 8-8pm. Also recommends early voting to be held on Sunday, September 5th from 2:30-8 pm at *Somebody Cares*, located at 358 Washington st
 - 8.2. Abatement report from Christine Webb, Assessor for the month of July 2021
- 9. UTILITY HEARING(S) AND RELATED ORDER(S):
- 10. HEARINGS AND RELATED ORDERS:
 - 10.1. <u>Document 32-C</u>: Application from Attorney Robert Harb for client Solar Smart LLC for CCSP-21-8 Solar Energy System Special Permit for Large Scale Ground Mounted Solar Energy System at 139 Amesbury Line rd
 - 10.2. <u>Document 32-D</u>: Application from Attorney Robert Harb for client Solar Smart LLC for CCSP-21-9 Solar Energy System Special Permit for Large Scale Ground Mounted Solar Energy System at 139 Amesbury Line rd; in Water Supply Protection Overlay District (WSPOD)
 Comments are included

Hearings postponed from June 15 2021

11. APPOINTMENTS:

- 11.1. Confirming Appointments:
- 11.2. Non-Confirming Appointments:
 - 11.2.1. Mayor's Task Force on Public Health:

Kevin McCarthy of Groundwork Lawrence

Tony Slabacheski, Holy Family Hospital, Haverhill Campus, Administrator in Charge <u>To Expire December 31 2021</u>

11.3. **Resignations:**

CITY OF HAVERHILL

CITY COUNCIL AGENDA

Tuesday, August 24, 2021 at 7:00 PM

Theodore A. Pelosi, Jr. Council Chambers, 4 Summer st, Room 202 In-Person/Remote Meeting

12. PETITIONS:

12.5.19.

12.5.20.

12.1.	Applicat	tions Handicap Parking Sign	
12.2.	Amusen	nent/Event Applications:	
12.3.	Tag Day	7	
		V Liquor License:	
		License Renewals:	
	12.5.1. I	Hawker Peddlers License 2021 - Fixed location	
		Coin-Op License Renewals 2021	
		Orainlayer License for 2021 - with City Engineer app	roval
		Christmas Tree Vendor	
	12.5.5.	Taxi Driver Licenses for 2021	
	1	2.5.5.1. Michael Brown, Manchester, NH – <i>new</i>	Denied by Police
	12.5.6.	Taxi License/ Limo/Livery	
	12.5.7.	Junk Dealer License	
	12.5.8.	Pool Tables	
	12.5.9.	Sunday Pool	
	12.5.10.	Bowling	
	12.5.11.	Sunday Bowling	
	12.5.12.	Buy & Sell Second Hand Articles	
	12.5.13.	Buy & Sell Second Hand Clothing	
	12.5.14.	Pawnbroker license	
	12.5.15.	Fortune Teller	
	12.5.16.	Buy & Sell Old Gold	
	12.5.17.	Roller Skating Rink	
	12.5.18.	Sunday Skating	

Exterior Vending Machines – 2021 renewals

Limousine/Livery License/Chair Cars

CITY OF HAVERHILL CITY COUNCIL AGENDA

Tuesday, August 24, 2021 at 7:00 PM

Theodore A. Pelosi, Jr. Council Chambers, 4 Summer st, Room 202 In-Person/Remote Meeting

13. MOTIONS AND ORDERS:

13.1. Order – Precinct Officers in the several wards of the City for the year 2021

14. COMMUNICATIONS FROM COUNCILLORS:

- 14.1. Communication from Councillor Daly O'Brien requesting to discuss closing Washington st and Wingate st on Friday and Saturday evenings making them pedestrian only
- 14.2. Communication from Councillor Daly O'Brien requesting to discuss a constituent's request to put an end to commercial truck traffic on Mill st and the issue of truck traffic through residential neighborhoods throughout the City
- 14.3. Communication from Councillor Joseph Bevilacqua requesting to discuss the opportunity for additional senior citizen housing
- 14.4. Communication from Councillor Joseph Bevilacqua requesting to recognize the 20th Anniversary Commemoration of the September 11, 2001 terrorist attacks
- 14.5. Communication from Councillor Daly O'Brien and Councillor Bevilacqua requesting to discuss the continuing neighborhood concerns with NETTS tractor trailer traffic on Monument st
- 15. Unfinished Business Of Preceding Meeting
- 16. RESOLUTIONS AND PROCLAMATIONS
- 17. COUNCIL COMMITTEE REPORTS AND ANNOUNCEMENTS
- 18. DOCUMENTS REFERRED TO COMMITTEE STUDY
- 19. Long term matters study list
- 20. ADJOURN



City Clerk's Office, Room 118 Phone: 978-374-2312 Fax: 978-373-8490 cityclerk@cityofhaverhill.com

August 20, 2021

Council President Barrett and Members of the City Council

RE: Early Voting in person

Dear President Barrett and Councillors:

As you are aware, the City will hold a preliminary election on September 14 2021. The Massachusetts Legislature has passed legislation allowing cities and towns holding municipal elections to conduct early voting this year, in person or by mail, before September 14th.

It is my recommendation that early voting be held in person in City Hall basement (former RMV location) from Tuesday, September 7 through Friday, September 10, from 8-4 and on Thursday, September 9, from 8-8PM. Additionally, I also recommend early voting be held on Sunday, September 5 from 2:30-8PM at Somebody Cares, located at 358 Washington St.

I request the Council's approval for this request.

Linda L Koutoulas

Sincerely

Haverhill City Clerk





ASSESSORS OFFICE – ROOM 115 Phone: 978-374-2316 Fax: 978-374-2319 Assessors@cityofhaverhill.com

Aug.13,2021

TO: MEMBERS OF THE HAVERHILL CITY COUNCIL:

In accordance with Municipal Ordinance, Chapter 7, entitled "Assessor" as follows:

The Board of Assessors shall file monthly with the City Council a copy of the report submitted to the Auditor showing a summary of the above abated amounts for that month.

Attached herewith is the report for the month of July as filed in the Assessors Office.

Very truly yours,

Christine Webb, MAA

Assessor

Transaction Summary All Years City of Haverhill

Page 1 of 2

All Entry Date range 07/01/2021 through 07/31/2021 for Abatements

8/16/2021 9:20:55AM

Transaction Summary All Years City of Haverhill

Page 2 of 2

All Entry Date range 07/01/2021 through 07/31/2021 for Abatements

			88.10	43,388.		Total All Charges	Total /				
0.00		43,388.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	Report
0.00	0	26,285.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2021
0.00	0	2,698.75	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2021 Real Estate
0.00	0	2,698.75	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	Property Tax
₽	Exemp	Abate	Refunds Reversals	Refunds	Reversals	Paid Reversals Reversals Reversals	Reversals	Paid	Paid	Paid	Totals
			Refund		Fee	Interest	Tax	Fees	Interest	Tax	

Total All Charges: Add all columns except Adjustments.

32 - C

C8P-N-8

ROBERT D. HA

ATTORNEY AT LAW 17 WEST STREET HAVERHILL, MASSACHUSETTS 01830

TEL: (978) 373-5611 FAX: (978) 373-7441 EMAIL: bobharb@aol.com Of Counsel

Alfred J. Cirome

April 8, 2021

City of Haverhill City Council 4 Summer Street, Haverhill, MA 01830

RE: 139 Amesbury Line Road:

Application For Solar Energy System Special Permit and Water Supply Protection District (WSPD) Special Permit

Dear City Council:

On behalf of the Applicant and Lessee, Solar Smart LLC, application is hereby made for a Special Permit for Large Scale Ground Mounted Solar Energy System in accordance with the City Zoning Ordinance (see Sections 7.8 and following).

Application is also made for a Special Permit for the installation of this solar energy system within the Water Supply Protection District in accordance with the City Zoning Ordinance (See Section 9.2.7).

Reference is hereby made to all the Plans and Specifications filed with this Application as well as the written testimony of Kyle Burchard, P.E. also filed with this Application and incorporated herein by reference

Financial Surety for this Large Scale Ground Mounted Solar Energy System project has been reviewed with the Planning Director and will be filed if this Special permit is approved during the Appeal period.

Applicant, based upon the testimony, plans and evidence submitted herewith and supplemented at the Public Hearing, respectfully requests the City Council to make a written determination and find that:

- 1. The proposed use or structure(s) shall not cause substantial detriment to the neighborhood or the City, taking into account the characteristics of the site and of the proposal in relation to that site.
- 2. The grant of a special permit for a large-scale ground-mounted solar energy system will promote the highest and best use of the subject property, taking into account the characteristics of the

subject property, including past land uses, possible presence of hazardous materials, and other development limitations.

- 3. There are Community energy needs which are served by this Project.
 - 4. There is safe traffic and pedestrian flow provided by this Project.
 - 5. There are adequate utilities and other public services for this Project.
 - 6. The Natural Environment will not be impacted.
 - 7. There is no impact on City services and this project will increase the city tax base.

In addition to meeting the above, the Council can also find that the proposed use:

- 1. Satisfies the design and operations guidelines set forth in the Zoning Ordinance;
- 2. Is in harmony with the purposes and intent of this Section and will promote the purposes of the WSPD;
- 3. Is appropriate to the natural topography, soils, and other characteristics of the site to be developed;
- 4. Will not, during construction or thereafter, have an adverse environmental impact on any water body or watercourse in the district; and 5. Will not adversely affect the quality or quantity of an existing water supply.

The Applicant respectfully requests Council approval of both the Solar Energy System Special Permit and The Water Supply Protection District (WSPD) Special Permit.

Robert D. Harb, Attorney for Solar Smart LLC
IN CITY COUNCIL: April 27 2021 VOTED: that HEARING BE HELD JUNE 15 2021 Attest:
Acting City Clerk
N CITY COUNCIL: June 15 2021 POSTPONED TO AUGUST 24 2021
City Clerk

Respectfully submitted

ROBERT D. HARB

ATTORNEY AT LAW 17 WEST STREET HAVERHILL, MASSACHUSETTS 01830

TEL: (978) 373-5611 FAX: (978) 373-7441

EMAIL:

Of Counsel Alfred

Alfred J. Cirome

June 15, 2021

City of Haverhill Haverhill City Council 4 Summer Street, Haverhill, MA 01830

Delivered In Hand

CC5P21-8

RE: 139 Amesbury Line Road: Special Permit Hearings: CCSP-21-8 and CCSP-21-9

Request For Continuance

CCSP-21-8 Application For Special Permit For Large Scale Ground Mounted Solar Energy System and

CCSP-21-9 - Application For Special Permit for Installation of a Large Scale Ground Mounted Solar energy System in the Water Supply Protection Overlay District (WSPOD)

Dear City Council:

On behalf of the Applicant and Lessee, Solar Smart LLC, request is hereby made for a continuance of the hearings for the above two Special Permit Hearing until August 24, 2021.

Applicant has been diligently working with all City Departments, including Fire, Conservation and Water Departments, and the abutters prior to and after filing the above Applications. There remain a few outstanding items that are moving towards a resolution; thus, this request for a continuance to allow the applicant the time to resolve these items.

This is Applicant's first request for a continuance.

Applicant hereby waives the 120-day hearing requirement.

Respectfully submitted,

Robert D. Harb, Attorney for Solar Smart LLC

CESP - 21 - 9 32-1

n

ROBERT D. HARB

ATTORNEY AT LAW 17 WEST STREET HAVERHILL, MASSACHUSETTS 01830 10,2)

TEL: (978) 373-5611 FAX: (978) 373-7441 EMAIL: <u>bobharb@aol.com</u> Of Counsel
Alfred J. Cirome

April 8, 2021

City of Haverhill
City Council
4 Summer Street, Haverhill, MA 01830

RE: 139 Amesbury Line Road:

Application For Solar Energy System Special Permit and Water Supply Protection District (WSPD) Special Permit

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- 2. The grant of a special permit for a large-scale ground-mounted solar energy system will promote the highest and best use of the subject property, taking into account the characteristics of the

2 S

subject property, including past land uses, possible presence of hazardous materials, and other development limitations.

- 3. There are Community energy needs which are served by this Project.
- 4. There is safe traffic and pedestrian flow provided by this Project.
- 5. There are adequate utilities and other public services for this Project.
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- 7. There is no impact on City services and this project will increase the city tax base.

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- 1. Satisfies the design and operations guidelines set forth in the Zoning Ordinance;
- 2. Is in harmony with the purposes and intent of this Section and will promote the purposes of the WSPD;
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Respectfully submitted Author Low Robert D. Harb, Attorney for Solar Sma	Solor Smooth LLC rt LLC
IN CITY COUNCIL: April 27 2021 VOTED THAT COUNCIL HEARING BE 1 JUNE 15 2021 Attest:	HELD
Ac	ting City Cler k
IN CITY COUNCIL: June 15 2021 POSTPONED TO AUGUST 24 2021 ATTEST:C	ity Clerk



CCSP-21-8

City Council Special Permit

Status: Active

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611 Date Created: Apr 13, 2021

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Important: Please Read Before Starting Your Application

Applicant Information

What is Your Role in This Process?

Attorney/Agent

Applicant Business/Firm Phone

9783735611

Applicant Business/Firm City

Haverhill

Applicant Business/Firm Zip

01830

Client Business Name

Solar Smart LLC

Client Email

peterr@solarsmartllc.com

Client City

Sommerville

Client Zip

29483

Client Business Structure

Limited Liability Corporation (LLC)

Applicant Business/Firm Name

Attorney Robert D Harb

Applicant Business/Firm Address

17 West Street

Applicant Business/Firm State

MA

Client Name

Solar Smart LLC

Client Phone

843-743-9180

Client Address

1207 Congressional Blvd.

Client State

SC

Client County

Dorchester

Property Information

Proposed Housing Plan Name

Solar Photovoltaic Project

How Long Owned by Current Owner?

13 years more or less

Lot Dimension(s)

583+feet frontage:718.27+ mean depth; and 26.813 acres

Zoning District Where Property Located

RS - Residential Rural Special

Proposed Street Name(s)

N/A

Type of Dwelling(s) Planned in Project

Single Family

Registry Plat Number, Block & Lot

430-11-12

08/18/2021

OpenGov

8/18/2021

PLEASE READ

8/18/2021 Office Use Only City Council Decision Reason for Council's Decision **City Council Members Absent City Council Members Present Continuance Meeting Date City Councilor Who Seconded Motion** City Councilors Who Voted Against Continuance Motion Decision City Councilors Who Voted in Favor Number of 12"x18" Mylar Copies

City Council Hearing Date

Also Present

City Councilor Who Made Motion

City Councilors Who Abstained

Who Submitted Continuance Request?

Appeal Expiration Date

Number of 18"x24" Mylar Copies

Attachments

Number of 24"x36" Mylar Copies

And ted x assent.pdf Uploaded by Robert Harb on Apr 8, 2021 at 10:16 pm (pdf) Haverhill Solar CC Special Permit Application Letter.pdf Uploaded by Robert Harb on Apr 8, 2021 at 10:22 pm doo Planning Board decision not required for Application.docx Uploaded by Robert Harb on Apr 8, 2021 at 10:49 pm doc3Approved Site Plan not required for Application.docx Uploaded by Robert Harb on Apr 8, 2021 at 10:49 pm pdf xenakis-plan-image - 2021-04-08T220120.941.pdf Uploaded by Robert Harb on Apr 8, 2021 at 10:23 pm pdf solar app-c.pdf Uploaded by Robert Harb on Apr 13, 2021 at 12:08 pm pdf ccsp 21 9 gpr.pdf Uploaded by LINDA KOUTOULAS on Apr 16, 2021 at 11:44 am pdf Haverhill Solar Site Plan Set 2021.04.08.pdf Uploaded by Robert Harb on Apr 8, 2021 at 10:34 pm pdf Appendix1-Solar Farm Components.pdf Uploaded by Robert Harb on Apr 8, 2021 at 10:31 pm pdf Appendix2-SWM Report and O&M.pdf Uploaded by Robert Harb on Apr 8, 2021 at 10:35 pm pdf Appendix3-Solar Facility O&M.pdf Uploaded by Robert Harb on Apr 8, 2021 at 10:31 pm [pdf]Appendix4-ConstructionAccessAgreement.pdf

Uploaded by Robert Harb on Apr 8, 2021 at 10:30 pm (pdf)Appendix5-Electrical One-Line Diagram (139 Amesbury Line Haverhill MA PV Rev6-E-1).pdf Uploaded by Robert Harb on Apr 8, 2021 at 10:30 pm

pdf Appendix6-Solar Site Illustratives.pdf

Uploaded by Robert Harb on Apr 8, 2021 at 10:31 pm

PDFAppendix7-Whittier School Sewer Plan.PDF -/Uploaded by Robert Harb on Apr 8, 2021 at 10:44 pm

[pdf]solar control.pdf

Uploaded by Robert Harb on Apr 8. 2021 at 11:01 pm

8/18/2021 OpenGov pdf solar description.pdf Uploaded by Robert Harb on Apr 13, 2021 at 12:09 pm (csv Abutters 139 Amesbury Line Rd 430.11.12.csv Uploaded by Christine Webb on Apr 16, 2021 at 1:00 pm pdf Mailing Labels 139 Amesbury Line Rd 430.11.12.pdf Uploaded by Christine Webb on Apr 16, 2021 at 1:00 pm pdf 06-15-21 CCSP-8 solar 139 Amesbury Line.pdf Uploaded by LINDA KOUTOULAS on May 6, 2021 at 2:57 pm doc Beekeeper Request.doc Uploaded by Robert Harb on May 24, 2021 at 1:26 pm. [pdf]20210602_33-1499_CEIStormwaterPeerReview1.pdf Uploaded by Robert Moore on Jun 11, 2021 at 12:46 pm pdf)Haverhill Solar AMENDED CC Special Permit Application Letter 2021.08.16.pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:31 pm (pdf Haverhill Solar AMENDED Site Plan Set 2021.08.16.pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:53 pm pdf Appendix1-AMENDED Solar Farm Components.pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:40 pm pdf Appendix1-AMENDED Solar Farm Components.pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:39 pm pdf Appendix2-AMENDED SWM Report and O&M.pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:44 pm pdf Appendix3-Solar Facility O&M.pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:38 pm [pdf]Appendix4-ConstructionAccessAgreement.pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:37 pm pdf)Appendix5-AMENDED Electrical One-Line Diagram (139 Amesbury Line Haverhill MA PV One-Line Rev9-E-1).pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:38 pm pdf Appendix6-Solar Site Illustratives.pdf Uploaded by Robert Harb on Aug 17, 2021 at 6:39 pm PDF Appendix 7-Whittier School Sewer Plan. PDF Uploaded by Robert Harb on Aug 17, 2021 at 6:58 pm

pdf Appendix8-AMENDED Haverhill Fire Department Cart Path Proposal.pdf

ಚರಾXSolar-2021.08.16 189 Amesbury Line Rd - Special Permit Comments and RESPONSES.docx

Uploaded by Robert Harb on Aug 17, 2021 at 6:42 pm

Uploaded by Robert Harb on Aug 17, 2021 at 6:40 pm

History

Date	Activity
Apr 8, 2021 at 9:47 pm	Robert Harb started a draft of Record CCSP-21-8
Apr 8, 2021 at 10:24 pm	Robert Harb added attachment _Haverhill Solar Site Plan Set 2021.04.08.pdf to Record CCSP-21-8
Apr 8, 2021 at 10:28 pm	Robert Harb added attachment Appendix1-Solar Farm Components.pdf to Record CCSP-21-8
Apr 8. 2021 at 10:28 pm	Robert Harb added attachment Appendix2-SWM Report and O&M.pdf to Record CCSP-21-8
Apr 8, 2021 at 10:29 pm	Robert Harb added attachment Appendix3-Solar Facility O&M.pdf to Record CCSP-21-8
Apr 8, 2021 at 10:29 pm	Robert Harb added attachment Appendix3-Solar Facility O&M.pdf to Record CCSP-21-8
Apr 8, 2021 at 10:29 pm	Robert Harb added attachment Appendix4-ConstructionAccessAgreement.pdf to Record CCSP-21-8
Apr 8, 2021 at 10:29 pm	Robert Harb added attachment Appendix5-Electrical One-Line Diagram (139 Amesbury Line Haverhill MA PV Rev6-E-1).pdf to Record CCSP-21-8
Apr 8, 2021 at 10:30 pm	Robert Harb added attachment Appendix6-Solar Site Illustratives.pdf to Record CCSP-21-8
Apr 8. 2021 at 10:30 pm	Robert Harb added attachment Appendix6-Solar Site Illustratives.pdf to Record CCSP-21-8
Apr 8, 2021 at 10:30 pm	Robert Harb added attachment Appendix 7-Whittier School Sewer Plan. PDF to Record CCSP-21-8
Apr 8, 2021 at 10:37 pm	Robert Harb removed attachment Appendix3-Solar Facility O&M.pdf from Record CCSP-21-8
Apr 8, 2021 at 10:37 pm	Robert Harb removed attachment Appendix6-Solar Site Illustratives.pdf from Record CCSP-21-8
Apr 8. 2021 at 11:01 pm	Robert Harb added attachment solar control pdf to Record CCSP-21-8
Apr 13, 2021 at 12:09 pm	Robert Harb added attachment solar description,pdf to Record CCSP-21-8
Apr 13, 2021 at 12:11 pm	Robert Harb submitted Record CCSP-21-8
Apr 13, 2021 at 12:33 pm	completed payment step Special Permit Filing Fee on Record CCSP-21-8
Apr 13, 2021 at 12:33 pm	approval step Building Inspector Review was assigned to Tom Bridgewater on Record CCSP-21-8
Apr 13, 2021 at 12:33 pm	approval step Planning Director Review was assigned to William Pillsbury on Record CCSP-21-8
Apr 13, 2021 at 12:33 pm	approval step City Clerk Review - Hearing Dates Set was assigned to Maria Bevilacqua on Record CCSP-21-8
Apr 13, 2021 at 12:57 pm	LINDA KOUTOULAS assigned approval step City Council Clerk Notified to LINDA KOUTOULAS on Record CCSP-21-8
Apr 13, 2021 at 12:58 pm	LINDA KOUTOULAS assigned approval step Assessor for Abutter's List to Christine Webb on Record CCSP-21-8
Apr 13, 2021 at 12:58 pm	LINDA KOUTOULAS assigned approval step Conservation Department Review to Robert Moore on Record CCSP-21-8



08/18/2021

CCSP-21-9

City Council Special Permit

Status: Active

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611 Date Created: Apr 15, 2021

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Important: Please Read Before Starting Your Application

Applicant Information

What is Your Role in This Process?

Attorney/Agent

Applicant Business/Firm Phone

19783735611

Applicant Business/Firm City

Haverhill

Applicant Business/Firm Zip

01830

Client Business Name

SOLAR SMART LLC

Client Email

PETERR@SOLARSMARTLLC.COM

Client City SOMMERVILLE

Client Zip 29483

Client Business Structure

Limited Liability Corporation (LLC)

Applicant Business/Firm Name

Attorney Robert D Harb

Applicant Business/Firm Address

17 West Street

Applicant Business/Firm State

MA

Client Name

SOLAR SMART LLC

Client Phone

843-743-9180

Client Address

1207 CONGRESSIONAL BLVD

Client State

SC

Client County

DORCHESTER

Property Information

Proposed Housing Plan Name

SOLAR PHOTOVOLTAIC PROJECT

How Long Owned by Current Owner?

13 YEARS MORE OR LESS

Lot Dimension(s)

583+feet frontage;718.27+ mean depth; and 26.813 acres

Zoning District Where Property Located

WSPD - Water Supply Protection District

Proposed Street Name(s)

N/A

Type of Dwelling(s) Planned in Project

Single Family

Registry Plat Number, Block & Lot

430-11-12

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8/18/2021	OpenGov
Deed Recorded in Essex South Registry: Block Number 27892	openacov
Deed Recorded in Essex South Registry: Page 453	
Does the Property Have Multiple Lots? No	IF YES, How Many Lots?
IF YES, What Is/Are the Map, Block Lot (MBL) Number(s)?	
Thoroughly Describe the Reason(s) for thre Special Permit WATER SUPPLY PROTECTION OVERLAY DISTRICT (WSPOD) SPECIAL SOLAR ENERGY STSTEM IN THE WSPOD.	PERMIT FOR INSTALLATION OF A LARGE SCALE GROUND MOUNTED
Property Description SEE PLANS AND BOUNDED DESCRIPTION FILED HEREWITH FOR PROUNDERLYING ZONES	OPERTY DESCRIPTION . nOTE PROPERTY ALOS INCLIDED IN RS AND RM
Current Property Use Residential Housing	TOTAL Number of Units Planned
TOTAL Number of Parking Spaces Planned O	
Special Circumstances	
Building Coverage ☐	Dimensional Variance □
Front Yard Setback	Side Yard Setback □
Rear Yard Setback	Lot Frontage
Lot Depth	Lot Area
Building Height	Floor Area Ratio
Open Space □	Parking
Sign Size □	Use □
Other ☑	IF OTHER, Please Describe Water Supply Protection District Overlay (WSPOD) Special Permit
Hearing Waiver	
Agrees No	
Agreement & Signature	
Agrees ☑	

Office Use Only **City Council Hearing Date City Council Decision Reason for Council's Decision City Council Members Absent City Council Members Present** Also Present **Continuance Meeting Date City Councilor Who Made Motion City Councilor Who Seconded Motion City Councilors Who Abstained** City Councilors Who Voted Against **Who Submitted Continuance Request? Continuance Motion Decision** City Councilors Who Voted in Favor **Appeal Expiration Date** Number of 12"x18" Mylar Copies Number of 18"x24" Mylar Copies Number of 24"x36" Mylar Copies **Attachments** pdf ted x assent.pdf Uploaded by Robert Harb on Apr 15, 2021 at 7:26 pm [pdf]_Haverhill Solar CC Special Permit Application Letter.pdf Uploaded by Robert Harb on Apr 15, 2021 at 7:28 pm doc)Planning Board decision not required for Application.docx Uploaded by Robert Harb on Apr 15, 2021 at 7:29 pm doc)Approved Site Plan not required for Application.docx Uploaded by Robert Harb on Apr 15, 2021 at 7:29 pm pdf xenakis-plan-image - 2021-04-08T220120.941.pdf Uploaded by Robert Harb on Apr 15, 2021 at 7:30 pm pdf solar application.pdf Uploaded by Robert Harb on Apr 15, 2021 at 7:35 pm pdf Haverhill Solar Site Plan Set 2021.04.08.pdf Uploaded by Robert Harb on Apr 15, 2021 at 7:48 pm pdf Appendix1-Solar Farm Components.pdf Jupioaded by Robert Harb on Apr 15, 2021 at 7:46 pm pdf Appendix2-SWM Report and O&M.pdf

Uploaded by Robert Harb on Apr 15, 2021 at 7:50 pm

pdf Appendix3-Solar Facility O&M.pdf Uploaded by Robert Harb on Apr 15, 2021 at 7:46 pm

pdf Appendix4-ConstructionAccessAgreement.pdf

Uploaded by Robert Harb on Apr 15, 2021 at 7:45 pm

(pdf)Appendix5-Electrical One-Line Diagram (139 Amesbury Line Haverhill MA PV Rev6-E-1).pdf

√Upioaded by Robert Harb on Apr 15, 2021 at 7:45 pm (pdf)Appendix6-Solar Site Illustratives.pdf

- $^{\prime}$ Uploaded by Robert Harb on Apr 15, 2021 at 7:47 pm

(PDP)Appendix7-Whittier School Sewer Plan.PDF √Uploaded by Robert Harb on Apr 15, 2021 at 8:02 pm

[pdf]solar control.pdf

Uploaded by Robert Harb on Apr 15, 2021 at 7:48 pm

√solar description.pdf Uploaded by Robert Harb on Apr 15, 2021 at 7:49 pm (pdf)ccsp 21 9 gpr.pdf Uploaded by LINDA KOUTOULAS on Apr 16, 2021 at 11:41 am csv Abutters 139 Amesbury Line Rd 430.11.12.csv Uploaded by Christine Webb on Apr 22, 2021 at 8:05 am (pdf)Mailing Labels 139 Amesbury Line Rd 430.11.12.pdf Uploaded by Christine Webb on Apr 22, 2021 at 8:06 am (pdf)06-15-21 CCSP-21-9 Spec Permit WSPOD.pdf Uploaded by LINDA KOUTOULAS on May 6, 2021 at 2:57 pm doc Beekeeper Request.doc Uploaded by Robert Harb on May 24, 2021 at 1:25 pm (pdf)20210602_33-1499_CEIStormwaterPeerReview1.pdf Uploaded by Robert Moore on Jun 11, 2021 at 12:48 pm pdf Haverhill Solar AMENDED CC Special Permit Application Letter 2021.08.16.pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:00 pm. pdf_Haverhill Solar AMENDED Site Plan Set 2021.08.16.pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:26 pm pdf Appendix1-AMENDED Solar Farm Components.pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:05 pm pdf Appendix2-AMENDED SWM Report and O&M.pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:10 pm pdf Appendix3-Solar Facility O&M.pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:04 pm pdf Appendix4-ConstructionAccessAgreement.pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:04 pm pdf Appendix5-AMENDED Electrical One-Line Diagram (139 Amesbury Line Haverhill MA PV One-Line Rev9-E-1).pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:04 pm pdf Appendix6-Solar Site Illustratives.pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:05 pm PDPAppendix7-Whittier School Sewer Plan.PDF Uploaded by Robert Harb on Aug 17, 2021 at 8:26 pm pdf Appendix8-AMENDED Haverhill Fire Department Cart Path Proposal pdf Uploaded by Robert Harb on Aug 17, 2021 at 8:08 pm GookSolar-2021.08.16 189 Amesbury Line Rd - Special Permit Comments and RESPONSES.docx Uploaded by Robert Harb on Aug 17, 2021 at 8:05 pm

History

Date	Activity
Apr 15, 2021 at 7:15 pm	Robert Harb started a draft of Record CCSP-21-9
Apr 15, 2021 at 7:37 pm	Robert Harb added attachment _Haverhill Solar Site Plan Set 2021.04.08.pdf to Record CCSP-21-9
Apr 15, 2021 at 7:42 pm	Robert Harb added attachment Appendix1-Solar Farm Components.pdf to Record CCSP-21-9
Apr 15, 2021 at 7:43 pm	Robert Harb added attachment Appendix2-SWM Report and O&M.pdf to Record CCSP-21-9
Apr 15, 2021 at 7:43 pm	Robert Harb added attachment Appendix3-Solar Facility O&M.pdf to Record CCSP-21-9
Apr 15, 2021 at 7:44 pm	Robert Harb added attachment Appendix4-ConstructionAccessAgreement.pdf to Record CCSP-21-9
Apr 15, 2021 at 7:44 pm	Robert Harb added attachment Appendix5-Electrical One-Line Diagram (139 Amesbury Line Haverhill MA PV Rev6-E-1).pdf to Record CCSP-21-9
Apr 15, 2021 at 7:45 pm	Robert Harb added attachment Appendix6-Solar Site Illustratives.pdf to Record CCSP-21-9
Apr 15, 2021 at 7:45 pm	Robert Harb added attachment Appendix7-Whittier School Sewer Plan.PDF to Record CCSP-21-9
Apr 15, 2021 at 7:48 pm	Robert Harb added attachment solar control pdf to Record CCSP-21-9
Apr 15. 2021 at 7:49 pm	Robert Harb added attachment solar description.pdf to Record CCSP-21-9
Apr 15, 2021 at 8:03 pm	Robert Harb submitted Record CCSP-21-9
Apr 15, 2021 at 8:12 pm	completed payment step Special Permit Filing Fee on Record CCSP-21-9
Apr 15, 2021 at 8:12 pm	approval step Building Inspector Review was assigned to Tom Bridgewater on Record CCSP-21-9
Apr 15, 2021 at 8:12 pm	approval step Planning Director Review was assigned to William Pillsbury on Record CCSP-21-9
Apr 15, 2021 at 8:12 pm	approval step City Clerk Review - Hearing Dates Set was assigned to Maria Bevilacqua on Record CCSP-21-9
Apr 16, 2021 at 11:07 am	William Pillsbury approved approval step Planning Director Review on Record CCSP-21-9
Apr 16, 2021 at 11:41 am	LINDA KOUTOULAS added attachment Zoning opinion to Record CCSP-21-9
Apr 16, 2021 at 11:41 am	LINDA KOUTOULAS removed attachment Zoning Opinion from Record CCSP-21-9
Apr 21, 2021 at 3:58 pm	LINDA KOUTOULAS changed IF OTHER. Please Describe from "Water Supply Protection District (WSPD) Special Permit" to "Water Supply Protection District Overlay (WSPOD) Special Permit" on Record CCSP-21-9

Date	Activity
Apr 21, 2021 at 3:58 pm	LINDA KOUTOULAS changed Thoroughly Describe the Research 6. H. C.
	PROTECTION DISTRICT (WSPD) SPECIAL PERMIT FOR INSTALLATION OF A LARGE SCALE GROUND M" to "WATER SUPPLY PROTECTION OVERLAY DISTRICT (WSPOD) SPECIAL PERMIT FOR INSTALLATION OF A LARGE SCALE GROUND M" to "WATER SUPPLY PROTECTION OVERLAY DISTRICT (WSPOD) SPECIAL PERMIT FOR INSTALLATION OF A LARGE SCALE" or Record CCSP-21-9
Apr 21, 2021 at 3:58 pm	LINDA KOUTOULAS changed Thoroughly Describe the Pagent's forthing
	PROTECTION OVERLAY DISTRICT (WSPOD) SPECIAL PERMIT FOR INSTALLATION OF A LARGE SCALE" to "WATER SUPPLY PROTECTION OVERLAY DISTRICT (WSPOD) SPECIAL PERMIT FOR INSTALLATION OF A LARGE SCALE" to "WATER Record CCSP-21-9
Apr 21, 2021 at 3:59 pm	LINDA KOUTOULAS assigned approval step City Council Clerk Notified to LINDA KOUTOULAS on Record CCSP-21-9
Apr 21, 2021 at 3,59 pm	LINDA KOUTOULAS assigned approval step Assessor for Abutter's List to Christine Webb on Record CCSP-21-9
Apr 21, 2021 at 3:59 pm	LINDA KOUTOULAS assigned approval step Conservation Department Review to Robert Moore on Record CCSP-21-9
Apr 21, 2021 at 3:59 pm	LINDA KOUTOULAS assigned approval step DPW Review to John Pettis on Record CCSP-21-9
Apr 21, 2021 at 3:59 pm	LINDA KOUTOULAS assigned approval step Engineering Department Review to John Pettis on Record CCSP-21-9
Apr 21, 2021 at 3:59 pm	LINDA KOUTOULAS assigned approval step Fire1 Department Review to Robert O'Brien on Record CCSP-21-9
Apr 21. 2021 at 3:59 pm	LINDA KOUTOULAS assigned approval step Health Department Review to Bonnie Dufresne on Record CCSP-21-9
Apr 21, 2021 at 3:59 pm	LINDA KOUTOULAS assigned approval step Police Department Review to Robert Pistone on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step School Department Review to Robert Pistone on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step School Department Review to Margaret Marotta on Record CCSP-21-9 LINDA KOUTOULAS assigned approval step Storm Water Devices to Parket Marotta on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step Storm Water Review to Robert Ward on Record CCSP-21-9 LINDA KOUTOULAS assigned approval step Wastewater Review to Robert Ward on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step Wastewater Review to Robert Ward on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step Water Department Review to Robert Ward on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step Water Supply Review to Robert Ward on Record CCSP-21-9
	LINDA KOUTOULAS assigned approval step Planning Director Approval for Agenda to William Pillsbury on Record CC 21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step Building Inspector Approval for Agenda to Tom Bridgewater on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step First Ad Placement to LINDA KOUTOULAS on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step Placed on Agenda to LINDA KOUTOULAS on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step Abutter Notification to LINDA KOUTOULAS on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step Second Ad Placement to LINDA KOUTOULAS on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step City Councilor A Review to Melinda Barrett on Record CCSP-21-9
Apr 21, 2021 at 4:00 pm	LINDA KOUTOULAS assigned approval step City Councilor B Review to Colin LePage on Record CCSP-21-9
Apr 21, 2021 at 4:01 pm	LINDA KOUTOULAS assigned approval step City Councilor C Review to Joe Bevilacqua on Record CCSP-21-9
Apr 21, 2021 at 4:01 pm	LINDA KOUTOULAS assigned approval step City Councilor D Review to John Michitson on Record CCSP-21-9
Apr 21, 2021 at 4:01 pm	LINDA KOUTOULAS assigned approval step City Councilor E Review to Thomas Sullivan on Record CCSP-21-9
Apr 21, 2021 at 4:01 pm	LINDA KOUTOULAS assigned approval step City Councilor F Review to Tim Jordan on Record CCSP-21-9
Apr 21, 2021 at 4:01 pm	LINDA KOUTOULAS assigned approval step City Councilor G Review to Michael McGonagle on Record COSB 21.0
pr 21, 2021 at 4:01 pm	LINDA KOUTOULAS assigned approval step City Councilor H Review to Mary Ellen Daly O'Brien on Record CCSP-21-9
pr 21, 2021 at 4:01 pm	LINDA KOUTOULAS assigned approval step City Councilor I Review to William Macek on Record CCSP-21-9
pr 21, 2021 at 4:01 pm	LINDA KOUTOULAS assigned approval step City Council Meeting to LINDA KOUTOULAS on Record CCSP-21-9
pr 22, 2021 at 8:05 am	Christine Webb added attachment Abutters 139 Amesbury Line Rd 430.11.12.csv to Record CCSP-21-9
pr 22, 2021 at 8:06 am	Christine Webb added attachment Mailing Labels 139 Amesbury Line Rd 430.11.12.pdf to Record CCSP-21-9
lay 6, 2021 at 2:57 pm	LINDA KOUTOULAS added attachment 06-15-21 CCSP-21-9 Spec Permit WSPOD.pdf to Record CCSP-21-9
lay 12, 2021 at 10:54 am	Tom Bridgewater approved approval step Building Inspector Review on Record CCSP-21-9
lay 18. 2021 at 8:13 am	LINDA KOUTOULAS assigned approval step City Clerk Review - Hearing Dates Set to LINDA KOUTOULAS on Record CCSP-21-9
ay 18, 2021 at 8:13 am	LINDA KOUTOULAS approved approval step City Clerk Review - Hearing Dates Set on Record CCSP-21-9
ay 18, 2021 at 8:13 am	LINDA KOUTOULAS approved approval step City Council Clerk Notified on Record CCSP-21-9
lay 18, 2021 at 8:13 am	LINDA KOUTOULAS assigned approval step Assessor for Abutter's List to LINDA KOUTOULAS on Record CCSP-21-9
ay 18, 2021 at 8:13 am	LINDA KOUTOULAS waived approval step Assessor for Abutter's List on Record CCSP-21-9
ay 18. 2021 at 8:13 am	approval step Fire2 Department Review was assigned to Michael Picard on Record CCSP-21-9
ay 18, 2021 at 8:30 am	Eric Tarpy assigned approval step Fire! Department Review to Eric Tarpy on Record CCSP-21-9
ay 18. 2021 at 8:36 am	Robert Pistone approved approval step Police Department Review on Record CCSP-21-9
ay 18. 2021 at 8:37 am	Bonnie Dufresne assigned approval step Health Department Review to Mark Tolman on Record CCSP-21-9
ay 18, 2021 at 4:27 pm	Michael Picard approved approval step Fire2 Department Review on Record CCSP-21-9
ay 24, 2021 at 1:25 pm	Robert Harb added attachment Beekeeper Request doc to Record CCSP-21-9
ay 25, 2021 at 3:53 pm	Eric Tarpy approved approval step Fire1 Department Review on Record CCSP-21-9
ay 27, 2021 at 9:42 am	Karen Buckley assigned approval step DPW Review to Karen Buckley on Record CCSP-21-9
ay 27, 2021 at 9:42 am	Karen Buckley assigned approval step DPW Review to John Pettis on Record CCSP-21-9
ay 27, 2021 at 9:44 am	Karen Buckley assigned approval step Water Supply Review to Paul Jessel on Record CCSP-21-9

Date	Activity Activity Devil lossed on Record CCSP-21-9
May 27, 2021 at 9:44 am	Karen Buckley assigned approval step Wastewater Review to Paul Jessel on Record CCSP-21-9
May 27, 2021 at 9:45 am	Karen Buckley assigned approval step Water Department Review to Glenn Smith on Record CCSP-21-9 Karen Buckley assigned approval step Water Department Review to Glenn Smith on Record CCSP-21-9
May 27, 2021 at 9:45 am	Karen Buckley assigned approval step Water Supply Review to John D'Aoust on Record CCSP-21-9 Karen Buckley assigned approval step Water Supply Review to John D'Aoust on Record CCSP-21-9
May 27, 2021 at 10:29 am	Paul Jessel approved approval step Wastewater Review on Record CCSP-21-9
May 27, 2021 at 1:47 pm	John D'Aoust approved approval step Water Supply Review on Record CCSP-21-9
Jun 1, 2021 at 4:41 pm	Glenn Smith approved approval step Water Department Review on Record CCSP-21-9
Jun 8, 2021 at 8:48 am	Glenn Smith approved approval step Water Department Review to Mike Pfifferling on Record CCSP-21-9 LINDA KOUTOULAS assigned approval step School Department Review to Mike Pfifferling on Record CCSP-21-9
Jun 8, 2021 at 2:19 pm	Mark Tollman approved approval step Health Department Review on Record CCSP-21-9
Jun 9, 2021 at 11:59 am	Mike Pfifferling approved approval step School Department Review on Record CCSP-21-9 Mike Pfifferling approved approval step School Department Review on Record CCSP-21-9
Jun 10, 2021 at 9:18 am	LINDA KOUTOULAS assigned approval step Storm Water Review to Robert Moore on Record CCSP-21-9
Jun 11, 2021 at 12:47 pm	Robert Moore approved approval step Conservation Department Review on Record CCSP-21-9
Jun 11, 2021 at 12:47 pm	Robert Moore approved approval step Storm Water Review on Record CCSP-21-9
Jun 11, 2021 at 12:48 pm	Robert Moore added attachment Stormwater Peer Review #1 to Record CCSP-21-9
Aug 12, 2021 at 9:48 am	LINDA KOUTOULAS assigned approval step DPW Review to Mike Stankovich on Record CCSP-21-9 Robert Harb added attachment Haverhill Solar AMENDED CC Special Permit Application Letter 2021.08.16.pdf to Record
Aug 17, 2021 at 8:00 pm	
	Haverbill Solar AMENDED Site Plan Set 2021.08.16.pdf to Record CCSP-21-9
Aug 17, 2021 at 8:01 pm	and the standard attachment Appendix 1-AMENDED Solar Farm Components put to Record Cool 21 9
Aug 17, 2021 at 8:02 pm	Pobert Harb added attachment Appendix2-AMENDED SWM Report and O&M.pdi to Record Codin 219
Aug 17, 2021 at 8:02 pm	D. book Leath added attachment Annendix3-Solar Facility O&M.pdf to Record CCSF-21-5
Aug 17, 2021 at 8:02 pm	
Aug 17, 2021 at 8:03 pm Aug 17, 2021 at 8:03 pm	Robert Harb added attachment Appendix5-AMENDED Electrical One-Line Diagram (139 Amesbury Line Harb Harb
Aug 17, 2021 at 6.00 pm	One I to Record (1.SP-21-9
Aug 17, 2021 at 8:03 pm	Robert Harb added attachment Appendix6-Solar Site Illustratives.pdf to Record CCSP-21-9
Aug 17, 2021 at 8:04 pm	Robert Harb added attachment Appendix7-Whittier School Sewer Plan.PDF to Record CCSP-21-9 Robert Harb added attachment Appendix7-Whittier School Sewer Plan.PDF to Record CCSP-21-9 Robert Harb added attachment Appendix7-Whittier School Sewer Plan.PDF to Record CCSP-21-9
Aug 17, 2021 at 8:04 pm	Robert Harb added attachment Appendix/ Whitele Costs Burnell Fire Department Cart Path Proposal pdf to Record Robert Harb added attachment Appendix8-AMENDED Haverhill Fire Department Cart Path Proposal pdf to Record CCSP-21-9
Aug 17, 2021 at 8:05 pm	Robert Harb added attachment Solar-2021.08.16 189 Amesbury Line Rd - Special Permit Comments and RESPONSES.docx to Record CCSP-21-9

Timeline

Hillemi	5					
Label		Status	Activated	Completed	Assignee	Due Date
Laber	Special Permit Filing Fee	Paid	Apr 15, 2021 at 8:03 pm	Apr 15, 2021 at 8:12 pm		-
∠	Planning Director Review	Complete	Apr 15. 2021 at 8:12 pm	Apr 16, 2021 at 11:07 am	William Pillsbury	-
.	Building Inspector Review	Complete	Apr 15, 2021 at 8:12 pm	May 12, 2021 at 10:54 am	Tom Bridgewater	•
.,	City Clerk Review - Hearing Dates Set	Complete	Apr 15, 2021 at 8:12 pm	May 18, 2021 at 8:13 am	LINDA KOUTOULAS	
.,	City Council Clerk Notified	Complete	May 18, 2021 at 8:13 am	May 18, 2021 at 8:13 am	LINDA KOUTOULAS	-
•	Assessor for Abutter's List	Skipped	May 18, 2021 at 8:13 am	May 18, 2021 at 8:13 am	LINDA KOUTOULAS	
_	Police Department Review	Complete	May 18, 2021 at 8:13 am	May 18, 2021 at 8:36 am	Robert Pistone	•
•	Fire2 Department Review	Complete	May 18, 2021 at 8:13 am	May 18, 2021 at 4:27 pm	Michael Picard	-
.,	Fire1 Department Review	Complete	May 18, 2021 at 8:13 am	May 25, 2021 at 3:53 pm	Eric Tarpy	•
*	Wastewater Review	Complete	May 18, 2021 at 8:13 am	May 27, 2021 at 10:29 am	Paul Jessel	•
*	Water Supply Review	Complete	May 18, 2021 at 8:13 am	May 27, 2021 at 1:47 pm	John D'Aoust	÷
.,	Water Department Review	Complete	May 18, 2021 at 8:13 am	Jun 1. 2021 at 4:41 pm	Glenn Smith	-
	Health Department Review	Complete	May 18, 2021 at 8:13 am	Jun 8, 2021 at 2:19 pm	Mark Tolman	
~	School Department Review	Complete	May 18, 2021 at 8:13 am	Jun 9, 2021 at 11:59 am	Mike Pfifferling	-
~	Conservation Department Review	Complete	May 18, 2021 at 8:13 am	Jun 11, 2021 at 12:47 pm	Robert Moore	-
~	Conservation Department (1975)			0:-1-1-		139%2

Label		Status	Activated	Completed	Assignee	Due Date
~	Storm Water Review	Complete	May 18, 2021 at 8:13 am	Jun 11, 2021 at 12:47 pm	Robert Moore	
~	DPW Review	Active	May 18, 2021 at 8:13 am	•	Mike Stankovich	•
*	Engineering Department Review	Active	May 18, 2021 at 8:13 am	• •	John Pettis	·
~	Planning Director Approval for Agenda	Pending	•	•	William Pillsbury	•
~	Building Inspector Approval for Agenda	Pending	-		Tom Bridgewater	·
~	First Ad Placement	Pending	-		LINDA KOUTOULAS	
~	Placed on Agenda	Pending	-		LINDA KOUTOULAS	
~	Abutter Notification	Pending	-	-	LINDA KOUTOULAS	-
~	Second Ad Placement	Pending	-	-	LINDA KOUTOULAS	-
~	City Councilor A Review	Pending		-	Melinda Barrett	
~	City Councilor B Review	Pending			Colin LePage	•
~	City Councilor C Review	Pending	-		Joe Bevilacqua	
~	City Councilor D Review	Pending		•	John Michitson	
~	City Councilor E Review	Pending	•		Thomas Sullivan	
Y	City Councilor F Review	Pending	-	-	Tim Jordan	
~	City Councilor G Review	Pending	-		Michael McGonagle	
~	City Councilor H Review	Pending	-		Mary Ellen Daly O'Brien	
~	City Councilor I Review	Pending	-		William Macek	
~	City Council Meeting	Pending	-		LINDA KOUTOULAS	-
~	Meeting Minutes & Decision Filed w/City Clerk	Pending		-		

ROBERT D. HARB

ATTORNEY AT LAW 17 WEST STREET HAVERHILL, MASSACHUSETTS 01830

TEL: (978) 373-5611 FAX: (978) 373-7441 EMAIL: bobharb@aol.com

Of Counsel
Alfred J. Cirome

April 8, 2021

City of Haverhill
City Council
4 Summer Street, Haverhill, MA 01830

RE: 139 Amesbury Line Road:

Application For Solar Energy System Special Permit and Water Supply Protection District (WSPD) Special Permit

Dear City Council:

On behalf of the Applicant and Lessee, Solar Smart LLC, application is hereby made for a Special Permit for Large Scale Ground Mounted Solar Energy System in accordance with the City Zoning Ordinance (see Sections 7.8 and following).

Application is also made for a Special Permit for the installation of this solar energy system within the Water Supply Protection District in accordance with the City Zoning Ordinance (See Section 9.2.7).

Reference is hereby made to all the Plans and Specifications filed with this Application as well as the written testimony of Kyle Burchard, P.E. also filed with this Application and incorporated herein by reference

Financial Surety for this Large Scale Ground Mounted Solar Energy System project has been reviewed with the Planning Director and will be filed if this Special permit is approved during the Appeal period.

Applicant, based upon the testimony, plans and evidence submitted herewith and supplemented at the Public Hearing, respectfully requests the City Council to make a written determination and find that:

- 1. The proposed use or structure(s) shall not cause substantial detriment to the neighborhood or the City, taking into account the characteristics of the site and of the proposal in relation to that site.
- 2. The grant of a special permit for a large-scale ground-mounted solar energy system will promote the highest and best use of the subject property, taking into account the characteristics of the

subject property, including past land uses, possible presence of hazardous materials, and other development limitations.

- 3. There are Community energy needs which are served by this Project.
- 4. There is safe traffic and pedestrian flow provided by this Project.
- 5. There are adequate utilities and other public services for this Project.
- 6. The Natural Environment will not be impacted.
- 7. There is no impact on City services and this project will increase the city tax base.

In addition to meeting the above, the Council can also find that the proposed use:

- 1. Satisfies the design and operations guidelines set forth in the Zoning Ordinance;
- 2. Is in harmony with the purposes and intent of this Section and will promote the purposes of the WSPD;
- 3. Is appropriate to the natural topography, soils, and other characteristics of the site to be developed;
- 4. Will not, during construction or thereafter, have an adverse environmental impact on any water body or watercourse in the district; and 5. Will not adversely affect the quality or quantity of an existing water supply.

The Applicant respectfully requests Council approval of both the Solar Energy System Special Permit and The Water Supply Protection District (WSPD) Special Permit.

Robert D. Harb, Attorney for Solar Smart LLC



Engineering Solutions for Land & Structures

April 8, 2021 AMENDED August 16, 2021

City of Haverhill City Council 4 Summer Street, Haverhill, MA 01830

139 Amesbury Line Road Solar Farm RE:

Application for Solar Energy Special Permit (§7.8.11) and Application for Water Supply Protection District (WSPD) Special Permit (§9.2.7)

Dear City Council:

On behalf of Solar Smart, LLC, the Applicant and Lessee, Goldsmith, Prest & Ringwall, Inc. (GPR) has compiled information below to support two special permit requests for the proposed 2 MW AC solar farm project at 139 Amesbury Line Road, City of Haverhill Assessors Property ID#430-11-12.

These special permit applications, including the plans and accompanying text, meet all the requirements to allow full evaluation of the proposed Large-Scale Ground-Mounted Solar Energy Use (hereinafter called the "Solar Lease Area") within the RS & RM Zoning Districts and within the City of Haverhill Water Supply Protection District (WSPD).

Introduction

The total land area of the subject property measures 26.81± acres, of which the proposed Solar Lease Area measures 18.40± 18.60± acres. Approximately 2,505 square feet of Jurisdictional wetlands present on the property shall not be altered and mitigated by wetland replication areas., and wWork within wetlands and wetland buffer zones shall be is documented in a Notice of Intent filing to the City of Haverhill Conservation Commission.

The Solar Lease Area partially straddles a natural drainage divide between the Merrimack River (to the east) and the Millvale Reservoir (to the west). This natural drainage divide also defines the limits of the City of Haverhill Water Supply Protection District (WSPD) for the Millvale Reservoir, as well as a zoning district line between the RS (Special Rural) and RM (Medium Density) residential zones. The WSPD and RS are one and the same over the Solar Lease Area. The WSPD also places a Zone 'A' Surface Water Supply Protection Area on the subject property, outside the Solar Lease Area. The remainder of the WSPD on the Solar Lease Area is considered Zone 'C' Surface Water Supply Protection Area, and all disturbances shall be documented in a Notice of Intent filing to the City of Haverhill Conservation Commission.

Goldsmith, Prest & Ringwall, Inc.

The solar energy facility is allowed in all districts by Special Permit, except the Waterfront District, as stipulated under City Ordinance Section 7.8.3.1. The project is not located in any portion of a Waterfront District.

Solar Energy Special Permit Request

City Ordinance Section 7.8.11 Special Permit Criteria for the Large-Scale Ground-Mounted Solar Energy Systems use states:

"In addition to any other criteria set forth in this Ordinance for the grant of a special permit, the SPGA shall consider whether the grant of a special permit for a Large-Scale Ground-Mounted Solar Energy System will promote the highest and best use of the subject property, taking into account the characteristics of the subject property, including past land uses, possible presence of hazardous materials, and other development limitations."

The proposed Solar Lease Area is currently forested, and slopes varying from 5% - 20% towards the Whittier School Driveway. The land is known to have been farmed in the past, and an old cart path and stone wall cuts generally east to west through the middle of the property, providing rough vehicular access and a scenic walking trail that has been used for several years.

The current WSPD overlay is built upon state code provisions in 314 CMR 4.00 Massachusetts Surface Water Quality Standards and 310 CMR 22.00 Drinking Water, in which there are numerous limitations on the installation of septic systems, animal farming, and uses of herbicides and pesticides, in order to protect and promote surface water quality. Test holes for drainage were dug, spaced across the Solar Lease Area, that identified relatively consistently shallow seasonal high groundwater depths.

Development options for the property are somewhat limited by the forementioned regulatory, topographic and subsurface groundwater constraints. Possible development options could include moderate-intensity organic farming, and limited residential development. These options, as well as leaving the land undeveloped, could comply with regulations and conform to the constraints of the land.

The proposed solar energy farm represents a highest and best use of the land within the various regulatory and physical constraints. The solar energy farm consists of construction materials and methods that produce no hazardous or toxic wastes or byproducts. At this location, a cooperative educational relationship is in development with Paul Moskevitz, the Vocational Technical Director of the Whittier Regional Vocational Technical School. The plan is to supply the school with access to weather and solar output data, along with access to resources for emerging technologies in energy systems engineering. Raised observation areas are proposed, along with a perimeter trail to maintain the old cart path walking connection. In addition to a WSPD compliant design, pollinator seeding areas are proposed and bee hives are to be installed to promote future generations of fruitful habitat in the area.

In a broader sense, our modern society that has been built on electrical infrastructure fueled by the combustion of fossil fuels, coal and natural gas, is sourcing other fuels, including solar. Local solar energy sources provide local power grids and end users with better options from distributed power generation. Improved battery technology to be employed at 139 Amesbury Line Road will also help buffer periods of peak power usage to add resilience to the local power grid. Over time, solar installations will provide renewable, distributed, redundant, and clean energy sources serving local communities directly.

Harnessing solar energy is a highest and best use for the land at 139 Amesbury Line Road, today and into the future, with the installation of mature solar technology, accompanied by the other proposed elements for environment and education.

Water Supply Protection District (WSPD) Special Permit Request

City of Haverhill Ordinance Section 9.2 Water Supply Protection District (WSPD) lists in Section 9.2.7 Uses Permitted by Special Permit, nine (9) articles describing qualified use categories which may be granted special permit by the City Council. The proposed solar energy facility qualifies for special permit under the fourth article, (Ordinance Section 9.2.7.4) which states:

"Any use otherwise permitted as of right or by special permit that requires a permit under the National Pollutant Discharge Elimination System permit program established pursuant to 33 U.S.C § 1342, the Surface Water Discharge Permit Program established pursuant to M.G.L. c.21, s.43, or the Groundwater Discharge Permit Program established pursuant to M.G.L. c. 21, s.43."

As the solar energy facility is allowed by special permit in all but the WD District (§7.8.11), and greater than 1 acre of proposed land disturbance triggers a National Point Discharge Elimination System (NPDES) with the U.S. Environmental Protection Agency (EPA) under a Construction General Permit Notice of Intent (CGP-NOI), Ordinance Section 9.2.7.4 allows the City Council to grant a WSPD Special Permit. The following is complete in all regards, meeting all the requirements of the City of Haverhill Ordinance to allow full evaluation of the proposed use on the Water Supply Protection District. The information is provided in sequence according to the numbering listed in the City of Haverhill Ordinance.

§9.2.8.1. Application. This Application has a list of all state, local and federal permits, licenses and approvals required for the proposed activity, and the status of all such permits, licenses and approvals:

<u>Status</u> Permit Applied Haverhill Solar Energy Special Permit Applied Haverhill WSPD Special Permit Haverhill Conservation Commission NOI Not Yet Applied Apply for Construction **EPA CGP-NOI Pending Selection** General Contractor License Apply for Construction **Building Permit** Apply for Construction **Electrical Permit**

§9.2.8.2. This application is prepared in accordance with the data requirements and BMPs of the proposed development (e.g., including but not limited to erosion and sedimentation control plan, stormwater requirements, septic system designs).

An updated Stormwater Management Report, Long-Term Pollution Prevention Plan and Stormwater O&M Plan prepared in accordance with the Massachusetts Stormwater Management Handbook, and in response to Peer Review comments to the Notice of Intent application, describing all BMP's is provided as attachment to this application. A Solar Facility O&M Manual is also provided as attachment. A complete updated site plan set is provided as attachment, to depict geometric layouts, grading, drainage, and erosion and sedimentation control plans and details.

§9.2.8.3. This application is required to include a complete list of chemicals, pesticides, fuels and other potentially hazardous materials to be used or stored on the premises in any quantity, however, there are none proposed with this project. The application shall include a Management Plan for the handling, storage and disposal of any materials identified.

Lithium-ion batteries used for energy storage and power transfer are proposed in fire-rated enclosures, with non-toxic fire suppression systems. Detailed technical information on these systems are included as attachment. No chemicals, pesticides, fuels or other potentially hazardous materials are proposed to be used or stored on the premises.

Electric transformers contain fluids for cooling. The transformers used on this project shall use Envirotemp™ 360 or FR3 fluid, which have the same general chemical composition as vegetable oil.

The proposed battery enclosures have a triple redundancy protection against failures. The modes of protection consist of:

- 1. The connex box itself is a sealed steel enclosure affixed to a concrete pad. The batteries are located inside the steel enclosure, protected from weather exposure.
- 2. An integrated cooling system and thermostat keeps the batteries from overheating.
- 3. The enclosure is equipped with a "FM-200™ Clean Agent Fire Suppression System" using the cleanest fire suppression technology available. A material safety data sheet for the active chemical, HFC-227ea is included in the appendix.

Should the cooling system fail, and the fire extinguishing system fail, any combustion of materials inside the steel connex container remains inside the container.

§9.2.8.4. This application includes an analysis by a professional Massachusetts licensed engineer experienced in groundwater evaluation to demonstrate that the proposed activity will not be detrimental to the purposes of this district as set forth in Section 9.2.1.

The proposed activity is not detrimental to the watershed to be protected.

The proposed solar panels, electrical equipment pads and gravel driveway do not generate TSS or other pollutants. The proposed drainage system provides stormwater recharge and peak flow attenuation in accordance with the standards of the Massachusetts Stormwater Management Handbook.

The site is within the watershed of the Millvale Reservoir. The existing ground surface within the project area is generally at a 15% slope draining towards the Whittier School driveway to the north. Roadside ditches along the Whittier School driveway capture runoff from the hillside and convey runoff under the road via three (3) concrete pipe culverts to a large wetland complex north of the driveway.

Two wetland areas on the subject property were flagged by wetland scientist Matthew S. Marro in September and October 2020. The third, larger wetland area on the north side of the Whittier School driveway was also flagged at this time. In July 2020, the Haverhill Conservation Commission hired a delineation consultant, Mary Rimmer of Rimmer Environmental Consulting, LTD who made changes and additions to the wetland delineation by Matthew Marro. The two consultants met and conferred on the delineation as shown on the Plan Amended 8/16/21, changing the shape of the two wetland areas and adding a third, isolated wetland area subject to the City of Haverhill Wetland Bylaw. Following the updated delineation, the project proposes wetland replication as mitigation for wetland impacts. The two primary wetland areas on the subject property form broad swales for conveyance of surface waters, and being at low points in the grade, these swales generally discharge into the drainage culverts under the Whittier School driveway. Some of the new delineated wetlands areas being impacted do not flow toward the Whittier driveway and are not in the WSPD.

On 1/8/2021 soil investigation of the property was conducted by Kyle Burchard, P.E., registered Massachusetts Soil Evaluator #14048. A series of drainage test pits were dug in several locations across the proposed development in order to identify estimated seasonal high groundwater elevations and existing soil conditions. Test hole logs are included in the Stormwater Management Report attached to this application. The seasonal high water table was identified fairly consistently at 27" below the ground surface according to mottles in the soil. The chroma in the strata below the estimated seasonal high groundwater was not significantly gleyed, indicating that the soils were typically saturated without a large amount of seasonal variation in the groundwater elevation that would tend to wash more of the chroma away. The soil profile and characteristics were consistent across the whole project area, being relatively shallow groundwater and a composition of sandy loam and loam.

The relatively shallow groundwater condition on the site, and the indication of nearly constant saturation supports the proposed site stormwater BMP strategy of minimal surface grading and no impervious pavement. Long, shallow-depth, and minimally-sloped grassed swales with check dams will be incised along the hillside to capture, slow, and promote runoff recharge to groundwater. The proposed shallow manipulation of surface soils achieves the minimum Massachusetts Stormwater Management Handbook Standards of matching predevelopment to post-development peak flows, maintaining existing groundwater recharge, and promoting water quality.

The drainage calculations for the grassed swales, conveyance channels and detention basins in the Stormwater Management Report show appropriate compensation for the change in land cover from forested to grassed hillside and gravel driveway conditions.

The Massachusetts Stormwater Handbook targets a neutral stormwater impact with various BMP's and the assortment of measures proposed achieve that.

§9.2.9. Design and Performance Standards.

At the time of this application, the proposed Solar Lease Area area is wooded with a gravel cart path crossing through it from east to west, bounded on the south side by a stone wall. Other various stone walls mark some of the boundaries of the subject property. Two wetland fingers reach into the property from culverts under the adjacent Whittier School driveway to the north. The only known former use of the property was as farmland. There are no known septic fields, and no known hazardous materials on the property.

Access from Amesbury Line Road provides both temporary construction access, and permanent facility access for routine maintenance of the solar facility. This driveway access provides Fire and EMS access as well. The gravel access driveway will also be maintained as needed for stable passage. The first 280 feet of driveway from Amesbury Line Road will be treated in an alternative manner so as to appear like an old cart path, but with a stable construction meeting the approval of the Haverhill Fire Department. During construction a secondary construction access has been secured by agreement with the abutting property owner of 235 Amesbury Line Road. This secondary access will reduce construction traffic passage on the primary access driveway.

§9.2.9.1 Safeguards.

Three (3) pad-mounted and enclosed lithium-ion battery banks are proposed with the project. These three (3) large batteries are equipped with automatically deployed gaseous firesuppression systems that suffocate any fire instantaneously without toxic residues.

Supports for the proposed solar panels consist of driven stainless-steel posts.

Buried wires and cabling are all waterproofed and insulated.

No toxic or hazardous materials or byproducts result from the solar farm installation.

§9,2.9.2. Location. The WSPD boundary onsite has been delineated by the natural drainage divide. Small deviations in the post-development drainage conditions are delineated on the drainage divide maps included with the Stormwater Management Report.

No toxic or hazardous discharges, nor septic discharges are proposed within the WSPD, or on the site.

§9.2.9.3. Disposal.

No onsite subsurface sewage disposal systems are proposed with this project.

§9.2.9.4. Stormwater.

The design of stormwater management measures conforms to the Massachusetts Stormwater Standards in all regards. See the Stormwater Management Report attached to this application.

The Applicant, based upon the testimony, plans and evidence submitted herewith and supplemented at the Public Hearing, respectfully requests that the City Council make a written determination and find that:

- 1. The proposed use or structure(s) shall not cause substantial detriment to the neighborhood or the City, taking into account the characteristics of the site and of the proposal in relation to that site.
- 2. There are Community energy needs which are served by this Project.
- 3. There is safe traffic and pedestrian flow provided by this Project.
- 4. There are adequate utilities and other public services for this Project.
- 5. The Natural Environment will not be impacted.
- 6. There is no impact on City services and this project will increase the city tax base.

In addition to meeting the above criteria set by Section 10.4.2, the Council can also find that the proposed use:

- 1. Satisfies the design and operations guidelines set forth in the Zoning Ordinance;
- 2. Is in harmony with the purposes and intent of this Section and will promote the purposes of the WSPD;
- 3. Is appropriate to the natural topography, soils, and other characteristics of the site to be developed;
- 4. Will not, during construction or thereafter, have an adverse environmental impact on any water body or watercourse in the district; and
- 5. Will not adversely affect the quality or quantity of an existing water supply.

The Applicant respectfully requests City Council approval of both the Solar Energy Special Permit and the Water Supply Protection District (WSPD) Special Permit.

Respectfully submitted,

Kyle Burchard, P.E.

Application Attachments:

Haverhill Solar Site Plan Set

Appendix 1- Solar Farm Components

Appendix 2- Stormwater Management Report and Operations & Maintenance Plan

Appendix 3- Solar Facility Operations & Maintenance Plan

Appendix 4- Construction Access Agreement

Appendix 5- Electrical One-Line Diagram

Appendix 6- Solar Site Illustratives

Appendix 7- Whittier School Sewer Plan

Copy to:

Theodore Xenakis, Esq. Solar Smart Development Robert D. Harb, Esq. **GPR file 181084**

Stormwater Management Report

Haverhill Solar Project 139 Amesbury Line Road Haverhill, MA

> April 2021 Revised August 2021

Submitted to:

City of Haverhill Department of Public Works City of Haverhill Conservation Commission 4 Summer Street Haverhill, MA 01830

Submitted by:

Solar Smart, LLC 1207 Congressional BLVD Summerville, SC 29483

Prepared by:

Goldsmith, Prest & Ringwall, Inc. 39 Main Street, Suite 301 Ayer, MA 01432

> <u>Project No:</u> 181084



Table of Contents

Section	Title
1	Introduction and Methodology
2	Hydrology Summary for 24-hour Storm
3	Mass DEP Stormwater Management Report Checklist
4	Appendix
	Mapped Soil Survey
	Soil Mapping Overlay and Testing Locus (24" x 36")
	Soil Suitability Assemssment for On-Site Solar Project - conducted January 8, 2021
	Flood Insurance Rate Map - Map No. 25009C0092F
	Pre-Development Watershed Map - Existing Conditions (24" x 36") Watershed Computations
	Post-Development Watershed Map - Developed Conditions (24" x 36") Watershed Computations Stormwater Quality Computations Groundwater Recharge Water Quality Retention Volume TSS Removal

Attachments: Haverhill Solar Project

"Site Plan- 139 Amesbury Line Road, Haverhill, MA" prepared for Solar Smart, Inc, Dated April 2021.

Long-Term Pollution Prevention Plan & Stormwater System Operation and Maintenance Plan, Dated April 2021.

Section 1 Introduction and Methodology

Introduction and Methodology

Regulatory Requirements and Design Intent

This narrative is intended to accompany the stormwater management report for the large scale ground mounted solar energy system known as the Haverhill Solar Project. Included in this report are calculations that support engineering design as required by the MassDEP Stormwater Management Handbook and applicable City of Haverhill Rules and Regulations. Site specific information is presented under two scenarios, "predevelopment" and "post-development" conditions, so that potential impacts due to the project can be identified, quantified and, as necessary, mitigated.

The final design intent seeks to meet the following interrelated goals:

- 1. Limit stormwater runoff rates for the 2, 10, and 100-year storms to existing (predevelopment) levels;
- 2. Provide adequate drainage for new surfaces;
- 3. Provide a cost-effective engineering solution that addresses regulatory as well as real-world constraints.

Existing Site Description

The subject property is shown on City of Haverhill Assessors Map 430, Block 11, Lot 12, and measures 26.81± acres. The property is generally bounded to the west by a private paved driveway serving the Whittier Regional Vocational Technical High School, to the north by Amesbury Line Road and residential properties, to the east by residential or farmed properties, and to the south by land holdings of the Whittier Regional Vocational Technical High School.

The subject site area is wholly contained within the subject property, and measures 18.40± acres. The subject site is referred to herein as the "Solar Lease Area" for the proposed installation of a Large-Scale Ground-Mounted Solar Energy System.

The Solar Lease Area partially straddles a natural drainage divide between the Merrimack River to the east, and the Millvale Reservoir to the west. This natural drainage divide also defines the limits of the City of Haverhill Water Supply Protection District (WSPD) for the Millvale Reservoir, as well as a zoning district line between the RS (Special Rural) and RM (Medium Density) residential zones. The WSPD and RS are one and the same over the Solar Lease Area. The WSPD also contains a Zone 'A' Surface Water Supply Protection Area on the subject property under definitions for public water supplies listed in 310 CMR 22.02 and is a Critical Area being addressed under the Massachusetts Stormwater Standard #6 herein. The Zone 'A' is outside the Solar Lease Area, and the remainder of the WSPD on the Solar Lease Area is defined as Zone 'C' Surface Water Supply Protection Area.

The subject property contains two (2) bordering vegetated wetland (BVW) areas, the westerly BVW being a long, finger-like wetland area projecting into the Solar Lease Area. After additional testing, the easterly BVW was determined to extend through the limits of the Solar Lease Area, within an area of proposed work, requiring minor alterations to the BVW. These two BVW areas occupy approximately 43,345 square feet on the overall subject property.

The subject property is mostly wooded with an existing single-family residence and driveway to the north, plus a separate gravel cart path trail crossing generally west-southwest to east-northeast through the property, along with several portions of stone walls. The existing house sits atop a rise in the landform with slopes as steep as 3:1 towards Amesbury Line Road, towards the Whittier School Driveway and to the easterly BVW. The Solar Lease Area that is covered by the WSPD generally drains westward towards the Whittier School driveway with relatively consistent land slopes between 10% and 20%. The Solar Lease Area outside the WSPD drains generally eastward with slopes between 1% and 8%. Relative high points in the topography at the western boundary of the Solar Lease Area also drain directly towards adjacent land owned by the Whittier School (Analysis Point #3 (AP-3)).

Analysis Point #1 (AP-1) is outside the WSPD, draining generally southeastward, ultimately towards the Merrimack River, a drainage area measuring 4.04± acres, consisting of both onsite areas and offsite areas passing through proposed BMP controls. The point of analysis is taken at the subject property line in common with the abutting property of Map 430 Block 11 Lot 12.

Analysis Point #2A (AP-2A) is entirely within the WSPD, and drains westward, ultimately towards the Millvale Reservoir, a drainage area measuring 16.63± acres, consisting of both onsite areas and offsite areas bypassing proposed BMP controls. The point of analysis is taken at one of the upstream headwalls/culverts for the Whittier School driveway, a 36" Reinforced Concrete Pipe (RCP).

Analysis Point #2B (AP-2B) is entirely within the WSPD, and drains westward, ultimately towards the Millvale Reservoir, a drainage area measuring 8.69± acres, consisting of both onsite areas and offsite areas bypassing proposed BMP controls. The point of analysis is taken at one of the upstream headwalls/culverts for the Whittier School driveway, a 24" Reinforced Concrete Pipe (RCP).

<u>Analysis Point #3 (AP-3)</u> is entirely within the WSPD, and drains south-southwesterly towards abutting lands owned by the Whittier School. The total drainage area measures 0.45± acres, not draining directly towards the Whittier School driveway.

Soil mapping from the Natural Resources Conservation Service (NRCS) indicates a small variety of soils generally confirmed by onsite soil testing. The NRCS lists Paxton Fine Sandy Loam, very stony on slopes varying from 8% to 35%, hydraulic soil group C, across the majority of the proposed Solar Lease Area and subject parcel. Deerfield

Loamy Fine Sand on 0% to 3% slopes, hydraulic group A is located in the northeast corner of the site along the driveway connection to Amesbury Line Road.

Site specific soil investigation consisted of a series of deep hole test pits, for drainage only, conducted on January 8, 2021 by a Certified Massachusetts Soil Evaluator. Soil logs of this investigation are included in the Appendix of this report, indicating fine sandy loam to loam soils and a typical seasonal high groundwater depth of 27-inches, corresponding to a hydrologic soil group C.

Project Description

The proposed project is to construct a 2± megawatt (MW) solar photovoltaic (PV) farm defined by the City of Haverhill Zoning Ordinance as a Large-Scale Ground-Mounted Solar Energy System consisting of 6,048 PV solar panels, supporting racking systems, chain link perimeter fencing and gates, with appurtenant wiring, conduits, inverters, transformers, battery storage units, secondary interconnection poles, buried and overhead electrical lines.

The proposed project also includes a gravel driveway for maintenance and emergency access with protective guardrail where appropriate, and numerous stormwater detention and conveyance BMP's as well as erosion and sediment control measures detailed on the Site Plan drawing set. Amenities also proposed include a restored trail connection across the property that is outside the fence line, educational observation platforms and kiosks, an apiary, several special seeding areas, and supplemental tree planting.

The proposed work includes all required electrical connections & equipment, wiring connections between the panels and inverters and transformer(s), some of which may be underground, and the interconnection of the entire array to the electrical grid via the existing pole and overhead power lines on Amesbury Line Road.

The solar panels will be installed above ground, and precipitation that lands on the panels will have the same opportunity to flow across permeable land to infiltrate in approximately the same distribution as it would in a pre-developed condition, by a series of distributed best management practices (BMP's) that clean and manage the runoff. The inherent increase of surface runoff due to changes in land cover is mitigated by the combination of BMP's that include a sediment forebay, grassed swales, conveyance channels, stone overflows, stone check dams, stone diaphragms, catch basins, outlet control structures and level spreader outlets.

Tree clearing is required to install the solar equipment, access driveway and BMP's, as well as to prevent shading of the panels. Total tree clearing on the subject site measures 14.6± acres, of which 13.7± acres will require removal of stumps, and 0.9±

acres within select BVW buffers will not be stumped or grubbed, as shown on the Site Plan drawing set. A total of 736 trees with 10" trunk diameter at breast height (DBH) or greater will be cut and of those, 693 stumps will be removed.

In the areas being stumped within the proposed solar panel arrays, topsoil stripping and surficial grading by raking or other mechanical processes will be performed to generally smooth the surface in preparation for the installation of numerous shallow (24"± deep) and flat (<0.5% longitudinal slope) grassed swales that shall provide the initial capture and detention storage of surface runoff.

When filled, the grass swales discharge over stone overflows into conveyance channels in which stone check dams will control flow velocities, sedimentation, and provide additional opportunities for groundwater recharge. The grass swales discharge to conveyance channels that discharge into two dry water quality swales (WQS's) with outlet control structures that allow for periodic inundation of the swales during higher rainfall events, affording an additional measure of stormwater detention. On the westerly side of the site, the grass swales and conveyance channels discharge to WQS #2 and on the easterly side of the site, the grass swales and conveyance channels discharge to WQS #1. A conveyance channel does discharge to WQS #3, however, no grass swales discharge to that particular conveyance channel. Additionally, each of these dry WQS's maintains a 2 foot separation between estimated high groundwater. Each WQS outlet control structure discharges concentrated flows through devices that mitigate flow energy and provide sheet flowing discharges. Each WQS also has a stone armored overflow spillway.

WQS's #1, #2 & #3 are located within the WSPD to manage WSPD critical area discharges. WQS #4 is outside the WSPD to manage non-WSPD discharges. WQS #4 primarily receives surface runoff from portions of the proposed gravel driveway. Unlike WQS's #1, #2 & #3, WQS #4 is proposed as a Wet Water Quality Swale and will be constructed at a minimum of 6" above the groundwater elevation.

WQS #4 has an outlet control structure discharging to a 12" perforated pipe within a 24" deep stone diaphragm, flush to grade, along the edge of a level portion of the driveway connection to Amesbury Line Road. This stone diaphragm provides another opportunity for recharge before activating surface discharge. WQS #4 also has a stone overflow towards the driveway, activated during the 100-year storm.

Steep topography along portions of the proposed driveway, and practical driveway slope limitations for emergency vehicles, result in cuts into existing grade greater than 27-inches that may seasonally intercept groundwater alongside portions of the driveway drainage ditches. Separate collection systems are proposed to convey and discharge such collected surface and/or groundwater flows at stable, riprap-armored, level spreader discharges to the easterly BVW.

All of the proposed grass swales, conveyance swales and Water Quality Swales are

graded such that they do not intercept the estimated seasonal high groundwater. None of the BMP's are lined or otherwise prohibit exfiltration for groundwater recharge, but no retention of volume for exfiltration is calculated. This provides a conservative calculation of managing stormwater peak flow discharges through the stormwater system.

No generators of total suspended solids (TSS) are proposed, and the only proposed impervious areas consist of 1,916± square feet of solar equipment pads and observation decks. A 1" water quality volume (WQV) over the impervious areas yields a total WQV= 160± cubic feet. Runoff from these few equipment pads is directed through a single sediment forebay in combination with a grassed swale to yield 50% TSS, then through WQS #1 to achieve 85% TSS removal prior to discharging to the critical area, Zone 'A' Surface Water Supply Area.

The WQV required is 160± cubic feet and the WQV provided in WQS#1 is 425± cubic feet. The total recharge volume required is 129± cubic feet, and the sum total of WQV provided in the proposed Water Quality Swales is 630± cubic feet.

In general, grading will result in smoothing of existing contours without significant cut to fill earthwork, or significant soil/gravel material haul-off or haul-in. The existing stone walls will not be sufficient for the driveway and various erosion control stone armoring, and other onsite sources of crushed stone are not anticipated such that crushed stone will need to be hauled onto the site.

Soil/slope stabilization will be accomplished by a variety of loam and seed, stone armoring, some slope stabilization treatments and use of geotextile fabrics as noted and detailed on the Site Plan drawing set.

Hydrologic and Hydraulic Computation Methodology

Runoff rates and volumes were computed using the Soil Conservation Service TR-55 Method entitled "Urban Hydrology for Small Watersheds". The following 24-hour rainfall events were analyzed:

Frequency (years): 2, 10, and 100

Northeast Regional Climate Center (NRCC) rainfall depths for each rainfall event were used for hydrologic and hydraulic analyses within Hydro-CAD version 10.10-4a.

The four analysis points described above (AP-1, AP-2A, AP-2B and AP-3) have been used to evaluate both pre-developed and post-developed peak discharge rates for the design storm frequencies. The hydraulic and hydrologic model accounted for proposed changes to land cover via tree removal, pad-mounted equipment, gravel driveway construction, time of concentration via grading changes, and the proposed stormwater BMP improvements.

Additional nodes were added to the post-development model to account for the driveway,

grassed swales, conveyance channels, water quality swales, and storm drainage piping, as depicted on the Watershed Maps and Diagrams provided herein.

Summary of Results

Surface Water Runoff

Tributary areas and peak rates of runoff for both conditions analyzed are displayed in the HYDROLOGY SUMMARY FOR 24-HOUR STORM that follows.

Compliance with Stormwater Management Standards

This project proposes nominal installation of impervious surfaces and an excess of water quality treatment measures in order to provide sufficient detention. This report seeks to show calculation of adequate treatment and peak runoff controls to demonstrate no proposed degradation to the existing wetland areas, critical areas or residential properties adjacent to the site. The following summary describes applicability of each Stormwater Standard, and compliance where required with the ten stormwater management standards as set forth on MassDEP "Checklist for Stormwater Report":

Standard 1: No New Untreated Discharges

The site proposes a sediment forebay in combination with a grassed swale and dry water quality swale to treat the limited new impervious equipment pads. The full treatment train path from these impervious equipment pads is; sediment forebay-grassed swale-stone overflow-conveyance swale-check dam-dry water quality swale-level spreader outlet.

Standard 2: Peak Rate Attenuation

Stormwater BMP's in the form of grassed swales, stone overflows, conveyance channels, check dams and dry water quality swales provide detention to attenuate peak rate discharges. At each analysis point, post-development peak rates of runoff are the same or less than predevelopment for all storms analyzed.

Standard 3: Recharge

All panels are elevated on support frames above permeable ground. Each support frame has several support posts driven directly into the ground without excavation for footings. Each row of solar panels is also separated from adjacent rows and each panel within the row is separated from adjacent panels resulting in a varied flow distribution of the panel runoff, not simply at the lowest edge of the panel row. Grassed swales are skewed to the alignment of the panel rows providing additional varied distribution of the runoff. Rainfall hitting the panels will be able to splash and flow off onto the ground where the runoff is then afforded multiple pervious vegetated catchments to infiltrate and recharge to groundwater.

Standard 4: Water Quality

Water quality retention (first flush = 1.0") is required for the proposed 1,916± square feet of proposed impervious equipment pads & observation decks. Total Suspended Solid (TSS) treatment is provided via a sediment forebay and grassed swale combination that then flows through a water quality swale to achieve the minimum 80% TSS required for discharge into a critical area.

Standard 5: Land Uses With Higher Pollutant Loads *Not applicable.*

Standard 6: Critical Area Discharges

Areas of the project site, including various outlets, discharge to a Zone 'A' Surface Water Supply Protection Area, and this is done to maintain existing flow patterns. The distributed points of discharge are at the end of a series of pervious detention and conveyance measures with multiple check dams and stone overflows acting as filters and energy dissipators. The points of discharge themselves are structural, armored level spreaders that reestablish sheet flow with energy dissipation at the outlet.

- Standard 7: Redevelopments and Other Projects Applicable to the Standards Only to The Maximum Extent Practicable

 This project is not a redevelopment project, and meets all applicable Standards as described hereon.
- Standard 8: Construction Period Pollution Prevention and Erosion & Sediment Control Measures for protecting the resource areas from construction period erosion and sediment are shown on the Permit Plans included with this report. The project shall be covered by a NPDES Construction General Permit but no SWPPP has been submitted. A SWPPP will be submitted as part of the NPDES Construction General Permit filing, no less than two weeks before land disturbance begins.
- Standard 9: Operation & Maintenance Plan

 An Operation and Maintenance Plan is attached.
- Standard 10: Prohibition of Illicit Discharges

 No Illicit Discharge Compliance Statement is attached but will be submitted prior to the discharge of any stormwater to post-construction BMPs.

Conclusion

The proposed BMP's provide adequate and appropriate stormwater detention and retention to compensate for the project's change in land cover from woods/brush to grass and gravel, and to mitigate the development's effects on runoff.

Further, the hydrologic drainage analysis of the project at three (3) analysis points show that peak runoff discharges from the project will be equal to or less than that which is discharged in the existing condition. Water quality treatment is provided as required, and appropriate mitigation for critical area discharges is provided. The project presents no degradation to the resource areas or abutting properties, and meets the applicable standards set forth in the MassDEP Stormwater Management Handbook, as detailed herein.

Section 2

Hydrology Summary for 24-hour Storm

HYDROLOGY SUMMARY FOR 24-HOUR STORM

139 Amesbury Line Road Haverhill, MA Project No. 181084

PEAK DISCHARGE RATE

Pre-Development (cfs)

Lte-Develobment (cis) =			100 100
Analysis Point	2-YR	10-YR	100-YR
AP-1	1.6	4.3	12.2
AP-2A	6.2	16.3	45.8
AP-2B	5.3	13.5	37.5
	0.3	0.7	2.1
AP-3		0.1	<u>. </u>

Development (cfs)

Development (cis)			100.10
Analysis Point	2-YR	10-YR	100-YR
AP-1	1.6	4.2	12.2
AP-2A	6.0	15.8	45.7
AP-2B	5.2	12.5	32.9
	0.3	0.7	2.0
AP-3			

Pre-Development vs. Developed (cfs)

Analysis Point	2-YR	10-YR	100-YR
AP-1	0.0	-0.1	0.0
AP-2A	-0.2	-0.5	-0.1
AP-2B	-0.1	-1.0	-4.6
AP-3	0.0	0.0	-0.1

PEAK DISCHARGE VOLUME

Pre-Development (Cubic feet)

Pre-Development (Capic rect)			
Analysis Point	2-YR	10-YR	100-YR
AP-1	9.688	23,168	64,033
AP-2A	35,778	85,567	236,495
AP-2B	42.086	98,686	268,207
AF-2B AP-3	1.414	3,381	9,344
AP-3	1,-11-		

Development (Cubic feet)

Development (Cubic feet	;)		
Analysis Point	2-YR	10-YR	100-YR
AP-1	12,127	26,704	68,803
AP-2A	39,261	94,660	319,974
AP-2B	28,490	64,353	169,316
7.11	1.401	3,284	8.925
AP-3	1,401	0,20.	

Pre-Development vs. Developed (Cubic feet)

10-YR 3,536 9,093	100-YR 4,770 83,479
	
0.003	02 470
9,093	03,479
-34,333	-98,891
	-419
	-34,333

Section 3

Mass DEP Stormwater Management Report Checklist



Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key





A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals. 1 This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 82
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

Checklist for Stormwater Report

B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature

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8/16/21

Checklist

Pro rede	ject Type: Is the application for new development, redevelopment, or a mix of new and evelopment?
	New development
	Redevelopment
	Mix of New Development and Redevelopment



Checklist for Stormwater Report

Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

No disturbance to any Wetl ■	
Site Design Practices (e.g.	clustered development, reduced frontage setbacks)
Reduced Impervious Area	(Redevelopment Only)
☐ Minimizing disturbance to €	existing trees and shrubs
☐ LID Site Design Credit Red	quested:
Credit 1	
Credit 2	
Credit 3	
□ Use of "country drainage"	versus curb and gutter conveyance and pipe
☐ Bioretention Cells (include	es Rain Gardens)
Constructed Stormwater	Wetlands (includes Gravel Wetlands designs)
☐ Treebox Filter	
Green Roof	
Other (describe):	Stone Diaphragm retention/recharge
Standard 1: No New Untrea	ated Discharges
No new untreated discha	arges
0	ned so there is no erosion or scour to wetlands and waters of the
Supporting calculations	specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Checklist for Stormwater Report

Ch	ecklist (continued)
Stan	ndard 2: Peak Rate Attenuation
	Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding. Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.
	Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24-hour storm.
Sta	ndard 3: Recharge
\boxtimes	Soil Analysis provided.
\boxtimes	Required Recharge Volume calculation provided.
	Required Recharge volume reduced through use of the LID site Design Credits.
\boxtimes	Sizing the infiltration, BMPs is based on the following method: Check the method used.
	Runoff from all impervious areas at the site discharging to the infiltration BMP.
	Runoff from all impervious areas at the site is <i>not</i> discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.
	Recharge BMPs have been sized to infiltrate the Required Recharge Volume.
	Recharge BMPs have been sized to infiltrate the Required Recharge Volume <i>only</i> to the maximum extent practicable for the following reason:
	Site is comprised solely of C and D soils and/or bedrock at the land surface
	M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
	Solid Waste Landfill pursuant to 310 CMR 19.000
	Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
\triangleright	
	☐ Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.
1	80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Checklist for Stormwater Report

Checklist (continued)
Standard 3: Recharge (continued)
The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
□ Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.
Standard 4: Water Quality
The Long-Term Pollution Prevention Plan typically includes the following: Good housekeeping practices; Provisions for storing materials and waste products inside or under cover; Vehicle washing controls; Requirements for routine inspections and maintenance of stormwater BMPs; Spill prevention and response plans; Provisions for maintenance of lawns, gardens, and other landscaped areas; Requirements for storage and use of fertilizers, herbicides, and pesticides; Pet waste management provisions; Provisions for operation and management of septic systems; Provisions for solid waste management; Snow disposal and plowing plans relative to Wetland Resource Areas; Winter Road Salt and/or Sand Use and Storage restrictions; Street sweeping schedules; Provisions for prevention of illicit discharges to the stormwater management system; Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL; Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan; List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
 A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent. Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
is within the Zone II or Interim Wellhead Protection Area
is near or to other critical areas
is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
involves runoff from land uses with higher potential pollutant loads.
☐ The Required Water Quality Volume is reduced through use of the LID site Design Credits.
Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Checklist for Stormwater Report

Checklist (continued)
Standard 4: Water Quality (continued)
The BMP is sized (and calculations provided) based on:
∑ The ½" or 1" Water Quality Volume or
The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
 The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior</i> to the discharge of stormwater to the post-construction stormwater BMPs.
★ The NPDES Multi-Sector General Permit does not cover the land use.
LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
□ The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.
Standard 6: Critical Areas
The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.



Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

Checklist for Stormwater Report

Checklist (continued)

Oncon	the service the maximum
extent pr	d 7: Redevelopments and Other Projects Subject to the Standards only to the maximum racticable project is subject to the Stormwater Management Standards only to the maximum Extent ticable as a:
☐ S F ☐ S with ☐ N	Limited Project Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area. Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development a discharge to a critical area Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff Bike Path and/or Foot Path
Cert expl The imp in V the	Redevelopment Project Redevelopment portion of mix of new and redevelopment. Itain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an elanation of why these standards are not met is contained in the Stormwater Report. Itain project involves redevelopment and a description of all measures that have been taken to project involves redevelopment and a description of all measures that have been taken to prove existing conditions is provided in the Stormwater Report. The redevelopment checklist found follows 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment of structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) proves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- ☑ A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



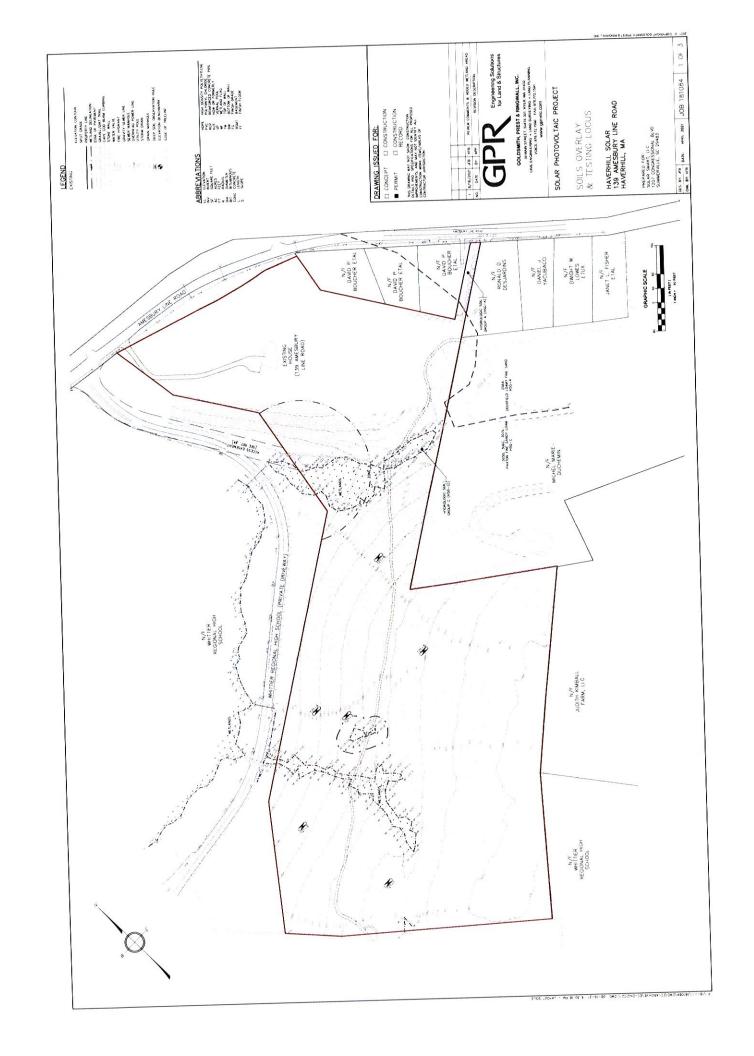
Checklist for Stormwater Report

Checklist (continued)

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)
The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has <i>not</i> been included in the Stormwater Report but will be submitted <i>before</i> land disturbance begins.
☐ The project is not covered by a NPDES Construction General Permit.
☐ The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the
Stormwater Report. The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.
Standard 9: Operation and Maintenance Plan
☐ The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
Name of the stormwater management system owners;
□ Party responsible for operation and maintenance;
Schedule for implementation of routine and non-routine maintenance tasks;
☑ Plan showing the location of all stormwater BMPs maintenance access areas;
□ Description and delineation of public safety features;
⊠ Estimated operation and maintenance budget; and
Operation and Maintenance Log Form.
The responsible party is not the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.
Standard 10: Prohibition of Illicit Discharges
An Illicit Discharge Compliance Statement is attached;
NO Illicit Discharge Compliance Statement is attached but will be submitted <i>prior to</i> the discharge of any stormwater to post-construction BMPs.

Section 4

Appendix





USDA

Natural Resources Conservation Service

Natural Resources Conservation Service USDA

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause line placement. The maps do not show the small areas of scale.

Please rely on the bar scale on each map sheet for map measurements.

Special Line Features

Very Stony Spot

Soils

Wet Spot Other

Stony Spot Spoil Area

MAP LEGEND

Streams and Canals

9

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Source of Map: Natural Resources Conservation Service Web Soil Survey URL

Coordinate System: Web Mercator (EPSG:3857)

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certifled data as of the version date(s) listed below.

Aerial Photography

-:

0

Soil Survey Area: Essex County, Massachusetts, Northern Part Survey Area Data: Version 16, Jun 9, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Aug 28, 2019—Sep

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

77

Severely Eroded Spot

Saline Spot Sandy Spot Slide or Slip

Sinkhole

Sodic Spot

Water Features Transportation Background W 8 0 ŧ Soil Map Unit Polygons Miscellaneous Water Area of Interest (AOI) Soil Map Unit Points Soil Map Unit Lines Closed Depression Marsh or swamp Perennial Water Mine or Quarry Rock Outcrop Gravelly Spot Special Point Features Borrow Pit Gravel Pit Lava Flow Clay Spot Area of Interest (AOI) Blowout Landfill

Interstate Highways

Rails

Major Roads Local Roads

US Routes



Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
	Water	0.1	0.0%
A	Scarboro mucky fine sandy loam, 0 to 3 percent slopes	1.8	0.5%
1A	Swansea muck, 0 to 1 percent slopes	3.2	0.9%
2A	Freetown muck, 0 to 1 percent slopes	44.7	12.9%
0A	Ridgebury fine sandy loam, 0 to 3 percent slopes	2.0	0.6%
53A	Hinckley loamy sand, 0 to 3 percent slopes	3.0	0.9%
53B	Hinckley loamy sand, 3 to 8 percent slopes	3.5	1.0%
53C	Hinckley loamy sand, 8 to 15 percent slopes	9.4	2.7%
55A	Windsor loamy sand, 0 to 3 percent slopes	5.4	1.6%
55B	Windsor loamy sand, 3 to 8 percent slopes	34.6	10.0%
56A	Deerfield loamy fine sand, 0 to 3 percent slopes	41.9	12.1%
05B	Paxton fine sandy loam, 3 to 8 percent slopes	11.0	3.2%
05C	Paxton fine sandy loam, 8 to 15 percent slopes	13.7	4.0%
05D	Paxton fine sandy loam, 15 to 25 percent slopes	40.8	11.8%
06B	Paxton fine sandy loam, 0 to 8 percent slopes, very stony	16.7	4.8%
06C	Paxton fine sandy loam, 8 to 15 percent slopes, very stony	21.6	6.2%
06D	Paxton fine sandy loam, 15 to 25 percent slopes, very stony	10.7	3.1%
07E	Paxton fine sandy loam, 25 to 35 percent slopes, extremely stony	35.0	10.1%
10B	Woodbridge fine sandy loam, 3 to 8 percent slopes	9.9	2.9%
10C	Woodbridge fine sandy loam, 8 to 15 percent slopes	6.5	1.9%
11B	Woodbridge fine sandy loam, 0 to 8 percent slopes, very stony	14.5	4.2%

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
405B	Charlton fine sandy loam, 3 to 8 percent slopes	5.0	1.4%
600	Pits, gravel	11.1	3.2%
651	Udorthents, smoothed	0.0	0.0%
711C	Charlton-Rock outcrop-Hollis complex, 8 to 15 percent slopes	0.5	0.2%
Totals for Area of Interest		346.5	100.0%

No.	181084	Date: 1 8 21
		*

Commonwealth of Massachusetts Haverhill Massachusetts

Soil Suitability Assessment for On-Site Solar Project

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-	Kyle Burchard, PE	, GPR	the section and section to the section of the secti	Date: 3/17/21	
Witnessed by:					
Location Addre	ess:		Applica	nt's Narr Solar Smart, LLC	(1)
or Lot No.	139 Amesbury Lin	e Road	Address	C	
	Haverhill, MA			Summerville, SC	29483
	(235 Amesbury Li	ne Road - Access)			
			Telepho	ne No.	
New Construct	ion 🗹 Upgr	ade 🔲 Rep	air 🗖		
Office Review					
	Survey Available:	No 🔲 Y	es 🗹		
Year Published		Publication Scal	le n	a Soil Map Unit	305D/306C
Soil Name	Paxton Fine Sandy Loan	Soil Limitations		Depth to restrictive feature	es, well drained
Soil Name		Soil Limitations	;	- · · · · · · · · · · · · · · · · · · ·	
Soil Name	_	Soil Limitations		_	
Surficial Geological	gic Report Available:	No 🗹 Yes			
Year Published	I MASS GIS P	ublication Scale			
Geologic Mate	rial(Map Unit)	Ice Contact Outw	ash		
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Current Water	Resource Conditions	s (USGS): Month	March		
Range: Above	<u>:</u> _		ormal 🔲	हार्चु क्षेत्रकृत नेतृत्ति कृतिक ती कर सामा सामाना सामाना सामाना सम्बद्धान्त कर हुन के तेत्र की तीव किसाना साम	an mannan newseren e-nedededelen-de
Other Referen					
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Location Address or Lot #: 139 Amesbury Line Road

Haverhill, MA

(235 Amesbury Line Road - Access)

Deep Hole #:	121-1	Date:	01/08/21 Tim	e:	9:30 AM	. Weather:	Clear 30°
Location (identif	y on site p	lan)	See Attached S	Sketch		gan degree to the anglement in this international materials and experience of the first in the	
Land Use Wooded			Slope (%)	2%-4%	handa ta and Halland	Surfaces Stones	Some Stones
(eg woodland, ag	ricultural	field, va	acant lot etc)				
Vegatation Mixe	d Forest, N	Mostly	Deciduous Upla	ınd			
Landform Kam	e Terrace						
Position on lands	cape	See a	ttached Sketch				
Distances from:							
Open ^v	Water Body	y >100	feet Dra	inage Way	100+	feet	
Possibl	e Wet Are	a >100	feet Prop	perty Line	100±	feet	
Drinking	Water Wel	1 >100	feet Oth	er:			
						feet	
Drinking	Water Wel	1 >100	feet Oth	er:		feet	

Deep Observation Hole Log							
Hole # 121	-1	NB			Suface El. 181.9		
Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (MUNSELL)	Soil Mottling	Other (Stucture, Stones, Boulders, Consistency, % Gravel)		
0-11 11-28 28-96	A B C	sl sl sl	10YR 3/3 10YR 3/4 2.5YR 4/3	-	myfr, most roots stop, 5% cobbles myfr 10% stones		

Parent Material (geologic) Ice Contact Outwash	Depth to Bedrock: >96"			
Depth to Groundwater: Standing Water in the Hole	n/a	Weeping from Pit Face: 64"		
Estimated Seasonal High Groundwater in the Hole	28"	Named on safety		
Aditional Notes		and a second back back the street and a second seco		
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Location Address or Lot #: 139 Amesbury Line Road

Haverhill, MA

(235 Amesbury Line Road - Access)

2 Date:	01.08.21 Tim	e:	11:00 AM	Weather:	Clear 32°
te plan)	See Attached S	Sketch			
	Slope (%)	lope (%) 2%-4% Surt			Some Stones
ral field, va	cant lot etc)				
st, Mostly I	Deciduous Upla	ınd			
ce					
See at	tached Sketch				
3ody >100	feet Drai	inage Way	/ 100± 1	Peet	
Area >100	feet Prop	erty Line	80± 1	Ceet	
Well >100	feet Oth	er:			
			!	l'eet	
	ral field, va st, Mostly L ce See at Body >100 Area >100	te plan) See Attached S Slope (%) ral field, vacant lot etc) st, Mostly Deciduous Uplace See attached Sketch Body >100 feet Area >100 feet Proj	Slope (%) 2%-4% ral field, vacant lot etc) st, Mostly Deciduous Upland ce See attached Sketch Body >100 feet Drainage Way Area >100 feet Property Line	te plan) See Attached Sketch Slope (%) 2%-4% ral field, vacant lot etc) st, Mostly Deciduous Upland ce See attached Sketch Body >100 feet Drainage Way Area >100 feet Property Line 80± 1 Well >100 feet Other:	te plan) See Attached Sketch Slope (%) 2%-4% Surfaces Stones ral field, vacant lot etc) st, Mostly Deciduous Upland ce See attached Sketch Body >100 feet Drainage Way 100± feet Area >100 feet Property Line 80± feet

Deep Observation Hole Log							
Hole # 121	-2	NB		<u> </u>	Suface El. 146.1		
Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (MUNSELL)	Soil Mottling	Other (Stucture, Stones, Boulders, Consistency, % Gravel)		
0-10 10-29 29-92	A B C	sl sl sl	10YR 3 3 10YR 4 6 2.5YR 5/4	(ä: 27°	myfr, 5-10% cobbles myfr, roots stop, 5-10% cobbles		

Parent Material (geologic) Ice Contact Outwash	Depth to Bedrock: >92"			
Depth to Groundwater: Standing Water in the Hole	92"	Weeping from Pit Face: 38"		
Estimated Seasonal High Groundwater in the Hole	27"			
Aditional Notes	I L B. HILL HOPE THE P. CO. CO. CO. CO. CO. CO. CO. CO. CO. CO			
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THE REPORT OF THE PROPERTY OF	off it was deferred degree in minimization in an in-	r these is saigligh description on a million of the million of the conference of a minimum of the conference of the conf		

Location Address or Lot #: 139 Amesbury Line Road

Haverhill, MA

(235 Amesbury Line Road - Access)

Deep Hole #:	121-3	Date:	01/08/21 Time	::	12:00 PM	Weather:	Clear 34°
Location (identif	y on site p	lan)	See Attached SI	ketch			
Land Use Wooded			Slope (%)	2%-4%		Surfaces Stones	Some Stones
(eg woodland, ag	ricultural	ield, va	acant lot etc)				
Vegatation Mixe	d Forest, N	Aostly I	Deciduous Uplai	nd			
Landform Kam	e Terrace						
Position on lands	cape	See a	ttached Sketch				
Distances from:							
Open V	Water Bod	y >100	feet Drain	iage Way	100±	feet	
Possibl	e Wet Area	a >100	feet Prop	erty Line	100±	feet	
Drinking	Water Wel	1 >100	feet Othe	r:			
			,			feet	

Deep Observation Hole Log									
Hole # 121	-3	NB			Suface El. 152.9				
Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (MUNSELL)	Soil Mottling	Other (Stucture, Stones, Boulders Consistency, % Gravel)				
0-10 10-28 28-72	A B C	sl sl sl	10YR 3-3 10YR 4-6 2.5YR 5/4	@ 27"	myfr, roots stop, 5-10% pebbles myfr, 20% cobbles				

Parent Material (geologic)	Depth to Bedrock: >72"				
Depth to Groundwater: Standing Water in the Hole	72"	Weeping from Pit Face: 27"			
Estimated Seasonal High Groundwater in the Hole	27"				
Aditional Notes	** H*H*** H *HH *** H* H H H H * H * H				
	ye nan wang approximen rang wang bayadjahanin opi dada bila				
	port sp. sp. sp. st. sp. sp. sp. sp. sp. sp. sp. sp. sp. sp	an arman masan masan mara unasan masan masan masan masan masan masan masan masan da sabib paba, paba			

Location Address or Lot #: 139 Amesbury Line Road

Haverhill, MA

(235 Amesbury Line Road - Access)

Deep Hole #:	121-4 Dat	e: 01/08/21 Tim	e:	1:00 PM	Weather:	Clear 36°
Location (identify	on site plan)	See Attached S	ketch			
Land Use Wood	led	Slope (%)	Slope (%) 2%-4% Surfaces Stone			
(eg woodland, agi	ricultural field,	vacant lot etc)				
Vegatation Mixed	d Forest, Mostl	Deciduous Upla	nd			
Landform Kame	Terrace		•			
Position on landso	cape See	attached Sketch				
Distances from:						
Open W	Vater Body >10	0 feet Drai	nage Way	100±	feet	
Possible	e Wet Area ≥10	0 feet Prop	erty Line	80±	feet	
Drinking V	Vater Well >10	0 feet Othe	er:			
					fect	

Deep Observation Hole Log									
Hole # 121	-4	NB			Suface El. 138.1				
Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (MUNSELL)	Soil Mottling	Other (Stucture, Stones, Boulders, Consistency, % Gravel)				
0-10 10-24 24-100	A B C	sl sl Is	10YR 3-3 10YR 4-6 10YR 5-1		mvfr mvfr, 5% pebbles 20% cobbles				

Parent Material (geologic)	Depth to Bedrock: >100"				
Depth to Groundwater: Standing Water in the Hole	n a	Weeping from Pit Face: 27"			
Estimated Seasonal High Groundwater in the Hole	25"	10 T = 101 00 T T T T T T T T T T T T T T T T			
Aditional Notes					
	मा मा मामास्यस्य महामा नास्य ज्यान पञ्चन ज्यान विद्यान है ।				
այս արգարգության փորժերը մրջակ ը փոստիգորիսի փոխիսի չեւ երի հետ են անդանական այս այս արաս արասարարան այլ այս այս		, Madelline, Marcellate, Marcellate, July Johnson, ի վերի վայի իրկրությունը արդագույթ արդարի արդարի արարարի արա			

Location Address or Lot #: 139 Amesbury Line Road

Haverhill, MA

(235 Amesbury Line Road - Access)

Deep Hole 1	t: 121-5	Date:	01 08 21	Time:	i	:50 PM	Weather:	Clear 36°
Location (id	entify on site p	lan)	See Attac	hed Sketcl	h			
Land Use Wooded			Slope (%) 2%-4%		6-4%		Surfaces Stones	Some Stones
eg woodlan	ıd, agricultural	field, va	icant lot et	c)				
Vegatation	Mixed Forest,	Mostly I	Deciduous	Upland				
Landform	Kame Terrace							
Position on	landscape	See a	ttached Sk	etch				
Distances fr	om:							
O	pen Water Bod	y >100	feet	Drainage	Way	100±	feet	
Po	ssible Wet Are	a >100	feet	Property	Line	100±	feet	
Drinl	king Water We	II >100	feet	Other:				
							feet	

	Deep Observation Hole Log										
Hole # 121-	-5	NB	***		Suface El. 179.5						
Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (MUNSELL)	Soil Mottling	Other (Stucture, Stones, Boulders, Consistency, % Gravel)						
0-9 9-30 30-112	A B C	1 1 1	10YR 3 4 10YR 4 6 10YR 7 1	(a ² 27" 10% 2.5YR 4-6	myfr 5% cobbles						

Parent Material (geologic) Ice Contact Outwash	Depth to Bedrock: >112"				
Depth to Groundwater: Standing Water in the Hole	n a	Weeping from Pit Face: 50"			
Estimated Seasonal High Groundwater in the Hole	27"				
Aditional Notes		ALL ARM O ARM OF A BANGE OF AN OFFICE AND AND AN AND AND AND AND AND AND AND			
According to the second	raasaajiimaiiimmi tama iliimiirii.				
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Location Address or Lot #: 139 Amesbury Line Road

Haverhill, MA

(235 Amesbury Line Road - Access)

Deep Hole	#:	121-6	Date:	01 08 21 Tim	ie:	2:30 PM	Weather:	Clear 38°
Location (i	identify o	n site pla	in)	See Attached S	Sketch			
Land Use	Wooded			Slope (%)	2%-4%	100 mm 11 200 mm 11 201 201 100 100 11 11 11 11 11 11 11 11 11 11	Surfaces Stones	Some Stones
(eg woodla	ınd, agric	ultural fi	eld, va	cant lot etc)				
Vegatation	Mixed F	orest, M	ostly I	Deciduous Upla	and			
Landform	Kame T	errace						
Position on	ı landscar	ie .	See at	ttached Sketch				
Distances f	from:							
(Open Wat	er Body	>100	feet Dra	inage Way	100± f	eet	
P	ossible W	et Area	>100	feet Prop	erty Line	100± f	eet	
Drir	nking Wa	ter Well	>100	feet Oth	er:			
						f	eet	

	Deep Observation Hole Log									
Hole # 121-	-6	NB			Suface El. 147.3					
Depth from Surface (inches)	Soil Horizon	Soil Texture (USDA)	Soil Color (MUNSELL)	Soil Mottling	Other (Stucture, Stones, Boulders, Consistency, % Gravel)					
0-12 12-30 30-	A B C	1 1 1	10YR 3 3 10YR 4 6 2.5Y 4/4	- (& 28" 10% 10YR 7/1 2.5YR 4 6	mvfr. 5% cobbles					

Parent Material (geologic) Ice Contact Outwash	Depth to Bedrock: >"				
Depth to Groundwater: Standing Water in the Hole	n a	Weeping from Pit Face: 38"			
Estimated Seasonal High Groundwater in the Hole	28"				
Aditional Notes	9 941 F R9RFF - LYSHIR RSG R REG R R A	110.0 % 0.0 M. W. 110.0 M. 110			
	er er er er er en skallen in de skallen er				
оонд тамент и от темпетина и от темпетина и принция и принция и и и и и и и и и и и и и и и и и и	distriction of Aphilonomera specificacy and programmy company pro-	HTEPETTERT PROTESTER PROTESTER STATES OF THE SECOND			

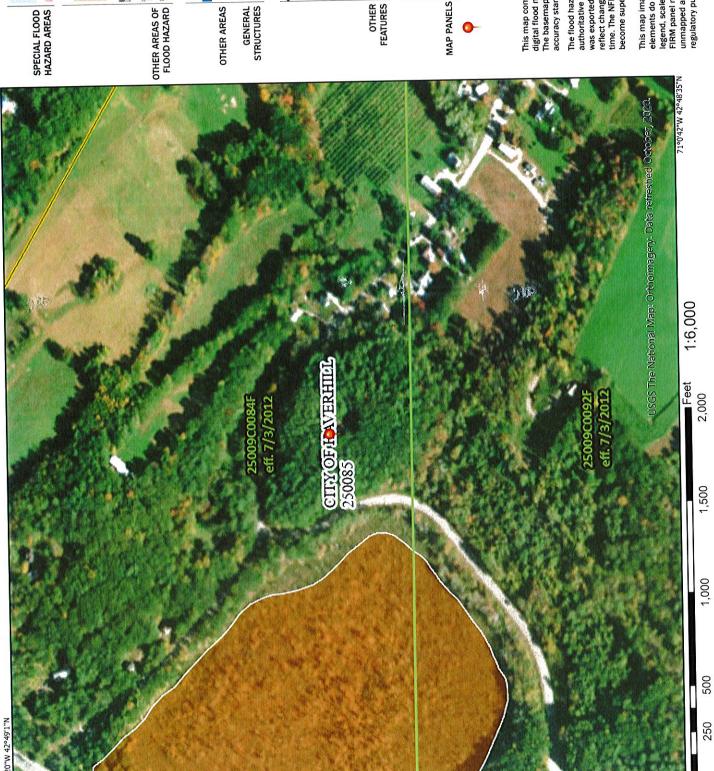
Location Address or Lot#: 139 Amesbury Line Road Haverhill, MA

Determination for Seasonal High Water Table

Method	Used:	
	Depth observed standing in observation hole inches Depth weeping from side of observation hole inches Depth to soil mottles * inches See individual Reports Ground water adjustment feet	
Index We	ll Number Reading Date Index Well Level	the little state of the second second second second second second second second
Adjustme	nt FactorAdjusted Ground Water Level	•
Depth of 1	Naturally Occuring Pervious Material	
	Does at least four feet of naturally occurring pervious material exist in all areas observed throughout the area proposed for the soil absorption system?	Yes
	If not, what is the depth of naturally occuring pervious material?	Feet
Certification	<u>on</u>	
Notes:	I certify that I am currently approved by the Department of Environmental Prot pursuant to 310 CMR 15.017 to conduct soil evaluations and that the above and has been performed by me consistent with the training, expertise and experienc in 310 CMR 15.017. I further certify that the results of my soil evaluation, as in on the attached soil evaluation form, are accurate and in accordance with 310 C 15.100 through 15.107. Signature Date 4/8	llysis e described dicated,

National Flood Hazard Layer FIRMette





Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

With BFE or Depth Zone AE, AO, AH, VE, AR

Regulatory Floodway

Without Base Flood Elevation (BFE)

0.2% Annual Chance Flood Hazard, Areas depth less than one foot or with drainage of 1% annual chance flood with average

areas of less than one square mile Zone

Future Conditions 1% Annual

Area with Reduced Flood Risk due to Chance Flood Hazard Zone Levee. See Notes. Zone >

Area with Flood Risk due to Levee Zone D

NO SCREEN Area of Minimal Flood Hazard Zone X **Effective LOMRs**

Area of Undetermined Flood Hazard Zone D

GENERAL

- - - Channel, Culvert, or Storm Sewer

STRUCTURES | 1111111 Levee, Dike, or Floodwall

Cross Sections with 1% Annual Chance Water Surface Elevation Coastal Transect

Base Flood Elevation Line (BFE) Limit of Study mm 513 mm

Jurisdiction Boundary

Coastal Transect Baseline Profile Baseline

OTHER

FEATURES

Hydrographic Feature

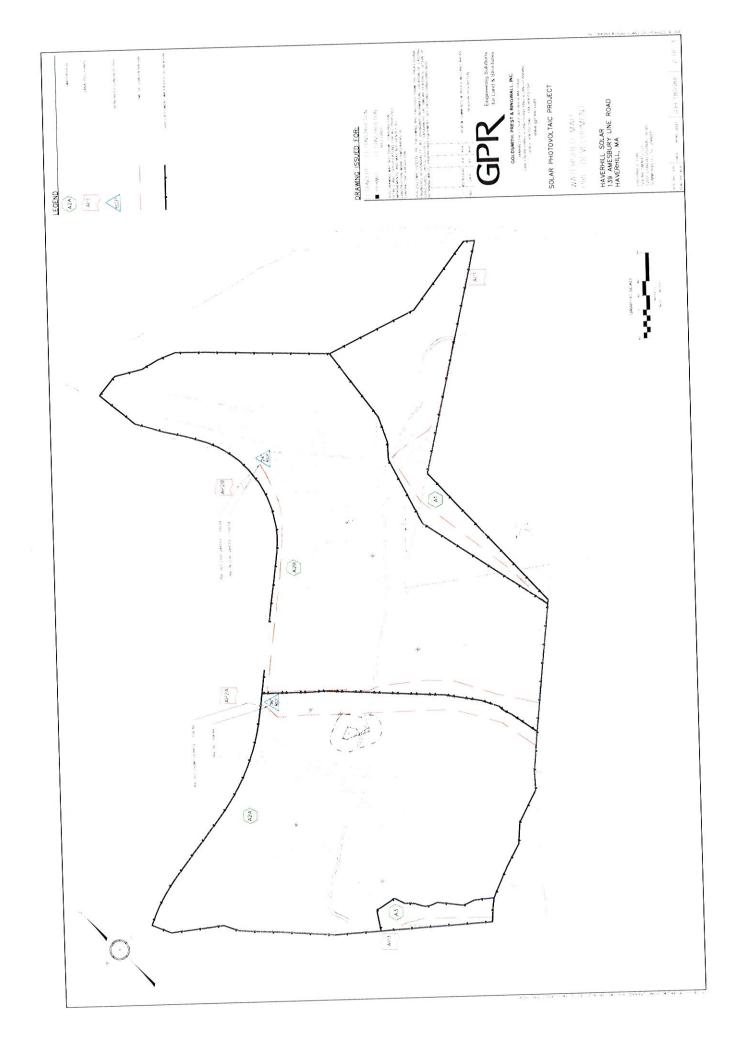
Digital Data Available

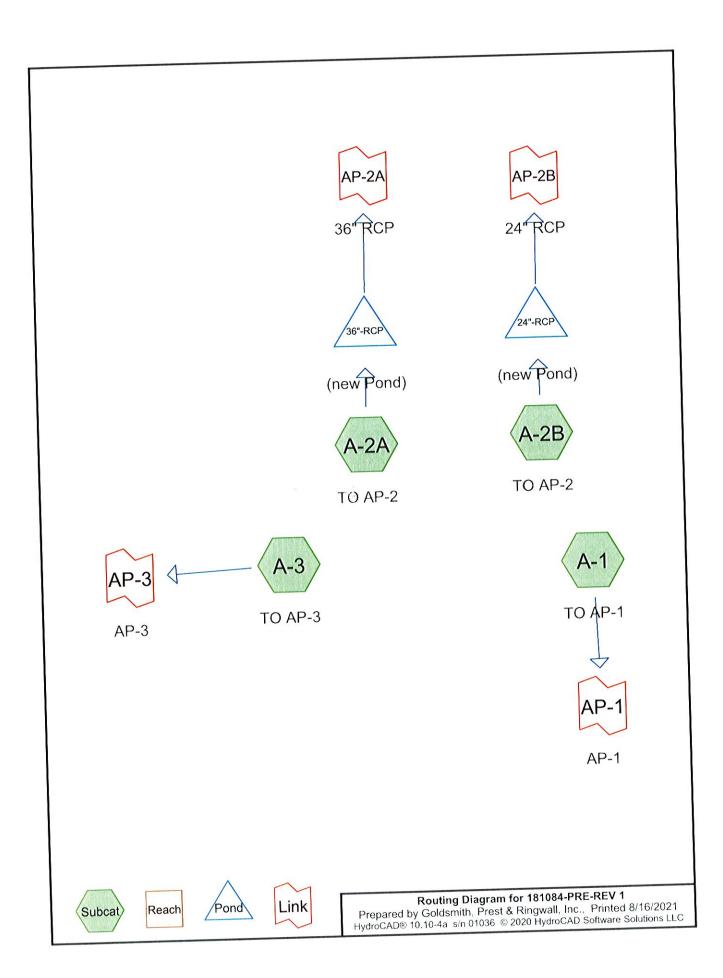
No Digital Data Available

point selected by the user and does not represent an authoritative property location. The pin displayed on the map is an approximate

This map complies with FEMA's standards for the use of The basemap shown complies with FEMA's basemap digital flood maps if it is not void as described below. accuracy standards

authoritative NFHL web services provided by FEMA. This map reflect changes or amendments subsequent to this date and was exported on 10/19/2020 at 10:45 AM and does not time. The NFHL and effective information may change or The flood hazard information is derived directly from the become superseded by new data over time. This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.





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Rainfall Events Listing

Event#		Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	Name 2-Year 10-Year 100-Year	NRCC 24-hr	D	Default	24.00	1	3.15	2
2		NRCC 24-hr	D	Default	24.00	1	4.83	2
3		NRCC 24-hr	D	Default	24.00	1	8.94	2

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 2-Year Rainfall=3.15" Printed 8/16/2021

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Page 3

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff by SCS 1R-20 method, 617 335, 518 Dyn-Stor-Ind method Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method						
Reach routing by Dy						
Subcatchment A-1: TO AP-1	Runoff Area=145,471 sf 0.46% Impervious Runoff Depth=0.80" Flow Length=999' Tc=20.8 min CN=70 Runoff=1.6 cfs 9,688 cf					
SubcatchmentA-2A: TO AP-2	Runoff Area=537,274 sf 1.78% Impervious Runoff Depth=0.80" Flow Length=788' Tc=19.9 min CN=70 Runoff=6.2 cfs 35,780 cf					
Subcatchment A-2B: TO AP-2	Runoff Area=595,445 sf 3.93% Impervious Runoff Depth=0.85" Flow Length=1,429' Tc=37.6 min CN=71 Runoff=5,3 cfs 42,088 cf					
Subcatchment A-3: TO AP-3	Runoff Area=21,227 sf 0.00% Impervious Runoff Depth=0.80" Flow Length=259' Tc=14.8 min CN=70 Runoff=0.3 cfs 1,414 cf					
Pond 24"-RCP: (new Pond)	Peak Elev=99.51' Storage=17 cf Inflow=5.3 cfs 42,088 cf 36.0" Round Culvert n=0.011 L=81.0' S=0.0062 '/' Outflow=5.3 cfs 42,086 cf					
Pond 36"-RCP: (new Pond)	Peak Elev=110.85' Storage=8 cf Inflow=6.2 cfs 35,780 cf 36.0" Round Culvert n=0.011 L=57.0' S=0.0135'/ Outflow=6.2 cfs 35,778 cf					
Link AP-1: AP-1	Inflow=1.6 cfs 9,688 cf Primary=1.6 cfs 9,688 cf					
	Inflow=6.2 cfs 35,778 cf					
Link AP-2A: 36" RCP	Primary=6.2 cfs 35,778 cf					
Link AP-2B: 24" RCP	Inflow=5.3 cfs 42,086 cf Primary=5.3 cfs 42,086 cf					
	Inflow=0.3 cfs 1,414 cf Primary=0.3 cfs 1,414 cf					
Link AP-3: AP-3	· ··· ,					

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Page 4

Summary for Subcatchment A-1: TO AP-1

Runoff =

1.6 cfs @ 12.33 hrs, Volume=

9,688 cf, Depth= 0.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

	Α	rea (sf)	CN [Description				
		9,812	39 >	75% Gras	s cover, Go	od, HSG A		
		28,748				od, HSG C		
		4,836	96 (Gravel surfa	ace, HSG C			
		288	98 F	Paved park	ing, HSG A			
		385	98 F	Roofs, HSC	βĀ			
	1	01,253	70 V	Voods, Go	od, HSG C			
		149	30 V	Voods, Go	od, HSG A			
	1	45,471	70 V	Veighted A	verage			
	1	44,798	9	9.54% Per	vious Area			
		673	C).46% Impe	ervious Area	a		
	_							
	Tc	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	10.5	75	0.0690	0.12		Sheet Flow,		
						Woods: Light underbrush n= 0.400 P2= 3.15"		
	0.3	85	0.0690			Shallow Concentrated Flow,		
						Unpaved Kv= 16.1 fps		
	1.1	291	0.0690	4.23		Shallow Concentrated Flow,		
						Unpaved Kv= 16.1 fps		
	1.3	151	0.1460	1.91		Shallow Concentrated Flow,		
				0.04		Woodland Kv= 5.0 fps		
	3.6	181	0.0280	0.84		Shallow Concentrated Flow,		
				0.00		Woodland Kv= 5.0 fps		
	4.0	216	0.0320	0.89		Shallow Concentrated Flow,		
_						Woodland Kv= 5.0 fps		
	20.8	999	Total					

Summary for Subcatchment A-2A: TO AP-2

Runoff

6.2 cfs @ 12.32 hrs, Volume=

35,780 cf, Depth= 0.80"

 Area (sf)	CN	Description	
527,687	70	Woods, Good, HSG C	
 9,587_	98	Paved parking, HSG C	
 537,274	70	Weighted Average	
527,687		98.22% Pervious Area	
9,587		1.78% Impervious Area	

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 2-Year Rainfall=3.15" Printed 8/16/2021

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Page 5

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.7		0.0430	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"
0.6	40	0.0430	1.04		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
1.8	136	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
2.2	207	0.1010	1.59		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
2.4	294	0.1670	2.04		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.2	36	0.2500	2.50		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
19.9	788	Total			

Summary for Subcatchment A-2B: TO AP-2

5.3 cfs @ 12.56 hrs, Volume= Runoff

42,088 cf, Depth= 0.85"

		·
Area (sf)	CN_	Description
 550,793	70	Woods, Good, HSG C
20,671	98	Paved parking, HSG C
21,260	74	>75% Grass cover, Good, HSG C
2,721	98	Roofs, HSG C
. 0	70	Woods, Good, HSG C
 595,445 572,053 23,392	71	Weighted Average 96.07% Pervious Area 3.93% Impervious Area

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Page 6

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)_	
14.6		0.0300	0.09		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"
0.5	26	0.0300	0.87		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
3.5	303	0.0826	1.44		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
2.1	232	0.1420	1.88		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.4	53	0.1700	2.06		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
0.5	72	0.2500	2.50		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
5.8	209	0.0144	0.60		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
5.4	234	0.0210	0.72		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
2.6	108	0.0190	0.69		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
1.6	61	0.0160	0.63		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
0.6	56	0.0890	1.49)	Shallow Concentrated Flow, Woodland Kv= 5.0 fps
37.6	1,429	Total			

Summary for Subcatchment A-3: TO AP-3

Runoff

0.3 cfs @ 12.25 hrs, Volume=

1,414 cf, Depth= 0.80"

NRCC 24	-nr D 2-1	teal Italii	ian 0.70		
	ea (sf) 21,227 21,227	70 W	oods, Goo 00.00% Pe	od, HSG C ervious Area	a
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.5	75	0.0440	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"
1.7	106	0.0440	1.05		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.6	78	0.1790	2.12		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
14.8	259	Total			

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Page 7

Summary for Pond 24"-RCP: (new Pond)

595,445 sf, 3.93% Impervious, Inflow Depth = 0.85" for 2-Year event Inflow Area = 42,088 cf

5.3 cfs @ 12.56 hrs, Volume= Inflow

42,086 cf, Atten= 0%, Lag= 0.0 min 5.3 cfs @ 12.56 hrs, Volume=

Outflow 5.3 cfs @ 12.56 hrs, Volume= 42,086 cf Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 99.51' @ 12.56 hrs Surf.Area= 27 sf Storage= 17 cf

Plug-Flow detention time= 0.1 min calculated for 42,057 cf (100% of inflow) Center-of-Mass det. time= 0.1 min (938.2 - 938.2)

-							
Volume _	Invert	Avail	Storage	Storage Description	- N. S. S.	halow (Pacalc)	
#1	98.00'		4,909 cf	Custom Stage Data	a (Irregular)Listed	Delow (Medalo)	
Elevation (feet)	Surf.,	Area sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft) 1	
98.00 99.00 100.00		1 15 42	3.0 22.0 31.0	0 7 27 60	0 7 34 94	41 87 134	
101.00 102.00 103.00 104.00		79 189 809 1,937 3,963	37.0 60.0 120.0 205.0 302.0	130 463 1,333	224 687 2,019 4,909	318 1,182 3,387 7,308	

105.00 Invert Outlet Devices Routing Device 36.0" Round Culvert 98.54" Primary #1

L= 81.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 98.54' / 98.04' S= 0.0062 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=5.3 cfs @ 12.56 hrs HW=99.51' TW=0.00' (Dynamic Tailwater) -1=Culvert (Inlet Controls 5.3 cfs @ 2.65 fps)

Summary for Pond 36"-RCP: (new Pond)

Inflow Area = Inflow = Outflow = Primary =	537,274 sf, 1.78% Impervious 6.2 cfs @ 12.32 hrs, Volume 6.2 cfs @ 12.32 hrs, Volume 6.2 cfs @ 12.32 hrs, Volume	35,770 01, 7 11011 5 717 5
--------------------------------------------	---------------------------------------------------------------------------------------------------------------------------	----------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 110.85' @ 12.32 hrs Surf.Area= 9 sf Storage= 8 cf

Plug-Flow detention time= 0.2 min calculated for 35,778 cf (100% of inflow) Center-of-Mass det. time= 0.0 min (926.2 - 926.2)

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HydroCAD®	10.10-4a_s					
Volume #1	Invert 109.00'	Avail.	Storage 412 cf	Storage Description Custom Stage Dat	a (Irregular)Listed	below (Recalc)
Elevation (feet) 109.00 110.00 111.00 112.00 113.00 114.00 115.00		rf.Area (sq-ft) 1 4 10 18 43 165 372	Perim. (feet) 4.0 9.0 15.0 19.0 27.0 52.0 74.0	Inc.Store (cubic-feet) 0 2 7 14 30 97 262	Cum.Store (cubic-feet) 0 2 9 23 53 150 412	Wet.Area (sq-ft) 1 9 26 46 83 245 475
	Routing Primary	Inv 109.	.79' 36. 6	let Devices "Round Culvert 57.0' CMP, projectin t / Outlet Invert= 109 0.011 Concrete pipe		

Primary OutFlow Max=6.1 cfs @ 12.32 hrs HW=110.84' TW=0.00' (Dynamic Tailwater)
1=Culvert (Inlet Controls 6.1 cfs @ 2.76 fps)

Summary for Link AP-1: AP-1

	145,471 sf, 0.46% Impervious	Inflow Depth = 0.80" for 2-Year event
IIIIOW / II oo	1 6 cfs @ 12.33 hrs, Volume:	9,000 of Attan= 0% 1 an= 0.0 min
Inflow = Primary =	1.6 cfs @ 12.33 hrs, Volume	= 9,688 CI, Allen = 070, Edg - 015

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2A: 36" RCP

		507 074 of	1.78% Impervious	, Inflow Depth =	0.80"	for 2-Year event
HIHOW	_	62 cfs @	12.32 hrs, Volume 12.32 hrs, Volume	33,770	of of, Att∈	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2B: 24" RCP

53 cfs @	3.93% Impervious, 12.56 hrs, Volume= 12.56 hrs, Volume=	Inflow Depth = 0.85" for 2-Year event 42,086 cf 42,086 cf, Atten= 0%, Lag= 0.0 min
----------	---------------------------------------------------------------	------------------------------------------------------------------------------------------

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 2-Year Rainfall=3.15"

181084-PRE-REV 1

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Page 9

Summary for Link AP-3: AP-3

21,227 sf, 0.00% Impervious, Inflow Depth = 0.80" for 2-Year event Inflow Area =

1,414 cf Inflow

0.3 cfs @ 12.25 hrs, Volume= 0.3 cfs @ 12.25 hrs, Volume= 1,414 cf, Atten= 0%, Lag= 0.0 min Primary

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 10-Year Rainfall=4.83" Printed 8/16/2021

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Page 10

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method					
Subcatchment A-1: TO AP-1	Runoff Area=145,471 sf 0.46% Impervious Runoff Depth=1.91" Flow Length=999' Tc=20.8 min CN=70 Runoff=4.3 cfs 23,168 cf				
Subcatchment A-2A: TO AP-2	Runoff Area=537,274 sf 1.78% Impervious Runoff Depth=1.91" Flow Length=788' Tc=19.9 min CN=70 Runoff=16.3 cfs 85,569 cf				
Subcatchment A-2B: TO AP-2	Runoff Area=595,445 sf 3.93% Impervious Runoff Depth=1.99" Flow Length=1,429' Tc=37.6 min CN=71 Runoff=13.5 cfs 98,688 cf				
Subcatchment A-3: TO AP-3	Runoff Area=21,227 sf 0.00% Impervious Runoff Depth=1.91" Flow Length=259' Tc=14.8 min CN=70 Runoff=0.7 cfs 3,381 cf				
Pond 24"-RCP: (new Pond)	Peak Elev=100.18' Storage=42 cf Inflow=13.5 cfs 98,688 cf 36.0" Round Culvert n=0.011 L=81.0' S=0.0062 '/' Outflow=13.5 cfs 98,686 cf				
Pond 36"-RCP: (new Pond)	Peak Elev=111.61' Storage=17 cf Inflow=16.3 cfs 85,569 cf 36.0" Round Culvert n=0.011 L=57.0' S=0.0135 '/' Outflow=16.3 cfs 85,567 cf				
Link AP-1: AP-1	Inflow=4.3 cfs 23,168 cf Primary=4.3 cfs 23,168 cf				
Link AP-2A: 36" RCP	Inflow=16.3 cfs 85,567 cf Primary=16.3 cfs 85,567 cf				
Link AP-2B: 24" RCP	Inflow=13.5 cfs 98,686 cf Primary=13.5 cfs 98,686 cf				
Link AP-3: AP-3	Inflow=0.7 cfs 3,381 cf Primary=0.7 cfs 3,381 cf				

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Page 11

Summary for Subcatchment A-1: TO AP-1

Runoff

4.3 cfs @ 12.31 hrs, Volume=

23,168 cf, Depth= 1.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

	Ar	ea (sf)		escription_						
_		9,812	39 >	39 >75% Grass cover, Good, HSG A						
	2	28,748			cover, Go					
		4,836			ce, HSG C					
		288			ng, HSG A					
		385		oofs, HSG						
	11	01,253		loods, Goo						
_		149			od, HSG A					
		45,471	70 V	Veighted A	verage					
	1	44,798			vious Area					
		673	U	.46% impe	rvious Area	1				
	To	Length	Slope	Velocity	Capacity	Description				
	Tc (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	10.5	75	0.0690	0.12		Sheet Flow,				
	10.5	, 0	0.0000			Woods: Light underbrush n= 0.400 P2= 3.15"				
	0.3	85	0.0690	4.23		Shallow Concentrated Flow,				
	0.0					Unpaved Kv= 16.1 fps				
	1.1	291	0.0690	4.23		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	1.3	151	0.1460	1.91		Shallow Concentrated Flow, Woodland Kv= 5.0 fps				
				^ ^ 4		Shallow Concentrated Flow,				
	3.6	181	0.0280	0.84		Woodland Kv= 5.0 fps				
		040	0.000	0.00		Shallow Concentrated Flow,				
	4.0	216	0.0320	0.89		Woodland Kv= 5.0 fps				
_			Total							
	20.8	999	Total							

Summary for Subcatchment A-2A: TO AP-2

Runoff

16.3 cfs @ 12.30 hrs, Volume=

85,569 cf, Depth= 1.91"

Area (sf)	CN	Description	
527,687 9,587	70 98_	Woods, Good, HSG C Paved parking, HSG C	
 537,274 527,687 9,587	70	Weighted Average 98.22% Pervious Area 1.78% Impervious Area	

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Pag	е	1	2

(mi	Tc in)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12	2.7	75	0.0430	0.10		Sheet Flow,
C).6	40	0.0430	1.04		Woods: Light underbrush n= 0.400 P2= 3.15" Shallow Concentrated Flow, Woodland Kv= 5.0 fps
1	8.1	136	0.0660	1.28		Shallow Concentrated Flow,
2	2.2	207	0.1010	1.59		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps
2	2.4	294	0.1670	2.04		Shallow Concentrated Flow,
C).2	36	0.2500	2.50		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps
19	9.9	788	Total			

Summary for Subcatchment A-2B: TO AP-2

13.5 cfs @ 12.53 hrs, Volume= Runoff

98,688 cf, Depth= 1.99"

Area (sf)	CN	Description			
550,793	70	Woods, Good, HSG C			
20,671	98	Paved parking, HSG C			
21,260	74	>75% Grass cover, Good, HSG C			
2,721	98	Roofs, HSG C			
0	70	Woods, Good, HSG C			
595,445	71	Weighted Average			
572,053		96.07% Pervious Area			
23,392		3.93% Impervious Area			

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Page 13

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
14.6	75	0.0300	0.09		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.15"
0.5	26	0.0300	0.87		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
3.5	303	0.0826	1.44		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.1	232	0.1420	1.88		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.4	53	0.1700	2.06		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.5	72	0.2500	2.50		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
5.8	209	0.0144	0.60		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
5.4	234	0.0210	0.72		Shallow Concentrated Flow,
			0.00		Woodland Kv= 5.0 fps
2.6	108	0.0190	0.69		Shallow Concentrated Flow,
	0.4	0.0400	0.00		Woodland Kv= 5.0 fps
1.6	61	0.0160	0.63		Shallow Concentrated Flow,
0.0	<i>"</i> 0	0.0000	4 40		Woodland Kv= 5.0 fps
0.6	56	0.0890	1.49		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
					woodiand ty- 5.0 lps
37.6	1,429	Total			

Summary for Subcatchment A-3: TO AP-3

Runoff =

0.7 cfs @ 12.24 hrs, Volume=

3,381 cf, Depth= 1.91"

	Α	rea (sf)	CN [Description		
		21,227	70 V	Voods, Go	od, HSG C	
	21,227 100.00% Pervious Area				ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	12.5	75	0.0440	0.10		Sheet Flow,
	1.7	106	0.0440	1.05		Woods: Light underbrush n= 0.400 P2= 3.15" Shallow Concentrated Flow, Woodland Kv= 5.0 fps
	0.6	78	0.1790	2.12		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
_	14.8	259	Total			

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Page 14

Summary for Pond 24"-RCP: (new Pond)

595,445 sf, 3.93% Impervious, Inflow Depth = 1.99" for 10-Year event Inflow Area =

98,688 cf 13.5 cfs @ 12.53 hrs, Volume= Inflow

13.5 cfs @ 12.53 hrs, Volume= 98,686 cf, Atten= 0%, Lag= 0.1 min Outflow

98,686 cf 13.5 cfs @ 12.53 hrs, Volume= Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 100.18' @ 12.53 hrs Surf.Area= 48 sf Storage= 42 cf

Plug-Flow detention time= 0.8 min calculated for 98,686 cf (100% of inflow)

Center-of-Mass det. time= 0.1 min (905.2 - 905.1)

Volume	Invert Av	ail.Storage	Storage Description				
#1	98.00'	4,909 cf	Custom Stage D	ata (Irregular)List	ed below (Recalc)		
Elevation (feet)	Surf.Area (sq-ft)		Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)		
98.00	1	3.0	0	0	1		
99.00	15	22.0	7	7	41		
100.00	42	31.0	27	34	87		
101.00	79	37.0	60	94	134		
102.00	189	60.0	130	224	318		
103.00	809	120.0	463	687	1,182		
104.00	1,937	205.0	1,333	2,019	3,387		
105.00	3,963		2,890	4,909	7,308		
Davisa Po	uting	Invert Out	et Devices				

Device Routing Invert Outlet Devices 36.0" Round Culvert 98.54' #1 Primary

L= 81.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 98.54' / 98.04' S= 0.0062 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=13.5 cfs @ 12.53 hrs HW=100.18' TW=0.00' (Dynamic Tailwater) 1=Culvert (Barrel Controls 13.5 cfs @ 4.94 fps)

Summary for Pond 36"-RCP: (new Pond)

537,274 sf, 1.78% Impervious, Inflow Depth = 1.91" for 10-Year event Inflow Area = 85,569 cf 16.3 cfs @ 12.30 hrs, Volume= Inflow 85,567 cf, Atten= 0%, Lag= 0.0 min

16.3 cfs @ 12.30 hrs, Volume= Outflow

16.3 cfs @ 12.30 hrs, Volume= 85,567 cf **Primary**

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 111.61' @ 12.30 hrs Surf.Area= 15 sf Storage= 17 cf

Plug-Flow detention time= 0.0 min calculated for 85,508 cf (100% of inflow)

Center-of-Mass det. time= 0.0 min (892.0 - 892.0)

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HydroCAD®	<u>10.10-4a s</u>	/n 01036 (© 2020 Hyd	MOCAD Software Con		
Volume	Invert 109.00'			Storage Description Custom Stage Data		pelow (Recalc)
#1 Elevation (feet) 109.00 110.00 111.00 112.00 113.00 114.00 115.00		rf.Area (sq-ft) 1 4 10 18 43 165 372	Perim. (feet) 4.0 9.0 15.0 19.0 27.0 52.0 74.0	Inc.Store (cubic-feet) 0 2 7 14 30 97 262	Cum.Store (cubic-feet) 0 2 9 23 53 150 412	Wet.Area (sq-ft) 1 9 26 46 83 245 475
	Routing Primary	Inv 109.	79' 36.0 '),011 Concrete pipe	ng, no headwall, K 9.79' / 109.02' S= 6 e, straight & clean,	Flow Area= 7.07 sf

Primary OutFlow Max=16.2 cfs @ 12.30 hrs HW=111.61' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 16.2 cfs @ 3.62 fps)

Summary for Link AP-1: AP-1

Inflow Area = 145,471 sf, 0.46% Impervious, Inflow = 4.3 cfs @ 12.31 hrs, Volume= 4.3 cfs @ 12.31 hrs, Volume=	100 4 Atton= 0% Lag= 0.0 min
----------------------------------------------------------------------------------------------------------------	------------------------------

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2A: 36" RCP

Inflow =	537,274 sf, 1.78% Impervious, 16.3 cfs @ 12.30 hrs, Volume= 16.3 cfs @ 12.30 hrs, Volume=	05 507 of Atton= 0% ag= 0.0 min
Primary =		

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2B: 24" RCP

Inflow Area = Inflow = Primary =	12 5 cfs (17)	3.93% Impervious, 12.53 hrs. Volume= 12.53 hrs, Volume=	98,686 cf	for 10-Year event n= 0%, Lag= 0.0 min
,				

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 10-Year Rainfall=4.83"

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Page 16

Summary for Link AP-3: AP-3

21,227 sf, 0.00% Impervious, Inflow Depth = 1.91" for 10-Year event 0.7 cfs @ 12.24 hrs, Volume= 3,381 cf Inflow Area =

Inflow

Primary = 0.7 cfs @ 12.24 hrs, Volume= 3,381 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94"

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Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=145,471 sf 0.46% Impervious Runoff Depth=5.28" Subcatchment A-1: TO AP-1 Flow Length=999' Tc=20.8 min CN=70 Runoff=12.2 cfs 64,033 cf

Runoff Area=537,274 sf 1.78% Impervious Runoff Depth=5.28" Subcatchment A-2A: TO AP-2 Flow Length=788' Tc=19.9 min CN=70 Runoff=45.8 cfs 236,497 cf

Runoff Area=595,445 sf 3.93% Impervious Runoff Depth=5.41" Subcatchment A-2B: TO AP-2 Flow Length=1,429' Tc=37.6 min CN=71 Runoff=37.5 cfs 268,209 cf

Runoff Area=21,227 sf 0.00% Impervious Runoff Depth=5.28" Subcatchment A-3: TO AP-3 Flow Length=259' Tc=14.8 min CN=70 Runoff=2.1 cfs 9,344 cf

Peak Elev=101.99' Storage=221 cf Inflow=37.5 cfs 268,209 cf Pond 24"-RCP: (new Pond) 36.0" Round Culvert n=0.011 L=81.0' S=0.0062'/ Outflow=37.5 cfs 268,207 cf

Peak Elev=114.20' Storage=185 cf Inflow=45.8 cfs 236,497 cf Pond 36"-RCP: (new Pond) 36.0" Round Culvert n=0.011 L=57.0' S=0.0135 '/' Outflow=45.8 cfs 236,495 cf

Inflow=12.2 cfs 64,033 cf Link AP-1: AP-1 Primary=12.2 cfs 64,033 cf

Inflow=45.8 cfs 236,495 cf Link AP-2A: 36" RCP Primary=45.8 cfs 236,495 cf

Inflow=37.5 cfs 268,207 cf Link AP-2B: 24" RCP Primary=37.5 cfs 268,207 cf

Inflow=2.1 cfs 9,344 cf Link AP-3: AP-3 Primary=2.1 cfs 9,344 cf

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Page 18

Summary for Subcatchment A-1: TO AP-1

Runoff = 12.2 cfs @ 12.30 hrs, Volume=

64,033 cf, Depth= 5.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

 Α	rea (sf)	CN [Description						
	9,812	39 >	>75% Grass cover, Good, HSG A						
	28,748	74 >	>75% Gras	s cover, Go	od, HSG C				
	4,836	96 (Gravel surfa	ace, HSG C					
	288	98 F	Paved park	ing, HSG A					
	385	98 F	Roofs, HSG	βA					
1	01,253	70 \	Noods, Go	od, HSG C					
	149	30 \	Noods, Go	od, HSG A					
1	45,471	70 \	Neighted A	verage					
1	44,798	(99.54% Per	vious Area					
	673	().46% Impe	ervious Area					
Тс	Length	Slope		Capacity	Description				
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
10.5	75	0.0690	0.12		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 3.15"				
0.3	85	0.0690	4.23		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
1.1	291	0.0690	4.23		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
1.3	151	0.1460	1.91		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
3.6	181	0.0280	0.84		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
4.0	216	0.0320	0.89		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
20.8	999	Total							

Summary for Subcatchment A-2A: TO AP-2

Runoff = 45.8 cfs @ 12.29 hrs, Volume=

236,497 cf, Depth= 5.28"

	Area (sf)	ÇN	Description
	527,687	70	Woods, Good, HSG C
	9,587	98	Paved parking, HSG C
•	537,274	70	Weighted Average
	527,687		98.22% Pervious Area
	9,587		1.78% Impervious Area

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181084-PRE-REV 1

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Page 19

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.7	75	0.0430	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"
0.6	40	0.0430	1.04		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
1.8	136	0.0660	1.28		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
2.2	207	0.1010	1.59		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
2.4	294	0.1670	2.04		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.2	36	0.2500	2.50		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
19.9	788	Total			

Summary for Subcatchment A-2B: TO AP-2

268,209 cf, Depth= 5.41" 37.5 cfs @ 12.51 hrs, Volume= Runoff

11110	· - ·		
	Area (sf)	<u>CN</u>	Description
	550,793	70	Woods, Good, HSG C
	20,671	98	Paved parking, HSG C
	21,260	74	>75% Grass cover, Good, HSG C
	2,721	98	Roofs, HSG C
	. 0	70	Woods, Good, HSG C
	595,445 572,053 23,392	71	Weighted Average 96.07% Pervious Area 3.93% Impervious Area

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Page 20

	Tc (min)	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	A
	14.6	75	0.0300	0.09		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.15"
	0.5	26	0.0300	0.87		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	3.5	303	0.0826	1.44		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	2.1	232	0.1420	1.88		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.4	53	0.1700	2.06		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.5	72	0.2500	2.50		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	5.8	209	0.0144	0.60		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	5.4	234	0.0210	0.72		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	2.6	108	0.0190	0.69		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	1,6	61	0.0160	0.63		Shallow Concentrated Flow,
		•	0.0.00	0.00		Woodland Kv= 5.0 fps
	0.6	56	0.0890	1.49		Shallow Concentrated Flow,
	0.0		0.0000	1.70		Woodland Kv= 5.0 fps
	37.6	1,429	Total			7700diditd 177-0.0 ip3
	31.0	1,429	iotai			

Summary for Subcatchment A-3: TO AP-3

Runoff

2.1 cfs @ 12.23 hrs, Volume=

9,344 cf, Depth= 5.28"

А	rea (sf)	CN	Description		
	21,227	70	Woods, Go	od, HSG C	
	21,227		100.00% Pe	ervious Are	a
Tc (min)	Length (feet)	Slope (ft/ft)	•	Capacity (cfs)	Description
12.5	75	0.0440	0.10		Sheet Flow,
1.7	106	0.0440	1.05		Woods: Light underbrush n= 0.400 P2≈ 3.15" Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.6	78	0.1790	2.12		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
14.8	259	Total			

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Page 21

Summary for Pond 24"-RCP: (new Pond)

595,445 sf, 3.93% Impervious, Inflow Depth = 5.41" for 100-Year event Inflow Area = 268,209 cf

37.5 cfs @ 12.51 hrs, Volume= Inflow

268,207 cf, Atten= 0%, Lag= 0.4 min 37.5 cfs @ 12.52 hrs, Volume=

Outflow 268,207 cf 37.5 cfs @ 12.52 hrs, Volume= Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 101.99' @ 12.52 hrs Surf.Area= 187 sf Storage= 221 cf

Plug-Flow detention time= 0.8 min calculated for 268,207 cf (100% of inflow)

Center-of-Mass det. time= 0.1 min (867.9 - 867.9)

olume #1	Invert 98.00'		Storage_ 4,909 cf	Custom Stage Data	a (Irregular)Listed	below (Recalc)
Elevation (feet)		f.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
98.00 99.00 100.00 101.00 102.00 103.00 104.00 105.00		1 15 42 79 189 809 1,937 3,963	3.0 22.0 31.0 37.0 60.0 120.0 205.0 302.0	0 7 27 60 130 463 1,333 2,890	0 7 34 94 224 687 2,019 4,909	41 87 134 318 1,182 3,387 7,308

36.0" Round Culvert 98.54 Primary #1

L= 81.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 98.54' / 98.04' S= 0.0062 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=37.4 cfs @ 12.52 hrs HW=101.97' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 37.4 cfs @ 5.29 fps)

Summary for Pond 36"-RCP: (new Pond)

537,274 sf, 1.78% Impervious, Inflow Depth = 5.28" for 100-Year event Inflow Area = 236,497 cf 45.8 cfs @ 12.29 hrs, Volume= 236,495 cf, Atten= 0%, Lag= 0.4 min Inflow 45.8 cfs @ 12.30 hrs, Volume= Outflow 236,495 cf 45.8 cfs @ 12.30 hrs, Volume= Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 114.20' @ 12.30 hrs Surf.Area= 199 sf Storage= 185 cf

Plug-Flow detention time= 0.0 min calculated for 236,331 cf (100% of inflow) Center-of-Mass det. time= 0.0 min (854.2 - 854.1)

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Page 22

<u>Volume</u>	Inv	<u>ert Avail.</u>	Storage	Storage Description	n		
#1	109.	00'	412 cf	Custom Stage Da	ta (Irregular)Liste	ed below (Recalc)	
Elevation (fee		Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
109.0	00	1	4.0	0	0	1	
110.0	00	4	9.0	2	2	9	
111.0	00	10	15.0	7	9	26	
112.0	00	18	19.0	14	23	46	
113.0	00	43	27.0	30	53	83	
114.0	00	165	52.0	97	150	245	
115.0	00	372	74.0	262	412	475	
Device	Routing	Inv	ert Outle	et Devices_			
#1	Primary	109.7	L= 5 Inlet	" Round Culvert 7.0' CMP, projectin / Outlet Invert= 109. 011 Concrete pipe,	.79' / 109.02' S=	0.0135 '/' Cc= 0	

Primary OutFlow Max=45.8 cfs @ 12.30 hrs HW=114.19' TW=0.00' (Dynamic Tailwater) —1=Culvert (Inlet Controls 45.8 cfs @ 6.47 fps)

Summary for Link AP-1: AP-1

Inflow Area	a =	145,471 sf,	0.46% Impervious,	Inflow Depth = 5.28"	for 100-Year event
Inflow	=	12.2 cfs @	12.30 hrs, Volume=	64,033 cf	
Primary	=	12.2 cfs @	12.30 hrs, Volume=	64,033 cf, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2A: 36" RCP

Inflow Are	a =	537,274 sf,	1.78% Impervious,	Inflow Depth = 5.28'	for 100-Year event
Inflow	=	45.8 cfs @	12.30 hrs, Volume=	236,495 cf	
Primary	=	45.8 cfs @	12.30 hrs, Volume=	236,495 cf, At	ten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2B: 24" RCP

Inflow Are	a =	595,445 sf,	3.93% Impervious,	Inflow Depth = 5.41"	for 100-Year event
Inflow	=	37.5 cfs @	12.52 hrs, Volume=	268,207 cf	
Primary	=	37.5 cfs @	12.52 hrs, Volume=	268,207 cf. Atte	en= 0%. Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

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Page 23

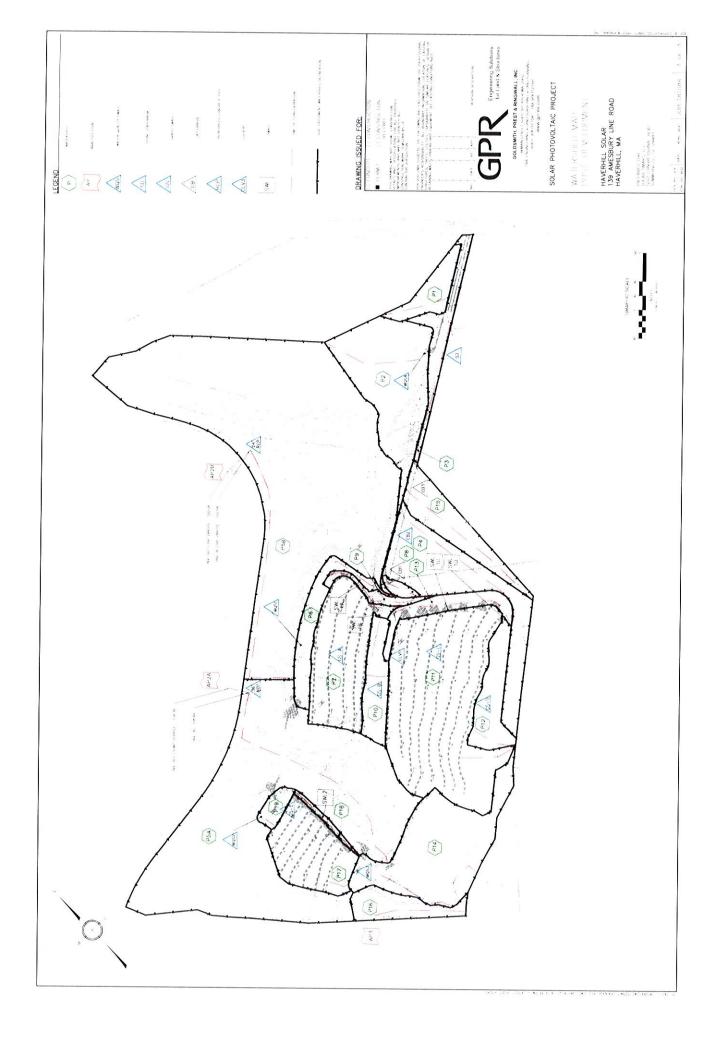
Summary for Link AP-3: AP-3

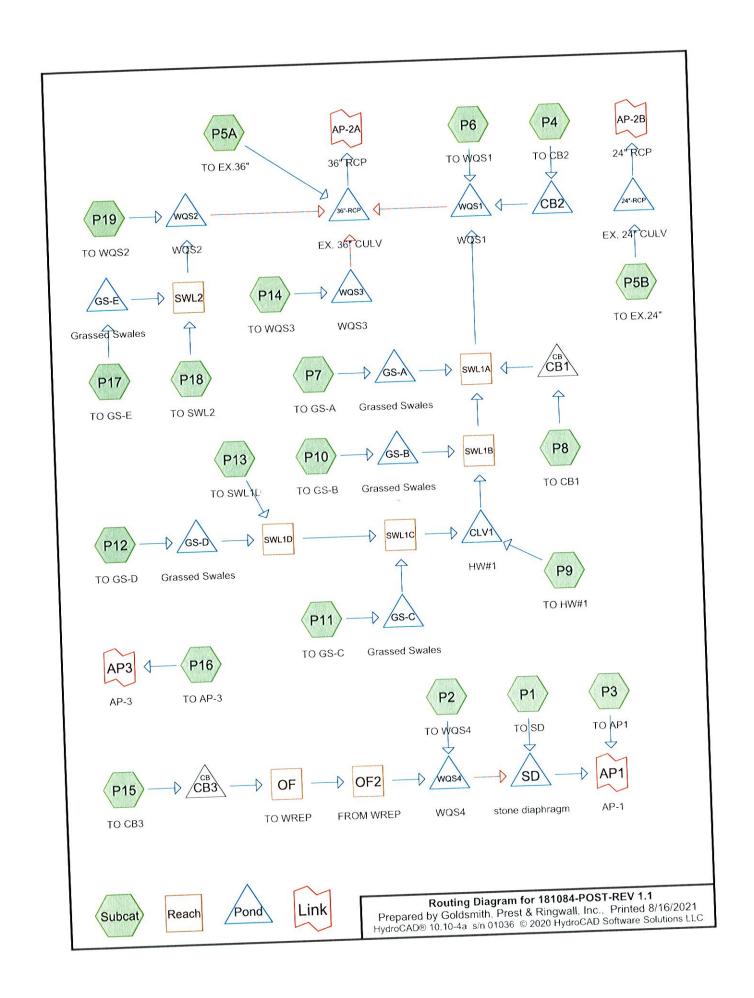
21,227 sf, 0.00% Impervious, Inflow Depth = 5.28" for 100-Year event Inflow Area =

9,344 cf Inflow

2.1 cfs @ 12.23 hrs, Volume= 2.1 cfs @ 12.23 hrs, Volume= 9,344 cf, Atten= 0%, Lag= 0.0 min Primary

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs





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Rainfall Events Listing

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	в/в	Depth (inches)	AMC
1	2-Year	NRCC 24-hr	D	Default	24.00	1	3.15	2
2	10-Year	NRCC 24-hr	D	Default	24.00	1	4.83	2
3	100-Year	NRCC 24-hr	D	Default	24.00	1	8.94	2

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Page 3

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff by SCS TR-2 Reach routing by Dyn-Stor-Ind m	ethod - Pond routing by Dyn-Stor-Ind method
SubcatchmentP1: TO SD	Runoff Area=16,143 sf 4.08% Impervious Runoff Depth=0.54" Flow Length=204' Tc=8.3 min CN=64 Runoff=0.2 cfs 721 cf
Subcatchment P10: TO GS-B Flow Length=45	Runoff Area=21,159 sf 1.51% Impervious Runoff Depth=1.18" Slope=0.0667 '/' Tc=5.0 min CN=77 Runoff=0.6 cfs 2,074 cf
Subcatchment P11: TO GS-C	Runoff Area=144,531 sf 0.00% Impervious Runoff Depth=1.06" Flow Length=67' Tc=5.0 min CN=75 Runoff=3.8 cfs 12,770 cf
Subcatchment P12: TO GS-D	Runoff Area=25,460 sf 0.00% Impervious Runoff Depth=1.43" Flow Length=75' Tc=5.0 min CN=81 Runoff=0.9 cfs 3,034 cf
Subcatchment P13: TO SWL1D	Runoff Area=17,550 sf 1.82% Impervious Runoff Depth=1.57" Flow Length=327' Tc=5.0 min CN=83 Runoff=0.7 cfs 2,294 cf
Subcatchment P14: TO WQS3	Runoff Area=81,404 sf 0.49% Impervious Runoff Depth=1.12" Flow Length=385' Tc=5.0 min CN=76 Runoff=2.3 cfs 7,580 cf
SubcatchmentP15: TO CB3	Runoff Area=31,226 sf 0.00% Impervious Runoff Depth=1.12" Flow Length=550' Tc=13.4 min CN=76 Runoff=0.7 cfs 2,908 cf
Subcatchment P16: TO AP-3	Runoff Area=19,815 sf 0.00% Impervious Runoff Depth=0.85" Flow Length=259' Tc=14.8 min CN=71 Runoff=0.3 cfs 1,401 cf
Subcatchment P17: TO GS-E	Runoff Area=43,526 sf 0.00% Impervious Runoff Depth=1.00" Flow Length=184' Tc=5.0 min CN=74 Runoff=1.1 cfs 3,644 cf
Subcatchment P18: TO SWL2	Runoff Area=3,212 sf 0.00% Impervious Runoff Depth=1.00" Tc=5.0 min CN=74 Runoff=0.1 cfs 269 cf
Subcatchment P19: TO WQS2 Flow Length=	Runoff Area=6,629 sf 0.00% Impervious Runoff Depth=1.00" =31' Slope=0.2260 '/' Tc=5.0 min CN=74 Runoff=0.2 cfs 555 cf
Subcatchment P2: TO WQS4	Runoff Area=75,884 sf 0.00% Impervious Runoff Depth=0.95" Flow Length=285' Tc=9.3 min CN=73 Runoff=1.5 cfs 6,014 cf
Subcatchment P3: TO AP1	Runoff Area=19,706 sf 1.38% Impervious Runoff Depth=1.64" Flow Length=498' Tc=6.6 min CN=84 Runoff=0.8 cfs 2,694 cf
SubcatchmentP4: TO CB2	Runoff Area=66,052 sf 0.00% Impervious Runoff Depth=0.90" Flow Length=824' Tc=16.4 min CN=72 Runoff=1.0 cfs 4,947 cf
SubcatchmentP5A: TO EX.36"	Runoff Area=273,835 sf 3.65% Impervious Runoff Depth=0.90" Flow Length=691' Tc=16.5 min CN=72 Runoff=4.0 cfs 20,510 cf
SubcatchmentP5B: TO EX.24"	Runoff Area=359,530 sf 6.51% Impervious Runoff Depth=0.95" Flow Length=783' Tc=19.6 min CN=73 Runoff=5.2 cfs 28,492 cf

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Page 4

Subcatchment P6: TO WQ\$1 Runoff Area=22,064 sf 0.00% Impervious Runoff Depth=1.00"

Flow Length=35' Slope=0.1700 '/' Tc=5.0 min CN=74 Runoff=0.5 cfs 1,847 cf

Subcatchment P7: TO GS-A Runoff Area=61,702 sf 0.00% Impervious Runoff Depth=1.00"

Flow Length=308' Tc=5.0 min CN=74 Runoff=1.5 cfs 5,166 cf

Subcatchment P8: TO CB1 Runoff Area=3,312 sf 0.00% Impervious Runoff Depth=1.00"

Flow Length=119' Slope=0.1180 '/' Tc=5.0 min CN=74 Runoff=0.1 cfs 277 cf

Subcatchment P9: TO HW#1 Runoff Area=6,677 sf 3.29% Impervious Runoff Depth=1.64"

Flow Length=267' Tc=5.0 min CN=84 Runoff=0.3 cfs 913 cf

Reach OF: TO WREP Avg. Flow Depth=0.05' Max Vel=1.02 fps Inflow=0.7 cfs 2,908 cf

n=0.035 L=180.0' S=0.0389 '/' Capacity=1,899.8 cfs Outflow=0.6 cfs 2,908 cf

Reach OF2: FROM WREP Avg. Flow Depth=0.28' Max Vel=2.62 fps Inflow=0.6 cfs 2,908 cf

n=0.035 L=126.0' S=0.0556 '/' Capacity=115.9 cfs Outflow=0.6 cfs 2,908 cf

Reach SWL1A: Avg. Flow Depth=0.12' Max Vel=3.47 fps Inflow=1.0 cfs 4,238 cf

n=0.035 L=157.0' S=0.1338 '/' Capacity=263.5 cfs Outflow=1.0 cfs 4,238 cf

Reach SWL1B: Avg. Flow Depth=0.11' Max Vel=3.85 fps Inflow=0.9 cfs 3,961 cf

n=0.035 L=20.0' S=0.2000 '/' Capacity=322.2 cfs Outflow=0.9 cfs 3,961 cf

Reach SWL1C: Avg. Flow Depth=0.12' Max Vel=2.47 fps Inflow=0.7 cfs 3,048 cf

n=0.035 L=301.0' S=0.0731 '/' Capacity=194.8 cfs Outflow=0.7 cfs 3,048 cf

Reach SWL1D: Avg. Flow Depth=0.10' Max Vel=2.92 fps Inflow=0.7 cfs 3,048 cf

n=0.035 L=25.0' S=0.1200'/' Capacity=249.6 cfs Outflow=0.7 cfs 3,048 cf

Reach SWL2: Avg. Flow Depth=0.11' Max Vel=2.10 fps Inflow=0.1 cfs 269 cf

n=0.035 L=265.0' S=0.1245 '/' Capacity=173.6 cfs Outflow=0.1 cfs 269 cf

Pond 24"-RCP: EX. 24" CULV Peak Elev=99.51' Storage=17 cf Inflow=5.2 cfs 28,492 cf

36.0" Round Culvert n=0.011 L=81.0' S=0.0062 '/' Outflow=5.2 cfs 28,490 cf

Pond 36"-RCP: EX. 36" CULV Peak Elev=110.83' Storage=8 cf Inflow=6.0 cfs 39,263 cf

36.0" Round Culvert n=0.011 L=57.0' S=0.0135 '/' Outflow=6.0 cfs 39,261 cf

Pond CB1: Peak Elev=166.12' Inflow=0.1 cfs 277 cf

12.0" Round Culvert n=0.013 L=62.0' S=0.0081 '/' Outflow=0.1 cfs 277 cf

Pond CB2: Peak Elev=148.00' Storage=0 cf Inflow=1.0 cfs 4,947 cf

15.0" Round Culvert n=0.013 L=264.0' S=0.0049'/ Outflow=1.0 cfs 4.947 cf

Pond CB3: Peak Elev=129.17' Inflow=0.7 cfs 2,908 cf

12.0" Round Culvert n=0.013 L=34.0' S=0.0118 '/' Outflow=0.7 cfs 2,908 cf

Pond CLV1: HW#1 Peak Elev=174.00' Storage=0 cf Inflow=0.9 cfs 3,961 cf

15.0" Round Culvert n=0.013 L=65.0' S=0.1231'/' Outflow=0.9 cfs 3,961 cf

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Pond GS-A: Grassed Swales Pond GS-B: Grassed Swales	Peak Elev=170.69' Storage=2,074 cf Inflow=0.6 cfs 2,074 cf Outflow=0.0 cfs 0 cf
Pond GS-C: Grassed Swales	Peak Elev=196.42' Storage=12,770 cf Inflow=3.8 cfs 12,770 cf Outflow=0.0 cfs 0 cf
Pond GS-D: Grassed Swales	Peak Elev=200.02' Storage=2,332 cf Inflow=0.9 cfs 3,034 cf Outflow=0.0 cfs 755 cf
Pond GS-E: Grassed Swales	Peak Elev=179.75' Storage=3,644 cf Inflow=1.1 cfs 3,644 cf Outflow=0.0 cfs 0 cf
Pond SD: stone diaphragm	Peak Elev=110.02' Storage=209 cf Inflow=1.3 cfs 9,640 cf Outflow=1.4 cfs 9,433 cf
Pond WQS1: WQS1	Peak Elev=143.49' Storage=2,352 cf Inflow=2.2 cfs 11,033 cf Primary=1.5 cfs 10,556 cf Secondary=0.0 cfs 0 cf Outflow=1.5 cfs 10,556 cf
Pond WQS2: WQS2	Peak Elev=143.48' Storage=378 cf Inflow=0.2 cfs 824 cf Primary=0.0 cfs 753 cf Secondary=0.0 cfs 0 cf Outflow=0.0 cfs 753 cf
Pond WQS3: WQS3	Peak Elev=181.88' Storage=1,808 cf Inflow=2.3 cfs 7,580 cf Primary=0.6 cfs 7,444 cf Secondary=0.0 cfs 0 cf Outflow=0.6 cfs 7,444 cf
Pond WQS4: WQS4	Peak Elev=112.49' Storage=997 cf Inflow=2.0 cfs 8,921 cf Primary=1.2 cfs 8,919 cf Secondary=0.0 cfs 0 cf Outflow=1.2 cfs 8,919 cf
Link AP-2A: 36" RCP	Inflow=6.0 cfs 39,261 cf Primary=6.0 cfs 39,261 cf
Link AP-2B: 24" RCP	Inflow=5.2 cfs 28,490 cf Primary=5.2 cfs 28,490 cf
Link AP1: AP-1	Inflow=1.6 cfs 12,127 cf Primary=1.6 cfs 12,127 cf
Link AP3: AP-3	Inflow=0.3 cfs 1,401 cf Primary=0.3 cfs 1,401 cf

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Page 6

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Summary for Subcatchment P1: TO SD

Runoff

0.2 cfs @ 12.17 hrs, Volume=

721 cf, Depth= 0.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

NRCC 24-	NRCC 24-III D 2-16ai Raiman 3-1							
Δre	a (sf)	CN D	escription_					
	370	98 R	Roofs, HSG	Α				
	288	no D	aved narkin	na. HSG A	1 1100 A			
	4,843	39 >	75% Grass	cover, Goo	6d, HSG A			
	0	96 C	Gravel surface	ce, HSG C	M HSG C			
	7,790		75% Grass	Cover, God	Ju, 1150 0			
	2,852		Voods, Goo Gravel surfa	ce HSG A				
	0							
	16,143	64	Meighted Av 95.92% Pen	vious Area				
	15,485		4.08% Impe	rvious Area	ı			
	658	•	4.00 /0 IMPC					
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)		(cfs)				
7.6	75	0.1540			Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"			
7.0					Shallow Concentrated Flow,			
0.2	28	0.1540) 1.96		Woodland Kv= 5.0 fps			
					Shallow Concentrated Flow,			
0.1	46	0.1540	6.32		Uppayed Kv= 16.1 tps			
		0.040	2.16		Shallow Concentrated Flow,			
0.4	55	0.0180	2.10		Unpaved Kv= 16.1 fps			
		Total						
8.3	204	I Qlai						

Summary for Subcatchment P10: TO GS-B

Runoff

0.6 cfs @ 12.12 hrs, Volume=

2,074 cf, Depth= 1.18"

1411002.	–		_
Are	a (s <u>f)</u>	CN	Description
	3,619	74	>75% Grass cover, Good, HSG C
	2,220	96	Gravel surface, HSG C
•	320	98_	Unconnected pavement, HSG C
•	1,159	77	Weighted Average 98.49% Pervious Area
2	0,839 320		1 51% Impervious Area
	320		100.00% Unconnected

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Page 7

Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
3.2	45	0.0667	0.23	•	Sheet Flow,
					Grass: Short n= 0.150 P2= 3.15"
1.8					Direct Entry, MIN. TC = 5.0 MIN
5.0	45	Total			

Summary for Subcatchment P11: TO GS-C

Runoff =

3.8 cfs @ 12.12 hrs, Volume=

12,770 cf, Depth= 1.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

	Αı	rea (sf)	CN	CN Description							
	1	40,163	74	74 >75% Grass cover, Good, HSG C							
		3,993	96	Gravel surfa	ace, HSG C						
		375	70	Woods, Go	od, HSG C						
	1	44,531	75	Weighted A	verage						
	1	44,531		100.00% Pe	ervious Are	a					
٦	ГС	Length	Slope		Capacity	Description					
(mi	<u>n) </u>	(feet)	(ft/ft) (ft/sec)	(cfs)						
0	.4	32	0.0310	1.29		Sheet Flow, GRVL DRV					
						Smooth surfaces n= 0.011 P2= 3.15"					
2	8.	35	0.0570	0.21		Sheet Flow,					
						Grass: Short n= 0.150 P2= 3.15"					
1	.8					Direct Entry, MIN. TC = 5.0 MIN					
5	.0	67	Total								

Summary for Subcatchment P12: TO GS-D

Runoff =

0.9 cfs @ 12.12 hrs, Volume=

3,034 cf, Depth= 1.43"

 Area (sf)	CN	Description
17,020	74	>75% Grass cover, Good, HSG C
7,895	96	Gravel surface, HSG C
442	70	Woods, Good, HSG C
 103	74	>75% Grass cover, Good, HSG C
25,460	81	Weighted Average
25,460		100.00% Pervious Area

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Page 8

_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.3	28	0.0357	1.33	-	Sheet Flow, grvl
						Smooth surfaces n= 0.011 P2= 3.15"
	3.2	31	0.0322	0.16		Sheet Flow,
	۰. ۳	4.0	0.0050			Grass: Short n= 0.150 P2= 3.15"
	0.5	16	0.0050	0.54		Sheet Flow,
	4.0					Smooth surfaces n= 0.011 P2= 3.15"
_	1.0					Direct Entry, 5.0 min.
	5.0	75	Total			

Summary for Subcatchment P13: TO SWL1D

Runoff = 0.7 cfs @ 12.12 hrs, Volume=

2,294 cf, Depth= 1.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

_	Α	rea (sf)	CN Description								
		10,471	74 >75% Grass cover, Good, HSG C								
		6,726	96 Gravel surface, HSG C								
		320			ed pavemer						
		33				ood, HSG C					
		17,550		Neighted A							
		17,230		_	vious Area						
		320	,	1.82% Impe	ervious Are	a					
		320		•	nconnected						
	Tc	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	'					
	0.3	30	0.0630	1.70		Sheet Flow, grvl					
						Smooth surfaces n= 0.011 P2= 3.15"					
	3.3	45	0.0630	0.23		Sheet Flow,					
						Grass: Short n= 0.150 P2= 3.15"					
	0.0	12	0.0630	4.04		Shallow Concentrated Flow,					
						Unpaved Kv= 16.1 fps					
	0.9	240	0.0750	4.41		Shallow Concentrated Flow,					
						Unpaved Kv= 16.1 fps					
_	0.5					Direct Entry, 5.0 min					
	5.0	327	Total		•						

Summary for Subcatchment P14: TO WQS3

Runoff =

2.3 cfs @ 12.12 hrs, Volume=

7,580 cf, Depth= 1.12"

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HydroCAL	<u> </u>	<u>u 0.11. 9 .</u>			
Ar	ea (s <u>f)</u>		Description		
	7,914	96 (Gravel surfa	ce, HSG _C	
•	70,819	74 >	75% Grass	cover, Goo	od, HSG C
	2,271	70 \	Noods, God	d, HSG C	H H G C C
	400		Jnconnecte >75% Grass	d pavemen	od HSG C
	0				50,1100
	81,404	76	Weighted Av 99.51% Per	verage vious ∆rea	
	81,004		99.51% Fei 0.49% Impe	nvious Area	
	400 400	'	100.00% Ur	connected	
	400		100.0070		
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	CDASS
1.0	75	0.0200	1.29		Sheet Flow, GRASS Smooth surfaces n= 0.011 P2= 3.15"
,,,,					Shallow Concentrated Flow,
1.3	175	0.0200	2.28		Unnaved Kv= 16.1 fps
		0.404	ე 5.19		Shallow Concentrated Flow,
0.4	135	0.104	J 5.19		Unpayed Ky= 16.1 fps
0.0					Direct Entry, 5.0 MIN.
2.3		Total			
5.0	385	Total			

Summary for Subcatchment P15: TO CB3

0.7 cfs @ 12.22 hrs, Volume= Runoff

2,908 cf, Depth= 1.12"

1411002		
Area (sf)	CN_	Description
12,202	74	>75% Grass cover, Good, HSG C
4,836	96	Gravel surface, HSG C
14,188	70	Woods, Good, HSG C
0	74	>75% Grass cover, Good, HSG C
31,226 31,226	76	Weighted Average 100.00% Pervious Area

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Page 10

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.5	75	0.0680	0.12		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.15"
1.1	87	0.0680	1.30		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.2	114	0.1500	6.24		Shallow Concentrated Flow,
0.3	114	0.1500	0.24		Unpaved Kv= 16.1 fps
0.2	81	0.1500	6.24		Shallow Concentrated Flow, grvrl
					Unpaved Kv= 16.1 fps
1.0	115	0.1500	1.94		Shallow Concentrated Flow,
0.0	70	0.4000	5.17		Woodland Kv= 5.0 fps Shallow Concentrated Flow,
0.3	78	0.1030	5.17		Unpaved Kv= 16.1 fps
13.4	550	Total		· .	

Summary for Subcatchment P16: TO AP-3

Runoff

0.3 cfs @ 12.25 hrs, Volume=

1,401 cf, Depth= 0.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

			1						
Α	rea (sf)	CN E	escription						
	12,429	70 V	70 Woods, Good, HSG C						
	7,386	74 >	74 >75% Grass cover, Good, HSG C						
	19,815		Veighted A						
	19,815	1	00.00% Pe	ervious Are	a				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
12.5	75	0.0440	0.10		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 3.15"				
1.7	106	0.0440	1.05		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
0.6	78	0.1790	2.12		Shallow Concentrated Flow, Woodland Kv= 5.0 fps				
				<u></u>	woodiand itv- 5.0 ips				
14.8	259	Total							

Summary for Subcatchment P17: TO GS-E

Runoff =

1.1 cfs @ 12.12 hrs, Volume=

3,644 cf, Depth= 1.00"

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Page 11

A	rea (sf)	CN [Description						
	43,526	74 >	74 >75% Grass cover, Good, HSG C						
	0	74 >	75% Gras	s cover, Go	ood, HSG C				
	43,526	74 V	Veighted A	verage					
	43,526	1	00.00% Pe	ervious Are	a				
Tç	Length	Slope	Velocity	Capacity	Description				
(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)					
0.6	75	0.0800	2.24		Sheet Flow, GRVL DRV				
					Smooth surfaces n= 0.011 P2= 3.15"				
0.3	49	0.0310	2.83		Shallow Concentrated Flow, GRVL DRV				
					Unpaved Kv= 16.1 fps				
0.5	60	0.0170	2.10		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
3.6					Direct Entry, 5.0 MIN				
5.0	184	Total							

Summary for Subcatchment P18: TO SWL2

Runoff =

0.1 cfs @ 12.12 hrs, Volume=

269 cf, Depth= 1.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

A	rea (sf)	CN D	Description					
	3,212	74 >	>75% Grass cover, Good, HSG C					
	3,212	1	00.00% Pe	ervious Are	a			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
5.0					Direct Entry, 5.0 MIN			

Summary for Subcatchment P19: TO WQS2

Runoff =

0.2 cfs @ 12.12 hrs, Volume=

555 cf, Depth= 1.00"

 Area (sf)	CN	Description	
6,629	74	>75% Grass cover, Good, HSG C	
6,629		100.00% Pervious Area	

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 2-Year Rainfall=3.15"

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Page 12

<u>HydroCAl</u>	O <u>® 10.10-</u>	4a_s/n_u_i	036 @ 202	<u> </u>	
	Length	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
<u>(min)</u> 1.5	(feet)_ 31	0.2260	0.35		Sheet Flow, Grass: Short n= 0.150 P2= 3.15"
• • • •					Direct Entry, MIN TC = 5.0 MIN
3.5		Tatal			
5.0	31	Total			

Summary for Subcatchment P2: TO WQS4

Runoff

1.5 cfs @ 12.17 hrs, Volume=

6,014 cf, Depth= 0.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

NRCC 24-hr D 2-	Year Rain	1ali-3.13		
Area (sf) 55,955 13,098 6,831 75,884 75,884	70 W 74 >7 96 G	ravel surfa /eighted A\	cover, Go ce, HSG C	
Tc Length (min) <u>(feet)</u>	7.21 (F1)	Velocity (ft/sec)	Capacity (cfs)	Sheet Flow,
7.4 75	0.1660	0.17		Woods: Light underbrush n= 0.400 P2= 3.13
0.4 55	0.1660	2.04		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
1.5 142	0.0950	1.54		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.0 13	0.3300	9.25		Shallow Concentrated Flow, Unpaved Ky= 16.1 fps
9.3 28	5 Total			

Summary for Subcatchment P3: TO AP1

Runoff

0.8 cfs @ 12.14 hrs, Volume=

2,694 cf, Depth= 1.64"

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Summary for Subcatchment P4: TO CB2

Runoff = 1.0 cfs @ 12.26 hrs, Volume=

4,947 cf, Depth= 0.90"

 Area (sf) 36,514 29,013 525 66,052 66,052	74 70 96 72	Description >75% Grass cover, Good, HSG C Woods, Good, HSG C Gravel surface, HSG C Weighted Average 100.00% Pervious Area
66,052		100.00% Pervious Area

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Page <u>14</u>

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
8.3	40	0.0350	0.08		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"			
3.4	35	0.0350	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 3.15"			
2.3	290	0.0170	2.10		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
0.4	90	0.0560	3.81		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
1.4	105	0.0670	1.29		Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
0.5	211	0.1660	6.56		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
0.1	53	0.1510	6.26		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
16.4	824	Total						

Summary for Subcatchment P5A: TO EX.36"

4.0 cfs @ 12.26 hrs, Volume= Runoff

20,510 cf, Depth= 0.90"

MIXOU Z4 III D Z	,	
Area (sf)	CN	Description
0	96	Gravel surface, HSG C
187,867 75,981 9,587 400	70 74 98 98	Woods, Good, HSG C >75% Grass cover, Good, HSG C Paved parking, HSG C Unconnected pavement, HSG C
273,835 263,848 9,987 400	72	Weighted Average 96.35% Pervious Area 3.65% Impervious Area 4.01% Unconnected

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Page 15

To <u>(min</u>		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.1	1 27	0.3300	0.40		Sheet Flow,
_					Grass: Short n= 0.150 P2= 3.15"
8.4	48	0.0490	0.10		Sheet Flow,
0.0		0.0400	4.44		Woods: Light underbrush n= 0.400 P2= 3.15"
3.0	3 54	0.0490	1.11		Shallow Concentrated Flow,
1.6	6 130	0.0770	1.39		Woodland Kv= 5.0 fps Shallow Concentrated Flow,
1.0	, 100	0.0770	1.00		Woodland Kv= 5.0 fps
2.5	305	0.1640	2.02		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.1	l 127	0.0390	0.99		Shallow Concentrated Flow,
_					Woodland Kv= 5.0 fps
16.5	5 691	Total			

Summary for Subcatchment P5B: TO EX.24"

Runoff = 5.2 cfs @ 12.30 hrs, Volume=

28,492 cf, Depth= 0.95"

Area (sf)	CN	Description
5,494	96	Gravel surface, HSG C
277,852	70	Woods, Good, HSG C
52,653	74	>75% Grass cover, Good, HSG C
20,671	98	Paved parking, HSG C
2,721	98	Roofs, HSG C
139	74	>75% Grass cover, Good, HSG C
359,530	73	Weighted Average
336,138		93.49% Pervious Area
23,392		6.51% Impervious Area

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Page 16

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.1	57	0.3300	0.46		Sheet Flow,
2.0	10	0.0500	0.45		Grass: Short n= 0.150 P2= 3.15"
2.0	18	0.2500	0.15		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.15"
0.3	52	0.2500	2.50		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
5.9	209	0.0140	0.59		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
5.5	221	0.0180	0.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.4	117	0.0260	0.81		Shallow Concentrated Flow,
		0.0200	0.0.		Woodland Kv= 5.0 fps
1.4	109	0.0700	1.32		Shallow Concentrated Flow,
1.4	103	0.0700	1.02		•
					Woodland Kv= 5.0 fps
19.6	783	Total			

Summary for Subcatchment P6: TO WQS1

Runoff =

0.5 cfs @ 12.12 hrs, Volume=

1,847 cf, Depth= 1.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

_	A	rea (sf)	CN	Description							
		21,626	74	>75% Grass cover, Good, HSG C							
_		438	96	Gravel surface, HSG C							
		22,064	74	Weighted Average							
		22,064 100.00% Pervious Area									
	Тс	Length	Slope		Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	1.8	35	0.1700	0.32		Sheet Flow,					
						Grass: Short n= 0.150 P2= 3.15"					
_	3.2					Direct Entry, MIN. TC = 5.0 MIN					
	5.0	35	Total								

Summary for Subcatchment P7: TO GS-A

Runoff =

1.5 cfs @ 12.12 hrs, Volume=

5,166 cf, Depth= 1.00"

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А	rea (sf)	CN Description								
	60,550	74 >		s cover, Go	ood, HSG C					
	1,152	96 G	ravel surfa	ace, HSG C						
	0	98 <u>L</u>	Inconnecte	d pavemer	nt, HSG C					
	61.702		Veighted A							
	61,702	1	00.00% Pe	ervious Are	a					
				0 :1	Description					
Tc	Length	Slope	Velocity	Capacity	Description					
<u>(min)</u>	(feet)	<u>(ft/ft)</u>	(ft/sec)	(cfs)	ODVI DOV					
0.5	75	0.1050	2.50		Sheet Flow, GRVL DRV					
					Smooth surfaces n= 0.011 P2= 3.15"					
0.1	39	0.1050	5.22		Shallow Concentrated Flow, GRVL DRV					
			- 00		Unpaved Kv= 16.1 fps Shallow Concentrated Flow, GRVL DRV					
0.1	30	0.1000	5.09		Unpaved Kv= 16.1 fps					
		0.0700	4.00		Shallow Concentrated Flow, GRVL DRV					
0.3	86	0.0700	4.26		Hanning Wy 16 1 fpc					

Summary for Subcatchment P8: TO CB1

Unpaved Kv= 16.1 fps
Shallow Concentrated Flow,

Unpaved Kv= 16.1 fps
Shallow Concentrated Flow,

Unpaved Kv= 16.1 fps

Direct Entry, MIN TC = 5.0 MIN

Runoff = 0.1 cfs @ 12.12 hrs, Volume=

9.29

6.30

19 0.3330

59 0.1530

Total

308

0.0

0.2

3.8

5.0

277 cf, Depth= 1.00"

A	rea (sf)		escription		1,1100,0				
	3,312 74 >75% Grass cover, Good, HSG C								
	3,312	100.00% Pervious Area							
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cf <u>s)</u>	Description				
3.9	75	0.1180	0.32	-	Sheet Flow,				
0.1	, -	0.1180	5.53		Grass: Short n= 0.150 P2= 3.15" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
1.0	_				Direct Entry, MIN. TC = 5.0 MIN				
5.0	119	Total							

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Page 18

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Summary for Subcatchment P9: TO HW#1

Runoff

0.3 cfs @ 12.12 hrs, Volume=

913 cf, Depth= 1.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 2-Year Rainfall=3.15"

А	rea (sf)	CN D	Description							
	3,729	74 >	>75% Grass cover, Good, HSG C							
	0			d pavemer						
	2,728			ace, HSG C						
 -	220	<u>98</u> L	<u>Inconnecte</u>	<u>d pavemer</u>	nt, HSG <u>C</u>					
	6,677		Veighted A	•						
	6,457	-	* * * * * * * * * * * * * * * * * * * *	vious Area						
	220		•	ervious Area						
	220	1	00.00% U	nconnected						
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
0.5	75	0.0950	2.40		Sheet Flow, GRVL DRV					
					Smooth surfaces n= 0.011 P2= 3.15"					
0.2	61	0.0660	4.14		Shallow Concentrated Flow, GRVL DRV					
		0.4400	0.00		Unpaved Kv= 16.1 fps					
0.1	28	0.1430	6.09		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps					
0.0	100	0.2040	7.27		Shallow Concentrated Flow,					
0.2	103	0.2040	1.21		Unpaved Kv= 16.1 fps					
4.0					Direct Entry, MIN. TC = 5.0 MIN					
5.0	267	Total	 ··							

Summary for Reach OF: TO WREP

31,226 sf, 0.00% Impervious, Inflow Depth = 1.12" for 2-Year event Inflow Area =

0.7 cfs @ 12.22 hrs, Volume= 2,908 cf Inflow

2,908 cf, Atten= 4%, Lag= 2.2 min 0.6 cfs @ 12.26 hrs, Volume= Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.02 fps, Min. Travel Time= 2.9 min Avg. Velocity = 0.60 fps, Avg. Travel Time= 5.0 min

Peak Storage= 111 cf @ 12.26 hrs

Average Depth at Peak Storage= 0.05', Surface Width= 14.91' Bank-Full Depth= 2.00' Flow Area= 220.0 sf, Capacity= 1,899.8 cfs

10.00' x 2.00' deep channel, n= 0.035 Earth, dense weeds

Side Slope Z-value= 50.0 '/' Top Width= 210.00'

Length= 180.0' Slope= 0.0389 '/'

Inlet Invert= 129.00', Outlet Invert= 122.00'

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 2-Year Rainfall=3.15"

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Page 19

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Summary for Reach OF2: FROM WREP

Inflow Area =

31,226 sf, 0.00% Impervious, Inflow Depth = 1.12" for 2-Year event 2.908 cf

Inflow

Outflow

0.6 cfs @ 12.26 hrs, Volume= 0.6 cfs @ 12.27 hrs, Volume=

2,908 cf. Atten= 0%, Lag= 0.6 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.62 fps, Min. Travel Time= 0.8 min

Avg. Velocity = 1.27 fps, Avg. Travel Time= 1.6 min

Peak Storage= 30 cf @ 12.27 hrs

Average Depth at Peak Storage= 0.28', Surface Width= 1.70'

Bank-Full Depth= 2.00' Flow Area= 12.0 sf, Capacity= 115.9 cfs

0.00' x 2.00' deep channel, n= 0.035 Earth, dense weeds

Side Slope Z-value= 3.0 '/' Top Width= 12.00'

Length= 126.0' Slope= 0.0556 '/'

Inlet Invert= 122.00', Outlet Invert= 115.00'

Summary for Reach SWL1A:

Inflow Area =

280,391 sf, 0.31% Impervious, Inflow Depth = 0.18" for 2-Year event

Inflow

1.0 cfs @ 12.14 hrs, Volume=

4,238 cf

Outflow

1.0 cfs @ 12.14 hrs, Volume=

4,238 cf, Atten= 0%, Lag= 0.6 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.47 fps, Min. Travel Time= 0.8 min

Avg. Velocity = 1.25 fps, Avg. Travel Time= 2.1 min

Peak Storage= 46 cf @ 12.14 hrs

Average Depth at Peak Storage= 0.12', Surface Width= 2.74'

Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 263.5 cfs

2.00' x 2.00' deep channel, n= 0.035

Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 157.0' Slope= 0.1338 '/'

Inlet Invert= 166.00', Outlet Invert= 145.00'

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Page 20



Summary for Reach SWL1B:

Inflow Area = 215,377 sf, 0.40% Impervious, Inflow Depth = 0.22" for 2-Year event

Inflow = 0.9 cfs @ 12.14 hrs, Volume= 3,961 cf

Outflow = 0.9 cfs @ 12.14 hrs, Volume= 3,961 cf, Atten= 0%, Lag= 0.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.85 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.46 fps, Avg. Travel Time= 0.2 min

Peak Storage= 5 cf @ 12.14 hrs

Average Depth at Peak Storage= 0.11', Surface Width= 2.63' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 322.2 cfs

2.00' x 2.00' deep channel, n= 0.035

Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 20.0' Slope= 0.2000 '/'

Inlet Invert= 170.00', Outlet Invert= 166.00'



Summary for Reach SWL1C:

Inflow Area = 187,541 sf, 0.17% Impervious, Inflow Depth = 0.20" for 2-Year event

Inflow = 0.7 cfs @ 12.12 hrs, Volume= 3,048 cf

Outflow = 0.7 cfs @ 12.14 hrs, Volume= 3,048 cf, Atten= 3%, Lag= 1.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.47 fps, Min. Travel Time= 2.0 min Avg. Velocity = 0.93 fps, Avg. Travel Time= 5.4 min

Peak Storage= 82 cf @ 12.14 hrs

Average Depth at Peak Storage= 0.12', Surface Width= 2.69'

Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 194.8 cfs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 2-Year Rainfall=3.15" Printed 8/16/2021

181084-POST-REV 1.1

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Page 21

2.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 14.00' Length= 301.0' Slope= 0.0731 '/' Inlet Invert= 196.00', Outlet Invert= 174.00'



Summary for Reach SWL1D:

43,010 sf, 0.74% Impervious, Inflow Depth = 0.85" for 2-Year event Inflow Area =

3.048 cf 0.7 cfs @ 12.12 hrs, Volume=

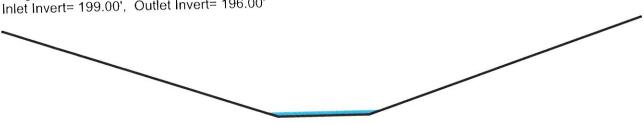
Inflow 3,048 cf, Atten= 1%, Lag= 0.2 min 0.7 cfs @ 12.12 hrs, Volume= Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.92 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.13 fps, Avg. Travel Time= 0.4 min

Peak Storage= 6 cf @ 12.12 hrs Average Depth at Peak Storage= 0.10', Surface Width= 2.62' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 249.6 cfs

2.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 14.00' Length= 25.0' Slope= 0.1200 '/' Inlet Invert= 199.00', Outlet Invert= 196.00'



Summary for Reach SWL2:

46,738 sf, 0.00% Impervious, Inflow Depth = 0.07" for 2-Year event Inflow Area =

0.1 cfs @ 12.12 hrs, Volume= 269 cf Inflow

269 cf, Atten= 5%, Lag= 1.6 min 0.1 cfs @ 12.15 hrs, Volume= Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.10 fps, Min. Travel Time= 2.1 min Avg. Velocity = 1.03 fps, Avg. Travel Time= 4.3 min

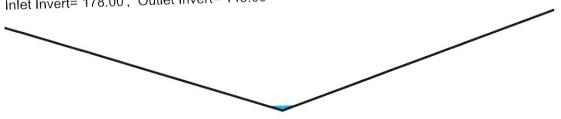
Peak Storage= 10 cf @ 12.15 hrs

Average Depth at Peak Storage= 0.11', Surface Width= 0.65' Bank-Full Depth= 2.00' Flow Area= 12.0 sf, Capacity= 173.6 cfs

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Page 22

0.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 12.00' Length= 265.0' Slope= 0.1245 '/' Inlet Invert= 178.00', Outlet Invert= 145.00'



Summary for Pond 24"-RCP: EX. 24" CULV

359,530 sf, 6.51% Impervious, Inflow Depth = 0.95" for 2-Year event Inflow Area = 5.2 cfs @ 12.30 hrs, Volume= 28,492 cf 28,490 cf, Atten= 0%, Lag= 0.0 min Inflow 5.2 cfs @ 12.31 hrs, Volume= = Outflow 5.2 cfs @ 12.31 hrs, Volume= 28,490 cf Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 99.51' @ 12.31 hrs Surf.Area= 27 sf Storage= 17 cf

Plug-Flow detention time= 0.1 min calculated for 28,470 cf (100% of inflow) Center-of-Mass det. time= 0.1 min (913.0 - 912.9)

Volume #1	Invert 98.00'	Avail.Stor 4,90	age 9 cf	Storage Description Custom Stage Data			-
Elevation (feet) 98.00 99.00 100.00 101.00 102.00 103.00 104.00 105.00	1,	1-ft) 1 15 42 79 189 809 937	erim. (feet) 3.0 22.0 31.0 37.0 60.0 120.0 205.0 302.0	Inc.Store (cubic-feet) 0 7 27 60 130 463 1,333 2,890	Cum.Store (cubic-feet) 0 7 34 94 224 687 2,019 4,909	Wet.Area (sq-ft) 1 41 87 134 318 1,182 3,387 7,308	
2011	outing imary	Invert 98.54'	36.0	let Devices " Round Culvert 31.0' CMP, projection	g, no headwall, k	(e= 0.900 0062 '/'	

L= 81.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 98.54' / 98.04' S= 0.0062 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=5.2 cfs @ 12.31 hrs HW=99.50' TW=0.00' (Dynamic Tailwater)
1=Culvert (Inlet Controls 5.2 cfs @ 2.64 fps)

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Summary for Pond 36"-RCP: EX. 36" CULV

777,113 sf, 1.45% Impervious, Inflow Depth = 0.61" for 2-Year event Inflow Area =

6.0 cfs @ 12.28 hrs, Volume= 39,263 cf Inflow

39,261 cf, Atten= 0%, Lag= 0.0 min 6.0 cfs @ 12.28 hrs, Volume= Outflow

39,261 cf 6.0 cfs @ 12.28 hrs, Volume= Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Peak Elev= 110.83' @ 12.28 hrs Surf.Area= 9 sf Storage= 8 cf

Plug-Flow detention time= 0.1 min calculated for 39,234 cf (100% of inflow)

Center-of-Mass det. time= 0.0 min (965.9 - 965.9)

<u>/olume</u> #1	Invert 109.00'		412 cf	Custom Stage Da	ta (Irregular)Listed	d below (Recalc)
Elevation (feet)		.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft) 1
109.00 110.00 111.00		1 4 10 18	4.0 9.0 15.0 19.0	0 2 7 14	2 9 23	9 26 46
112.00 113.00 114.00 115.00		43 165 372	27.0 52.0 74.0	30 97 262	53 150 412	83 245 475

Routing Device 36.0" Round Culvert 109.79 #1 Primary

L= 57.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 109.79' / 109.02' S= 0.0135 '/' Cc= 0.900

n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=5.9 cfs @ 12.28 hrs HW=110.82' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 5.9 cfs @ 2.73 fps)

Summary for Pond CB1:

3,312 sf, 0.00% Impervious, Inflow Depth = 1.00" for 2-Year event Inflow Area = 277 cf

0.1 cfs @ 12.12 hrs, Volume= Inflow

277 cf, Atten= 0%, Lag= 0.0 min 0.1 cfs @ 12.11 hrs, Volume= Outflow

277 cf 0.1 cfs @ 12.11 hrs, Volume= Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 166.12' @ 12.19 hrs

Device #1	Routing Primary	164.00'	Outlet Devices 12.0" Round Culvert L= 62.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 164.00' / 163.50' S= 0.0081 '/' Cc= 0.900
			Inlet / Outlet invert= 104.00 / 100.00

Inlet / Outlet Invert= 164.00' / 163.50' S= 0.0081 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

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Page 24

Primary OutFlow Max=0.0 cfs @ 12.11 hrs HW=166.10' TW=166.12' (Dynamic Tailwater) 1=Culvert (Controls 0.0 cfs)

Summary for Pond CB2:

Inflow Area = 66,052 sf, 0.00% Impervious, Inflow Depth = 0.90" for 2-Year event
Inflow = 1.0 cfs @ 12.26 hrs, Volume= 4,947 cf
Outflow = 1.0 cfs @ 12.26 hrs, Volume= 4,947 cf, Atten= 0%, Lag= 0.0 min
Primary = 1.0 cfs @ 12.26 hrs, Volume= 4,947 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 148.00' @ 0.00 hrs Surf.Area= 3 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume #1	Invert 148.00'	Avail.	Storage 119 cf	Storage Descriptio Custom Stage Da		ed below	<u></u>
Elevation (feet)	Sı	urf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
148.00 149.00 150.00		3 50 154	6.0 25.0 44.0	0 22 97	0 22 119	3 52 162	
	outing rimary	Inv 144.:	30' 15.0 L= 2	et Devices " Round Culvert 64.0' CMP, projec / Outlet Invert= 144 0.013 Corrugated P	1,30' / 143.00' S=	= 0.0049 '/' Cc= ().900 3 sf

Primary OutFlow Max=0.0 cfs @ 12.26 hrs HW=148.00' TW=143.48' (Dynamic Tailwater) 1=Culvert (Passes 0.0 cfs of 6.7 cfs potential flow)

Summary for Pond CB3:

Inflow Area = Inflow = Outflow = Primary =	0.7 cfs @ 0.7 cfs @	0.00% Impervious, 12.22 hrs, Volume= 12.22 hrs, Volume= 12.22 hrs, Volume=	2,908 cf, Atten= 0%, Lag= 0.0 min
--------------------------------------------	------------------------	-------------------------------------------------------------------------------------	-----------------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 129.17' @ 12.23 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 34.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 128.50' / 128.10' S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

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Page 25

Primary OutFlow Max=0.6 cfs @ 12.22 hrs HW=129.16' TW=129.05' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.6 cfs @ 1.60 fps)

Summary for Pond CLV1: HW#1

194,218 sf, 0.28% Impervious, Inflow Depth = 0.24" for 2-Year event Inflow Area = 0.9 cfs @ 12.14 hrs, Volume= 3,961 cf Inflow 3,961 cf, Atten= 0%, Lag= 0.0 min 0.9 cfs @ 12.14 hrs, Volume= Outflow 0.9 cfs @ 12.14 hrs, Volume= 3,961 cf Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 174.00' @ 0.00 hrs Surf.Area= 274 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 0.0 min (929.2 - 929.2)

Volume	Invert 174.00'	Avai	.Storage 1,585 cf	Storage Description Custom Stage Da		ed below	
Elevation (feet)		rf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
174.00 175.00 176.00 177.00		274 583 583 583	91.0 126.0 126.0 126.0	0 419 583 583	0 419 1,002 1,585	274 888 1,014 1,140	
	outing rimary	<u>In</u> 173	.00' 15.0	et Devices " Round Culvert 5.0' CMP, projectir / Outlet Invert= 173	ng, no headwall, 3.00' / 165.00' S=	Ke= 0.900 = 0.1231 '/' Cc= 0.900	

Inlet / Outlet Invert= 173.00' / 165.00' S= 0.1231 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.0 cfs @ 12.14 hrs HW=174.00' TW=170.10' (Dynamic Tailwater) -1=Culvert (Passes 0.0 cfs of 2.8 cfs potential flow)

Summary for Pond GS-A: Grassed Swales

Outflow	=	1.5 cfs @ 0.0 cfs @	0.00% Impervious, 12.12 hrs, Volume= 0.00 hrs, Volume= 0.00 hrs, Volume=	0 cf, Atten= 100%, Lag= 0.0 min
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 166.33' @ 24.35 hrs Surf.Area= 10,414 sf Storage= 5,166 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

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Printed 8/16/2021 Page 26

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Volume	Inve	Invert Avail.Storage Storage Description					
#1	165.5	0' 24,03	32 cf Custor	n Stage Data (Co	nic)Listed below	x 4	
Elevatio (fee 165.5 166.0 166.5 167.0 167.5	60 60 60 60	Surf.Area (sq-ft) 434 1,736 3,038 4,340 5,642	Inc.Store (cubic-feet) 0 506 1,178 1,835 2,488	Cum.Store (cubic-feet) 0 506 1,685 3,520 6,008	Wet.Area (sq-ft) 434 1,737 3,042 4,348 5,656		
Device	Routing	Invert	Outlet Devic	es			
#1	Primary	167.00'	6.0' long x 2.0' breadth Broad-Crested Rectangular Weir X 4.06 Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.0 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32				

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=165.50' TW=166.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond GS-B: Grassed Swales

Inflow Area = 21,159 Inflow = 0.6 cfs (Outflow = 0.0 cfs (Primary = 0.0 cfs (The same and the s	low Depth = 1.18" for 2-Year event 2,074 cf 0 cf, Atten= 100%, Lag= 0.0 min 0 cf
---------------------------------------------------------------------------------	--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	-------------------------------------------------------------------------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 170.69' @ 24.35 hrs Surf.Area= 3,001 sf Storage= 2,074 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert A	vail.Storage		Description		
#1	169.50'	5,152 cf	Custom	i Stage Data (Pr	r ismatic) Listed belo	JW X Z
Elevation (feet)	Surf.Are (sq-		c.Store ic-feet)	Cum.Store (cubic-feet)		
169.50 170.00 170.50 171.00 171.50		40	0 230 506 782 1,058	0 230 736 1,518 2,576		
Davisa P	outing	Invert Out	let Device	es		

Invert Device Routing 6.0' long x 2.0' breadth Broad-Crested Rectangular Weir X 2.00 171.00' Primary #1 Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88

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Page 27

2.85 3.07 3.20 3.32

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=169.50' TW=170.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond GS-C: Grassed Swales

Inflow Area = 144,531 sf, 0.00% Impervious, Inflow Depth = 1.06" for 2-Year event

Inflow = 3.8 cfs @ 12.12 hrs, Volume= 12,770 cf

Outflow = 0.0 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 100%, Lag= 0.0 min

Primary = 0.0 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 196.42' @ 24.35 hrs Surf.Area= 23,358 sf Storage= 12,770 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	lnv	ert Avail.Sto	rage Storage [Description	
#1	195.	50' 50,0	64 cf Custom	Stage Data (Pr	rismatic)Listed below x 8
Elevatio		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
195.5 196.0 196.5 197.0	00 50 00	447 1,788 3,129 4,470 5,811	0 559 1,229 1,900 2,570	0 559 1,788 3,688 6,258	
Device	Routing	Invert	Outlet Devices		
#1	Primary	197.00'	Head (feet) 0. 2.50 3.00 3.5	20 0.40 0.60 0) 2.54 2.61 2.	ad-Crested Rectangular Weir X 7.00 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=195.50' TW=196.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond GS-D: Grassed Swales

Inflow Area =	25,460 sf, 0.00% Impervious,	Inflow Depth = 1.43" for 2-Year event
Inflow =	0.9 cfs @ 12.12 hrs, Volume=	3,034 cf
Outflow =	0.0 cfs @ 17.35 hrs, Volume=	
Primary =	0.0 cfs @ 17.35 hrs, Volume=	755 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 200.02' @ 17.35 hrs Surf.Area= 2.838 sf Storage= 2.332 cf

Plug-Flow detention time= 525.3 min calculated for 755 cf (25% of inflow)

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Page 28

Center-of-Mass det. time= 350.8 min (1,217.3 - 866.5)

Center-or-w	1000 0011					
Volume	Invert 198.50'	Avail.Stora 3,89	age Storage I 0 cf Custom	Description Stage Data (Conic		
Elevation (feet) 198.50 199.00 199.50 200.00 200.50	Su	1rf.Area (sq-ft) 281 1,124 1,967 2,810 3,653	Inc.Store (cubic-feet) 0 328 763 1,188 1,611	Cum.Store (cubic-feet) 0 328 1,091 2,279 3,890	Wet.Area (sq-ft) 281 1,125 1,971 2,818 3,667	
	Routing Primary	Invert 200.00'	Head (feet)(.0' breadth Broad 0.20 0.40 0.60 0.8 50 h) 2.54 2.61 2.61 20 3.32	-Crested Rectangula 30 1.00 1.20 1.40 1 2.60 2.66 2.70 2.7	77 2.89 2.88

Primary OutFlow Max=0.0 cfs @ 17.35 hrs HW=200.02' TW=199.02' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.0 cfs @ 0.33 fps)

Summary for Pond GS-E: Grassed Swales

Inflow Area : Inflow Outflow Primary	= 1.1 = 0.0	1 cfs @ 0 cfs @	12.12 hrs,	Volume= Volume=	epth = - 3,644 cf 0 cf 0 c	f, Atte	for 2-Year n= 100%, L	event .ag= 0.0 min
					 	مم مداحا		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 179.75' @ 24.35 hrs Surf.Area= 6,664 sf Storage= 3,644 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Center-or w				
Volume	Invert Av. 178.50'	ail.Storage 10,496 cf	Storage D Custom S	escription Stage Data (Prismatic)Listed below x 9
Elevation	Surf.Area	,	.Store	Cum.Store

Elevation	Surf.Area	Inc.Store	Cum Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
178.50	75	0	0
179.00	135	53	53
179.50	540	169	221
180.00	945	371	593
180.50	1,350	574	1,166

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2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=178.50' TW=178.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond SD: stone diaphragm

Inflow Area = 123,253 sf, 0.53% Impervious, Inflow Depth = 0.94" for 2-Year event
Inflow = 1.3 cfs @ 12.34 hrs, Volume= 9,640 cf
Outflow = 1.4 cfs @ 12.35 hrs, Volume= 9,433 cf, Atten= 0%, Lag= 0.5 min
Primary = 1.4 cfs @ 12.35 hrs, Volume= 9,433 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 110.02' @ 12.35 hrs Surf.Area= 200 sf Storage= 209 cf Flood Elev= 110.50' Surf.Area= 200 sf Storage= 247 cf

Plug-Flow detention time= 16.7 min calculated for 9,426 cf (98% of inflow) Center-of-Mass det. time= 5.3 min (917.6 - 912.3)

Volume #1 #2	Invert 108.00' 108.30'	169 cf	Storage Description Custom Stage Data (Prismatic)Listed below (Recalc) 500 cf Overall - 79 cf Embedded = 421 cf x 40.0% Voids 12.0" Round Pipe Storage Inside #1 L= 100.0'
	<u> </u>	247 cf	Total Available Storage

Elevation	Surf.Area	Inc.Store	Cum.Store (cubic-feet)
(feet)	(sq-ft)	(cubic-feet)	
108.00	200	0	0
110.50	200	500	500

Device Routing #1 Primary	110.00'	Outlet Devices 195.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32
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Primary OutFlow Max=1.4 cfs @ 12.35 hrs HW=110.02' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 1.4 cfs @ 0.37 fps)

Summary for Pond WQS1: WQS1

Inflow = 2.2 cfs @ Outflow = 1.5 cfs @ 1.5 cfs @ 1.5 cfs @	0.23% Impervious, 12.16 hrs, Volume= 12.32 hrs, Volume= 12.32 hrs, Volume= 0.00 hrs, Volume=	10,556 cf, Alleri 35%, Lag 3.0 min
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Page 30

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 143.49' @ 12.32 hrs Surf.Area= 5,570 sf Storage= 2,352 cf Flood Elev= 143.10' Surf.Area= 4,391 sf Storage= 425 cf

Plug-Flow detention time= 180.1 min calculated for 10,556 cf (96% of inflow) Center-of-Mass det. time= 157.1 min (1,073.8 - 916.7)

Volume	Invert	Avail.S	torage	Storage Description		
#1	143.00'	14	,736 cf	Custom Stage Data	a (Irregular)Listed	below (Recalc)
Elevatio (fee	• •	urf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
143.0		4,110	838.0	0	0 5,648	4,110 7,599
144.0		7,342	863.0	5,648	· · · · · · · · · · · · · · · · · · ·	10,378
145.0	0	10,953	882.0	9,088	14,736	10,370
Device	Routing	Inve		et Devices		14 0 500
#1	Primary	139.50	Inlet	" Round Culvert Ol / Outlet Invert= 139.	50' / 136.50' S= 0	.0261 '/' Cc= 0.900
				.013 Corrugated PE	, smooth interior, t	-low Area= 1.23 si
#2	Device 1	143.10		Vert. LOW FLOW C		
			Limi	ted to weir flow at lov	v neads Novicipe CoatMe	ID C= 0.600
#3	Device 1	143.4		" x 48.0" Horiz. TOF		IR C= 0.000
			Limi	ted to weir flow at lov	v neads	CDII UMAV
#4	Secondary	144.5	0' 10.0	' long x 10.0' bread	ITH EMERGENCY	O 1 40 1 60
			Hea	d (feet) 0.20 0.40 0),60 0,80 1.00 1.4 30 0.70 0.60 0.69	20 1.40 1.00
			Coe	f. (English) 2.49 2.5	00 2.70 2.09 2.00	2.09 2.01 2.04

Primary OutFlow Max=1.5 cfs @ 12.32 hrs HW=143.49' TW=110.81' (Dynamic Tailwater)
1=Culvert OUTLET (Passes 1.5 cfs of 10.8 cfs potential flow)
-2=LOW FLOW OUTLET (Orifice Controls 0.1 cfs @ 2.46 fps)
-3=TOP OVERFLOW WEIR (Weir Controls 1.3 cfs @ 0.96 fps)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=143.00' TW=109.00' (Dynamic Tailwater) T-4=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS2: WQS2

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 143.48' @ 14.84 hrs Surf.Area= 932 sf Storage= 378 cf Flood Elev= 143.10' Surf.Area= 712 sf Storage= 69 cf

Plug-Flow detention time= 352.2 min calculated for 752 cf (91% of inflow) Center-of-Mass det. time= 310.0 min (1,206.4 - 896.4)

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Page 31

Volume_	Invert	Avail.Stor	age_	Storage Description		Lalaw (Boods)
#1	143.00'		'5 cf	Custom Stage Data	a (Irregular)Listed I	below (Recalc)
Elevation (feet 143.0 144.0	t) 0 0	(sq-ft) 659 1,283	erim. (feet) 196.0 225.0 251.0	Inc.Store (cubic-feet) 0 954 1,621	Cum.Store (cubic-feet) 0 954 2,575	Wet,Area (sq-ft) 659 1,653 2,666
145.0	U	1,904	201.0	,		
Device_	Routing	Invert	Outl	et Devices " Round Culvert O	UT: ET 1 = 35.1' k	(e= 0.500
#1	Primary	141.25'	Inlet	t / Outlet Invert= 141. 2 013 Corrugated PE	25' / 139.50' S= 0 smooth interior, l	Flow Area= 1.23 sf
#2	Device 1	143.10'	1.0"	' Vert. LOW FLOW C	N heads	
#3	Device 1	143.65'	1:00	o" x 48.0" Horiz. TOI ited to weir flow at lo	w heads	
#4	Secondar	y 144.50'		lined to well flow dictors lined to well flow dictors ad (feet) 0.20 0.40 (ef. (English) 2.49 2.5	TAN NEU LUUL.	/() 1.40 1.00
					TM-110 16' (Dvn:	amic Tailwater)

Primary OutFlow Max=0.0 cfs @ 14.84 hrs HW=143.48' TW=110.16' (Dynamic Tailwater)
1=Culvert OUTLET (Passes 0.0 cfs of 7.5 cfs potential flow)

-2=LOW FLOW OUTLET (Orifice Controls 0.0 cfs @ 2.79 fps)

-3=TOP OVERFLOW WEIR (Controls 0.0 cfs)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=143.00' TW=109.00' (Dynamic Tailwater) —4=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS3: WQS3

Inflow = 2.3 cfs @ Outflow = 0.6 cfs @ Outflow = 0.6 cfs @	, 0.49% Impervious, 12.12 hrs, Volume= 12.39 hrs, Volume= 12.39 hrs, Volume= 0.00 hrs, Volume=	7,444 cf
------------------------------------------------------------	------------------------------------------------------------------------------------------------------------	----------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 181.88' @ 12.39 hrs Surf.Area= 2,976 sf Storage= 1,808 cf Flood Elev= 181.10' Surf.Area= 1,420 sf Storage= 134 cf

Plug-Flow detention time= 53.8 min calculated for 7,444 cf (98% of inflow) Center-of-Mass det. time= 43.7 min (930.7 - 887.0)

00			
Volume	Invert	Avail.Storage	Storage Description Custom Stage Data (Irregular)Listed below (Recalc)
#1	181.00'	17,330 cf	

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Printed 8/16/2021 _____Page 32

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Elevation	Surf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area
(feet)	(sg-ft)	(feet)	(cubic-fe <u>et)</u>	(cubic-feet)	(sq-ft)
181.00	1,261	147.0	0	0	1,261
182.00	3,271	245.0	2,188	2,188	4,324
183.00	4,534	296.0	3,885	6,073	6,537
184.00	5,604	338.0	5,060	11,133	8,679
185.00	6,810	396.0	6,197	17,330	12,087

Device	Routing	Invert	Outlet Devices
#1	Primary	179.00'	18.0" Round Culvert OUTLET L= 89.1' Ke= 0.500 Inlet / Outlet Invert= 179.00' / 177.50' S= 0.0168 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	181.10'	3.0" Vert. LOW FLOW OUTLET X 3.00 C= 0.000 Limited to weir flow at low heads
#3	Device 1	181.90'	3.0" Vert. MIDDLE ORIFICES X 3.00 C= 0.600 Limited to weir flow at low heads
#4	Device 1	184.00'	48.0" x 48.0" Horiz. TOP OVERFLOW WEIR C= 0.600 Limited to weir flow at low heads
#5	Secondary	184.50'	10.0' long x 10.0' breadth EMERGENCY SPILLWAY Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.6 cfs @ 12.39 hrs HW=181.88' TW=110.73' (Dynamic Tailwater)

-1=Culvert OUTLET (Passes 0.6 cfs of 12.4 cfs potential flow)

-2=LOW FLOW OUTLET (Orifice Controls 0.6 cfs @ 3.89 fps)

-3=MIDDLE ORIFICES (Controls 0.0 cfs)

-4=TOP OVERFLOW WEIR (Controls 0.0 cfs)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=181.00' TW=109.00' (Dynamic Tailwater) -5=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS4: WQS4

Inflow = 2.0 cfs @ Outflow = 1.2 cfs @ Primary = 1.2 cfs @	0.00% Impervious, 12.19 hrs, Volume= 12.35 hrs, Volume= 12.35 hrs, Volume= 0.00 hrs, Volume=	8,919 cf, Atten= 37%, Lag= 5.4 min 8,919 cf
------------------------------------------------------------	----------------------------------------------------------------------------------------------------------	---------------------------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 112.49' @ 12.35 hrs Surf Area= 1,716 sf Storage= 997 cf Flood Elev= 111.30' Surf.Area= 43 sf Storage= 2 cf

Plug-Flow detention time= 7.3 min calculated for 8,913 cf (100% of inflow) Center-of-Mass det. time= 7.2 min (909.7 - 902.5)

Volume	Invert	Avail.Storage	Storage Description Custom Stage Data (Irregular)Listed below (Recalc)
#1	111.20'	6,843 cf	
#1	111.20'	6,843 cf	Custom Stage Data (Irregular) Elsted bolon (1 toosie)

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Page 33

Elevation (feet) 111.20 111.50 112.00 113.00 114.00	Surf.Area (sq-ft) 10 179 1,102 2,495 3,426	Perim. (feet) 5.0 88.0 222.0 276.0 314.0	Inc.Store (cubic-feet) 0 23 288 1,752 2,948	Cum.Store (cubic-feet) 0 23 311 2,062 5,011 6,843	Wet.Area (sq-ft) 10 624 3,931 6,085 7,894 8,627
114.50	3,908	328.0	1,832	6,843	0,027

	, ,			
Device	Routing	Invert	Outlet Devices	
#1	Primary	109.60'	12.0" Round Culvert OUTLET L= 134.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 109.60' / 108.30' S= 0.0097 '/' Cc= 0.900 n= 0.013, Flow Area= 0.79 sf	
#2	Device 1	111.30'	6.0" W x 3.0" H Vert. LOW FLOW OUTLET C= 0.600 Limited to weir flow at low heads	
#3	Device 1	112.05'	8.0" W x 15.0" H Vert. MIDDLE WEIR C= 0.600 Limited to weir flow at low heads	
#4	Device 1	113.30'	Limited to woir flow at low heads	
#5	Secondary	114.00'	10.0' long x 7.0' breadth EMERGENCY SPILLWAY Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.0 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.65 2.66 2.68 2.70 2.73 2.78	
			2.65 2.66 2.65 2.66 2.68 2.70 2.73 2.78	

Primary OutFlow Max=1.2 cfs @ 12.35 hrs HW=112.49' TW=110.02' (Dynamic Tailwater)

1-Culvert OUTLET (Passes 1.2 cfs of 4.0 cfs notantial flow)

-1=Culvert OUTLET (Passes 1.2 cfs of 4.0 cfs potential flow)

—2=LOW FLOW OUTLET (Orifice Controls 0.6 cfs @ 4.97 fps)

-3=MIDDLE WEIR (Orifice Controls 0.6 cfs @ 2.13 fps)

-4=TOP WEIR (Controls 0.0 cfs)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=111.20' TW=108.00' (Dynamic Tailwater) 5=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Link AP-2A: 36" RCP

777,113 sf, 1.45% Impervious, Inflow Depth = 0.61" for 2-Year event Inflow Area = 39,261 cf 6.0 cfs @ 12.28 hrs, Volume=

39,261 cf, Atten= 0%, Lag= 0.0 min Inflow = 6.0 cfs @ 12.28 hrs, Volume=

Primary

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2B: 24" RCP

359,530 sf, 6.51% Impervious, Inflow Depth = 0.95" for 2-Year event Inflow Area = 28,490 cf

5.2 cfs @ 12.31 hrs, Volume= Inflow

28,490 cf, Atten= 0%, Lag= 0.0 min 5.2 cfs @ 12.31 hrs, Volume= Primary

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

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Summary for Link AP1: AP-1

142,959 sf, 0.65% Impervious, Inflow Depth = 1.02" for 2-Year event Inflow Area = 12,127 cf

1.6 cfs @ 12.25 hrs, Volume= Inflow

12,127 cf, Atten= 0%, Lag= 0.0 min 1.6 cfs @ 12.25 hrs, Volume= Primary

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP3: AP-3

19,815 sf, 0.00% Impervious, Inflow Depth = 0.85" for 2-Year event Inflow Area = 1,401 cf

0.3 cfs @ 12.25 hrs, Volume=

1,401 cf, Atten= 0%, Lag= 0.0 min Inflow 0.3 cfs @ 12.25 hrs, Volume= Primary

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 10-Year Rainfall=4.83" Printed 8/16/2021

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Page 35

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Runoff by SCS TR-2 Reach routing by Dyn-Stor-Ind r	20 method, UH=SCS, Weighted-CN nethod - Pond routing by Dyn-Stor-Ind method
Subcatchment P1: TO SD	Runoff Area=16,143 sf 4.08% Impervious Runoff Depth=1.47" Flow Length=204' Tc=8.3 min CN=64 Runoff=0.5 cfs 1,979 cf
Subcatchment P10: TO GS-B Flow Length=45	Runoff Area=21,159 sf 1.51% Impervious Runoff Depth=2.48" Slope=0.0667 '/' Tc=5.0 min CN=77 Runoff=1.3 cfs 4,375 cf
Subcatchment P11: TO GS-C	Runoff Area=144,531 sf 0.00% Impervious Runoff Depth=2.31" Flow Length=67' Tc=5.0 min CN=75 Runoff=8.5 cfs 27,848 cf
Subcatchment P12: TO GS-D	Runoff Area=25,460 sf 0.00% Impervious Runoff Depth=2.84" Flow Length=75' Tc=5.0 min CN=81 Runoff=1.8 cfs 6,016 cf
Subcatchment P13: TO SWL1D	Runoff Area=17,550 sf 1.82% Impervious Runoff Depth=3.02" Flow Length=327' Tc=5.0 min CN=83 Runoff=1.3 cfs 4,418 cf
Subcatchment P14: TO WQS3	Runoff Area=81,404 sf 0.49% Impervious Runoff Depth=2.40" Flow Length=385' Tc=5.0 min CN=76 Runoff=5.0 cfs 16,255 cf
SubcatchmentP15: TO CB3	Runoff Area=31,226 sf 0.00% Impervious Runoff Depth=2.40" Flow Length=550' Tc=13.4 min CN=76 Runoff=1.4 cfs 6.235 cf
SubcatchmentP16: TO AP-3	Runoff Area=19,815 sf 0.00% Impervious Runoff Depth=1.99" Flow Length=259' Tc=14.8 min CN=71 Runoff=0.7 cfs 3,284 cf
Subcatchment P17: TO GS-E	Runoff Area=43,526 sf 0.00% Impervious Runoff Depth=2.23" Flow Length=184' Tc=5.0 min CN=74 Runoff=2.5 cfs 8,086 cf
Subcatchment P18: TO SWL2	Runoff Area=3,212 sf 0.00% Impervious Runoff Depth=2.23" Tc=5.0 min CN=74 Runoff=0.2 cfs 597 cf
Subcatchment P19: TO WQS2 Flow Length=3	Runoff Area=6,629 sf 0.00% Impervious Runoff Depth=2.23" 31' Slope=0.2260 '/' Tc=5.0 min CN=74 Runoff=0.4 cfs 1,232 cf
Subcatchment P2: TO WQS4	Runoff Area=75,884 sf 0.00% Impervious Runoff Depth=2.15" Flow Length=285' Tc=9.3 min CN=73 Runoff=3.6 cfs 13,583 cf
Subcatchment P3: TO AP1	Runoff Area=19,706 sf 1.38% Impervious Runoff Depth=3.12" Flow Length=498' Tc=6.6 min CN=84 Runoff=1.5 cfs 5,116 cf
Subcatchment P4: TO CB2	Runoff Area=66,052 sf 0.00% Impervious Runoff Depth=2.07" Flow Length=824' Tc=16.4 min CN=72 Runoff=2.4 cfs 11,382 cf
SubcatchmentP5A: TO EX.36"	Runoff Area=273,835 sf 3.65% Impervious Runoff Depth=2.07" Flow Length=691' Tc=16.5 min CN=72 Runoff=9.9 cfs 47,186 cf
SubcatchmentP5B: TO EX.24"	Runoff Area=359,530 sf 6.51% Impervious Runoff Depth=2.15" Flow Length=783' Tc=19.6 min CN=73 Runoff=12.5 cfs 64,355 cf

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Page 36

Runoff Area=22,064 sf 0.00% Impervious Runoff Depth=2.23" Subcatchment P6: TO WQS1

Flow Length=35' Slope=0.1700'/' Tc=5.0 min CN=74 Runoff=1.2 cfs 4,099 cf

Runoff Area=61,702 sf 0.00% Impervious Runoff Depth=2.23" Flow Length=308' Tc=5.0 min CN=74 Runoff=3.5 cfs 11,463 cf Subcatchment P7: TO GS-A

Runoff Area=3,312 sf 0.00% Impervious Runoff Depth=2.23" Flow Length=119' Slope=0.1180 '/' Tc=5.0 min CN=74 Runoff=0.2 cfs 615 cf Subcatchment P8: TO CB1

Runoff Area=6.677 sf 3.29% Impervious Runoff Depth=3.12

Flow Length=267' Tc=5.0 min CN=84 Runoff=0.5 cfs 1,733 cf Subcatchment P9: TO HW#1

Avg. Flow Depth=0.08' Max Vel=1.30 fps Inflow=1.4 cfs 6,235 cf n=0.035 L=180.0' S=0.0389 '/' Capacity=1,899.8 cfs Outflow=1.4 cfs 6,235 cf Reach OF: TO WREP

Avg. Flow Depth=0.38' Max Vel=3.20 fps Inflow=1.4 cfs 6,235 cf n=0.035 L=126.0' S=0.0556'/' Capacity=115.9 cfs Outflow=1.4 cfs 6,235 cf Reach OF2: FROM WREP

Avg. Flow Depth=0.18' Max Vel=4.30 fps Inflow=2.0 cfs 11,842 cf n=0.035 L=157.0' S=0.1338 '/ Capacity=263.5 cfs Outflow=2.0 cfs 11,842 cf Reach SWL1A:

Avg. Flow Depth=0.15' Max Vel=4.76 fps Inflow=1.8 cfs 11,228 cf n=0.035 L=20.0' S=0.2000 '/' Capacity=322.2 cfs Outflow=1.8 cfs 11,228 cf Reach SWL1B:

Avg. Flow Depth=0.17' Max Vel=3.06 fps Inflow=1.3 cfs 8,155 cf n=0.035 L=301:0' S=0.0731 '/' Capacity=194.8 cfs Outflow=1.3 cfs 8,155 cf Reach SWL1C:

Avg. Flow Depth=0.15' Max Vel=3.63 fps Inflow=1.3 cfs 8,155 cf n=0.035 L=25.0' S=0.1200'/' Capacity=249.6 cfs Outflow=1.3 cfs 8,155 cf Reach SWL1D:

Avg. Flow Depth=0.15' Max Vel=2.58 fps Inflow=0.2 cfs 3,351 cf n=0.035 L=265.0' S=0.1245 '/' Capacity=173.6 cfs Outflow=0.2 cfs 3,351 cf Reach SWL2:

Peak Elev=100.11' Storage=39 cf Inflow=12.5 cfs 64,355 cf 36.0" Round Culvert n=0.011 L=81.0' S=0.0062 '/' Outflow=12.5 cfs 64,353 cf Pond 24"-RCP: EX. 24" CULV

Peak Elev=111.58' Storage=16 cf Inflow=15.8 cfs 94,661 cf 36.0" Round Culvert n=0.011 L=57.0' S=0.0135 '/' Outflow=15.8 cfs 94,660 cf Pond 36"-RCP: EX. 36" CULV

Peak Elev=166.18' Inflow=0.2 cfs 615 cf 12.0" Round Culvert n=0.013 L=62.0' S=0.0081 '/' Outflow=0.2 cfs 614 cf Pond CB1:

Peak Elev=148.00' Storage=0 cf Inflow=2.4 cfs 11,382 cf 15.0" Round Culvert n=0.013 L=264.0' S=0.0049 '/' Outflow=2.4 cfs 11,382 cf Pond CB2:

Peak Elev=129.37' Inflow=1.4 cfs 6,235 cf 12.0" Round Culvert n=0.013 L=34.0' S=0.0118 '/' Outflow=1.4 cfs 6,235 cf Pond CB3:

Peak Elev=174.00' Storage=0 cf Inflow=1.8 cfs 9,889 cf 15.0" Round Culvert n=0.013 L=65.0' S=0.1231'/ Outflow=1.8 cfs 9,889 cf Pond CLV1: HW#1

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Page 37

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Pond GS-A: Grassed Swales	Peak Elev=166.82' Storage=11,463 cf Inflow=3.5 cfs 11,463 cf Outflow=0.0 cfs 0 cf
Pond GS-B: Grassed Swales	Peak Elev=171.02' Storage=3,100 cf Inflow=1.3 cfs 4,375 cf Outflow=0.1 cfs 1,339 cf
Pond GS-C: Grassed Swales	Peak Elev=196.95' Storage=27,848 cf Inflow=8.5 cfs 27,848 cf Outflow=0.0 cfs 0 cf
Pond GS-D: Grassed Swales	Peak Elev=200.10' Storage=2,601 cf Inflow=1.8 cfs 6,016 cf Outflow=0.5 cfs 3,737 cf
Pond GS-E: Grassed Swales	Peak Elev=180.01' Storage=5,429 cf Inflow=2.5 cfs 8,086 cf Outflow=0.1 cfs 2,754 cf
Pond SD: stone diaphragm	Peak Elev=110.03' Storage=210 cf Inflow=3.4 cfs 21,795 cf Outflow=3.4 cfs 21,588 cf
Pond WQS1: WQS1	Peak Elev=143.59' Storage=2,944 cf Inflow=4.9 cfs 27,323 cf Primary=4.5 cfs 26,846 cf Secondary=0.0 cfs 0 cf Outflow=4.5 cfs 26,846 cf
Pond WQS2: WQS2	Peak Elev=143.68' Storage=580 cf Inflow=0.5 cfs 4,582 cf Primary=0.3 cfs 4,511 cf Secondary=0.0 cfs 0 cf Outflow=0.3 cfs 4,511 cf
Pond WQS3: WQS3	Peak Elev=182.53' Storage=4,102 cf Inflow=5.0 cfs 16,255 cf Primary=1.3 cfs 16,119 cf Secondary=0.0 cfs 0 cf Outflow=1.3 cfs 16,119 cf
Pond WQS4: WQS4	Peak Elev=113.12' Storage=2,375 cf Inflow=4.7 cfs 19,818 cf Primary=3.2 cfs 19,816 cf Secondary=0.0 cfs 0 cf Outflow=3.2 cfs 19,816 cf
Link AP-2A: 36" RCP	Inflow=15.8 cfs 94,660 cf Primary=15.8 cfs 94,660 cf
Link AP-2B: 24" RCP	Inflow=12.5 cfs 64,353 cf Primary=12.5 cfs 64,353 cf
Link AP1: AP-1	Inflow=4.2 cfs 26,704 cf Primary=4.2 cfs 26,704 cf
Link AP3: AP-3	Inflow=0.7 cfs 3,284 cf Primary=0.7 cfs 3,284 cf

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Summary for Subcatchment P1: TO SD

Runoff

0.5 cfs @ 12.16 hrs, Volume=

1,979 cf, Depth= 1.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

At	ea (sf)	CN_D	escription_		
 	370	98 F	oofs, HSG	Α	
	288	98 F	aved parkit	ng, HSG A	
	4,843	39 >	75% Grass	cover, Go	od, HSG A
	0	96 (Bravel surfa	ice, HSG C	
	7,790	74 >	75% Grass	s cover, Go	ood, HSG C
	2,852	70 V	Voods, God	od, HSG C	
	0		Gravel surfa		
	16,143	64 \	Weighted A	verage	
	15,485	ξ	95.92% Per	vious Area	
	658	4	1.08% Impe	rvious Area	a
_		Class	Velocity	Capacity	Description
Tç	Length	Slope		(cfs)	
 <u>(min)</u>	(feet)	(ft/ft)		(010)	Sheet Flow,
7.6	75	0.1540	0.16		Woods: Light underbrush n= 0.400 P2= 3 15"
	00	0.4540	1.96		Shallow Concentrated Flow,
0.2	28	0.1540	1.90		Woodland Kv= 5.0 fps
0.4	46	0.1540	6.32		Shallow Concentrated Flow,
0.1	40	0.1540	0.02		Unpayed Kv= 16.1 fps
0.4	55	0.0180	2.16		Shallow Concentrated Flow,
0.4	00	0.0100			Unpaved Kv= 16.1 fps
 8.3	204	Total			
0.0					

Summary for Subcatchment P10: TO GS-B

Runoff

1.3 cfs @ 12.12 hrs, Volume=

4,375 cf, Depth= 2.48"

Area	ı (s <u>f)</u>	CN_	Description
18	,619	74	>75% Grass cover, Good, HSG C
	,220	96	Gravel surface, HSG C
_	320	98	Unconnected pavement, HSG C
	,159 ,839 320 320	77	Weighted Average 98.49% Pervious Area 1.51% Impervious Area 100.00% Unconnected

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Page 39

119410					
Tc	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
(min)			0.23		Sheet Flow,
3.2	45	0.0667	0.23		Grass: Short n= 0.150 P2= 3.15"
					Direct Entry, MIN. TC = 5.0 MIN
1.8					Direct Entry, Mile. 10 old miles
	45	Total			
5.0	45	Total			

Summary for Subcatchment P11: TO GS-C

Runoff

8.5 cfs @ 12.12 hrs, Volume=

27,848 cf. Depth= 2.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

NRCC 24	-(II D 10	100			
Ar	ea (sf)	CN [Description		
	40,163	74 :	>75% Grass	cover, Go	od, HSG C
	3,993	96	Gravel surfa	ice, HSG C	
_	375		Woods, Goo		
1-	44,531	75	Weighted A	verage	^
1	44,531		100.00% P€	ervious Are	a
Tc	Length	Slope (ft/ft		Capacity (cfs)	Description
(min)_	(feet)				Sheet Flow, GRVL DRV
0.4	32	0.0310) 1.29		Smooth surfaces n= 0.011 P2= 3.15"
2.8	35	0.0570	0.21		Sheet Flow, Grass: Short n= 0.150 P2= 3.15"
1.8					Direct Entry, MIN. TC = 5.0 MIN
5.0	67	Total			

Summary for Subcatchment P12: TO GS-D

Runoff

1.8 cfs @ 12.11 hrs, Volume=

6,016 cf, Depth= 2.84"

Area (sf) CN Description 17,020 74 >75% Grass cover, Good, HSG C 7,895 96 Gravel surface, HSG C 442 70 Woods, Good, HSG C 103 74 >75% Grass cover, Good, HSG C 25,460 81 Weighted Average 25,460 100.00% Pervious Area	1	ood, HSG C	96 70 74
--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	---	------------	----------------

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 10-Year Rainfall=4.83" Printed 8/16/2021

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Page 40

HydroCA	D® 10.10-4	la s/n U 10	J30 © 2020	7 1 y a 0 0 / 1	
	Length	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)_	
<u>(min)</u>	(feet)		1.33		Sheet Flow, grvl
0.3	28	0.0357	1.55		Sheet Flow, givi Smooth surfaces n= 0.011 P2= 3.15"
3.2	31	0.0322	0.16		Sheet Flow, Grass: Short n= 0.150 P2= 3.15"
0.5	16	0.0050	0.54		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.15"
					Direct Entry, 5.0 min.
1.0					
5.0	75	Total			

Summary for Subcatchment P13: TO SWL1D

1.3 cfs @ 12.11 hrs, Volume= Runoff

4,418 cf, Depth= 3.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

NRCC 24-III	-10 ע	i cai i te	•••		
Area	(sf)	CN D	escription		
	471	7/ >	75% Grass	cover, Goo	od, HSG C
	726	~~ (rough curtai	re Hatitu	
	320	98 L	Inconnected 75% Grass	pavemen cover Goo	od, HSG C
	33	74 >	Veighted A	rerage	
17,	550	83 \	98,18% Per	vious Area	
17,	,230 320		1 82% Impe	rvious Area	a e e e e e e e e e e e e e e e e e e e
	320	,	100.00% Ur	connected	
		_,	\/-looit\	Capacity	Description
	ength	Slope (ft/ft)		(cfs)	
<u>(min)</u>	(feet)	0.0630			Sheet Flow, grvl
0.3	30	0.0030	, , , , , ,		Smooth surfaces n= 0.011 P2= 3.15"
3.3	45	0.0630	0.23		Sheet Flow, Grass: Short n= 0.150 P2= 3.15"
5.0					Shallow Concentrated Flow,
0.0	12	0.063	3 4.04		Uppayed $KV = 16.1 \text{ IPS}$
	040	0.075	0 4.41		Shallow Concentrated Flow,
0.9	240	0.015	0		Unpaved Kv= 16.1 fps
0.5					Direct Entry, 5.0 min
5.0	327	Total			

Summary for Subcatchment P14: TO WQS3

5.0 cfs @ 12.12 hrs, Volume= Runoff

16,255 cf, Depth= 2.40"

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Ar	ea (sf)	CN [Description		
	7,914	96 (Gravel surfa	ce, HSG C	
	70,819	74 >	75% Grass	cover, Go	od, HSG C
	2,271	70 \	Noods, Goo	d, HSG C	. 1100 0
	400	98 l	Jnconnecte	d pavemer	11, H5G C
	0				ood, HSG C
	81,404	76 \	Weighted A	verage	
	81,004	(99.51% Per	vious Area	a
	400		0.49% Impe 100.00% Ur	noonnacted	a 1
	400		100.00% 01	COMECIC	,
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)		(cfs)	- 100
1.0	75	0.0200			Sheet Flow, GRASS Smooth surfaces n= 0.011 P2= 3.15"
1,0					Smooth surfaces 11–0.011 12 5.10 Shallow Concentrated Flow,
1.3	175	0.0200) 2.28		Unpaved Kv= 16.1 fps
					Shallow Concentrated Flow,
0.4	135	0.1040	5.19		Unpaved Kv= 16.1 fps
					Direct Entry, 5.0 MIN.
2.3					
5.0	385	Total			

Summary for Subcatchment P15: TO CB3

1.4 cfs @ 12.22 hrs, Volume= Runoff

6,235 cf, Depth= 2.40"

Area (sf) 12,202 4,836 14,188	74 96 70 74	Description >75% Grass cover, Good, HSG C Gravel surface, HSG C Woods, Good, HSG C >75% Grass cover, Good, HSG C
31,226 31,226	76	Weighted Average 100.00% Pervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.5		0.0680	0.12		Sheet Flow,
1.1	87	0.0680	1.30		Woods: Light underbrush n= 0.400 P2= 3.15" Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.3	114	0.1500	6.24		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.2	81	0.1500	6.24		Shallow Concentrated Flow, grvrl Unpaved Kv= 16.1 fps
1.0	115	0.1500	1.94		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
0.3	78	0.1030	5.17		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
13.4	550	Total			

Summary for Subcatchment P16: TO AP-3

Runoff

0.7 cfs @ 12.24 hrs, Volume=

3,284 cf, Depth= 1.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

А	rea (sf)	CN D	escripti <u>on</u>					
	12,429 7,386	70 V 74 >	Woods, Good, HSG C >75% Grass cover, Good, HSG C					
	19,815 19,815	71 V	Weighted Average 100.00% Pervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
12.5	75	0.0440	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"			
1.7	106	0.0440	1.05		Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
0.6	78	0.1790	2.12		Shallow Concentrated Flow, Woodland Kv= 5.0 fps			
14.8	259	Total						

Summary for Subcatchment P17: TO GS-E

Runoff

2.5 cfs @ 12.12 hrs, Volume=

8,086 cf, Depth= 2.23"

Total

184

5.0

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181084-POST-REV 1.1		Page 43
181084-POST-NEV The pared by Goldsmith, Prest & Ringwall, Inc. Prepared by Goldsmith, Prest & Ringwall, Inc. HydroCAD® 10.10-4a s/n 01036 © 2020 HydroCAD Software Solutions LLC		1 ago 10
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43	a (sf) 3,526 0	74 > 74 >	escription 75% Grass 75% Grass Veighted Av	cover, Go	od, HSG C od, HSG C
	3,526 3,526	74 V	00.00% Pe	rvious Area	
	_ength (feet)	Slope (ft/ft)		Capacity (cfs)	Description CRVI DRV
<u>(min)</u> 0.6	75	0.0800			Sheet Flow, GRVL DRV Smooth surfaces n= 0.011 P2= 3.15" Smooth surfaces n= 0.011 P2= 3.15"
0.3	49	0.0310	2.83		Smooth surfaces 11- 0.01 Flow, GRVL DRV Shallow Concentrated Flow, GRVL DRV Unpaved Kv= 16.1 fps
0.5	60	0.0170	2.10		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Direct Entry, 5.0 MIN
					011001

Summary for Subcatchment P18: TO SWL2

597 cf, Depth= 2.23" 0.2 cfs @ 12.12 hrs, Volume= Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

5.0	
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs) Direct Entry, 5.0 MIN	
Area (sf) CN Description 3,212 74 >75% Grass cover, Good, HSG C 3,212 100.00% Pervious Area	
NRCC 24-hr D 10-Year (Valifical)	

Summary for Subcatchment P19: TO WQS2

1,232 cf, Depth= 2.23" 0.4 cfs @ 12.12 hrs, Volume=

NRCC 24-hr D 10-Yea	Naman 1195
Area (sf) CN 6,629 74 6,629	Description >75% Grass cover, Good, HSG C 100.00% Pervious Area

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Page 44

1 (mi		Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	.5	31	0.2260	0.35		Sheet Flow, Grass: Short n= 0.150 P2= 3.15"
3	.5					Direct Entry, MIN TC = 5.0 MIN
5	5.0	31	Total			

Summary for Subcatchment P2: TO WQS4

3.6 cfs @ 12.17 hrs, Volume= Runoff

13,583 cf, Depth= 2.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

Δ	rea (sf)	CN D	escription						
	55,955		Woods, Good, HSG C						
	13.098	74 >	75% Grass	s cover, Go	ood, HSG C				
	6,831	96 G	aravel surfa	ice, HSG C					
	75,884 75,884	73 V 1	Veighted A 00.00% Pe	verage ervious Area	a				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
7.4	75	0.1660	0.17		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"				
0.4	55	0.1660	2.04		Shallow Concentrated Flow, Woodland Kv= 5.0 fps				
1.5	142	0.0950	1.54		Shallow Concentrated Flow, Woodland Kv= 5.0 fps				
0.0	13	0.3300	9.25		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps				
9.3	285	Total							

Summary for Subcatchment P3: TO AP1

1.5 cfs @ 12.14 hrs, Volume= Runoff

5,116 cf, Depth= 3.12"

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Page 45

		ea (sf)	CN [N Description						
		1,002	39 :	>75% Grass	od, HSG A					
		4,040	96	Gravel surfa	ce, HSG A					
		6,422	96	Gravel surfa	ce, HSG C					
		5,625	74	>75% Grass	cover, Go	od, HSG C				
		2,270	70	Woods, God	od, HSG C					
		76	30	Woods, God	od. HSG A					
		256	98	Unconnecte	d pavemen	it, HSG C				
		15		Roofs, HSG						
		19,706	84	Weighted A	verage					
		19,435		98.62% Per						
		271		1.38% Impe		∄				
		256		94.46% Und	connected					
				V Ladika	Canacity	Description				
	Tc	Length	Slope		Capacity (cfs)					
_	(min)	(feet)_	(ft/ft		(013)	Sheet Flow,				
	4.1	75	0.100	0.30		Grass: Short n= 0.150 P2= 3.15"				
			0.400	0 5.09		Shallow Concentrated Flow,				
	0.0	12	0.100	0 5.09		Unnaved Kv= 16.1 fps				
		C 0	0.075	0 4.41		Shallow Concentrated Flow, GRVL				
	0.2	53	0.075	0 4.71		Unpayed Kv= 16.1 fps				
	2.2	358	0.025	0 2.55		Shallow Concentrated Flow,				
	2.3	330	0.020	,,_		Unpaved Kv= 16.1 fps				
-	6.6	498	Total			-				
	0.0	7,00								

Summary for Subcatchment P4: TO CB2

2.4 cfs @ 12.25 hrs, Volume= Runoff

11,382 cf, Depth= 2.07"

Area (sf)	<u>CN</u>	Description
36,514	74	>75% Grass cover, Good, HSG C
29,013	70	Woods, Good, HSG C
525	96	Gravel surface, HSG C
66,052 66,052	72	Weighted Average 100.00% Pervious Area

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HydroCAL	10.10-2			O a altri	Description
Tc	Length	Slope	Velocity	Capacity (cfs)	Description
(min)	(feet)	(ft/ <u>f</u> t)	(ft/sec)	(013)	Sheet Flow,
8.3	40	0.0350	0.08		Woods: Light underbrush n= 0.400 P2= 3.15"
3.4	35	0.0350	0.17		Sheet Flow, Grass: Short n= 0.150 P2= 3.15"
0					Shallow Concentrated Flow,
2.3	290	0.0170	2.10		Unpaved Kv= 16.1 fps
					Shallow Concentrated Flow,
0.4	90	0.0560	3.81		Unpaved Kv= 16.1 fps
			1.29		Shallow Concentrated Flow,
1.4	105	0.0670	1.29		Woodland Kv= 5.0 fps
	244	0.4660	6.56		Shallow Concentrated Flow,
0.5	211	0.1660	0.50		Unnaved Kv= 16.1 fps
	C 0	0.1510	6.26		Shallow Concentrated Flow,
0.1	53	0.1510	0.20		Unpaved Kv= 16.1 fps
40.4	824	Total			
16.4	024	i Otai			

Summary for Subcatchment P5A: TO EX.36"

9.9 cfs @ 12.26 hrs, Volume= Runoff

47,186 cf, Depth= 2.07"

Area (sf)	CN	Description
- 0	96	Gravel surface, HSG C
187,867	70	Woods Good, HSG C
75,981	74	>75% Grass cover, Good, HSG C
9,587	98	Paved parking, HSG C
400	98	Unconnected pavement, HSG C
273,835 263,848 9,987 400	72	Weighted Average 96.35% Pervious Area 3.65% Impervious Area 4.01% Unconnected

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 10-Year Rainfall=4.83" Printed 8/16/2021

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Page 47

HydroCAD)® 10.10-4	ia s/n u it	30 @ 2020	o riyare e	
	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)_	
(min)_			0.40		Sheet Flow,
1.1	27	0.3300	0,40		Grass: Short n= 0.150 P2= 3.15"
8.4	48	0.0490	0.10		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"
0.8	54	0.0490	1.11		Shallow Concentrated Flow, Woodland Ky= 5.0 fps
1.6	130	0.0770	1.39		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
2.5	305	0.1640	2.02		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
2.1	127	0.0390	0.99		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
16.5	691	Total			

Summary for Subcatchment P5B: TO EX.24"

12.5 cfs @ 12.29 hrs, Volume= Runoff

64,355 cf, Depth= 2.15"

NRCC 24-III D TO	100	
Area (sf) 5,494 277,852 52,653 20,671 2,721	96 70 74 98 98 74	Description Gravel surface, HSG C Woods, Good, HSG C >75% Grass cover, Good, HSG C Paved parking, HSG C Roofs, HSG C >75% Grass cover, Good, HSG C
359,530 336,138 23,392	73	Weighted Average 93.49% Pervious Area 6.51% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	57	0.3300	0.46	_	Sheet Flow,
2.1	57	0.5500	0.10		Grass: Short n= 0.150 P2= 3.15"
2.0	18	0.2500	0.15		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15"
	50	0.000	2.50		Shallow Concentrated Flow,
0.3	52	0.2500	2.50		Woodland Kv= 5.0 fps
5.9	209	0.0140	0.59		Shallow Concentrated Flow, Woodland Kv= 5.0 fps
. .	221	0.0180	0.67		Shallow Concentrated Flow,
5.5	2.21	0.0100	0.01		Woodland Kv= 5.0 fps
2.4	117	0.0260	0.81		Shallow Concentrated Flow, Woodland Kv= 5.0 fps

Summary for Subcatchment P6: TO WQS1

Shallow Concentrated Flow,

Woodland Kv= 5.0 fps

Runoff = 1.2 cfs @ 12.12 hrs, Volume=

109 0.0700

783 Total

1.4

19.6

1.32

4,099 cf, Depth= 2.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

	ea (sf) 21,626	74 >			od, HSG C				
	438								
	22,064	74 \	veignted A	verage					
	22,064	100.00% Pervious Area							
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description				
1.8	35	0.1700			Sheet Flow,				
1.0	00	0.17.00			Grass: Short n= 0.150 P2= 3.15"				
3.2					Direct Entry, MIN. TC = 5.0 MIN				
	35	Total							
5.0	33	Total							

Summary for Subcatchment P7: TO GS-A

Runoff = 3.5 cfs @ 12.12 hrs, Volume=

11,463 cf, Depth= 2.23"

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Page 49

HydroCAL	10.10-4	<u>u 3/11/01/</u>	000 @ <u>202</u>							
Ar	ea (sf <u>)</u>	CN D	CN Description							
	30,550	74 >75% Grass cover, Good, HSG C								
	1,152	96 G	ravel surfa	ice, HSG C	, HSC C					
	0			d pavemer	ц, нэо с					
	61,702	74 V	Veighted A	verage ervious Are	a					
	61,702	·	00.00701	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,						
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	CDVI DDV					
0.5	75	0.1050	2.50		Sheet Flow, GRVL DRV Smooth surfaces n= 0.011 P2= 3.15"					
		0.4050	5.22		Shallow Concentrated Flow, GRVL DRV					
0.1	39	0.1050	5.22		Unpayed Kv= 16.1 fps					
0.1	30	0.1000	5.09		Shallow Concentrated Flow, GRVL DRV					
0.1	50	0.1000			Unpaved Kv= 16.1 fps					
0.3	86	0.0700	4.26		Shallow Concentrated Flow, GRVL DRV Unpaved Kv= 16.1 fps					
			0.00		Shallow Concentrated Flow,					
0.0	19	0.3330	9.29		Unnaved Ky= 16.1 fps					
0.0	E 0	0.1530	6.30		Shallow Concentrated Flow,					
0.2	59	0.1550	0.00		Unnaved Ky= 16.1 fps					
3.8					Direct Entry, MIN TC = 5.0 MIN					
5.0		Total								

Summary for Subcatchment P8: TO CB1

Runoff =

0.2 cfs @ 12.12 hrs, Volume=

615 cf, Depth= 2.23"

	Λ.,	on (of)	CN D	escription					
	<u>A</u> I	ea (sf)	74 >75% Grass cover, Good, HSG C						
	_	3,312 3,312	100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
-	3.9		0.1180	0.32	···	Sheet Flow,			
	0.1		0.1180	5.53		Grass: Short n= 0.150 P2= 3.15" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Direct Entry, MIN. TC = 5.0 MIN			
	1.0				<u> </u>	Direct Likely www.			
-	5.0	119	Total						

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Summary for Subcatchment P9: TO HW#1

0.5 cfs @ 12.11 hrs, Volume= Runoff

1,733 cf, Depth= 3.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 10-Year Rainfall=4.83"

NRCC 24-III D 10 104 104 104										
	Area (sf)	(sf) CN Description								
2 720 74 >75% Grass cover, Good, HSG C										
	0	98	Unconnected pavement, HSG C							
	2,728	96	Gravel surface, HSG C							
	220		Unconnected pavement, HSG C Weighted Average							
	6,677									
	6,457		96.71% Pervious Area 3.29% Impervious Area							
	220 220		100.00% Ur	connected						
	220									
T	c Length	Slope		Capacity	Description					
(min		(ft/ft		(cfs)	Sheet Flow, GRVL DRV					
0.	5 75	0.095	0 2.40		Smooth surfaces $n=0.011 P2=3.15$					
_	o (1	0.0660	0 4.14		Shallow Concentrated Flow, GRVL DRV					
0.	2 61	0.000	0 11.7.		Unpayed Ky= 16.1 fps					
0.	1 28	0.1430	0 6.09		Shallow Concentrated Flow,					
0.					Unpaved Kv= 16.1 fps Shallow Concentrated Flow,					
0	.2 103	0.204	.0 7.27		Unnaved Kv= 16.1 fps					
	_				Direct Entry, MIN. TC = 5.0 MIN					
4	.0									
5	.0 267	Total								

Summary for Reach OF: TO WREP

31,226 sf, 0.00% Impervious, Inflow Depth = 2.40" for 10-Year event 6.235 cf

Inflow Area = 1.4 cfs @ 12.22 hrs, Volume= Inflow

6,235 cf, Atten= 3%, Lag= 1.9 min 1.4 cfs @ 12.25 hrs, Volume= Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.30 fps, Min. Travel Time= 2.3 min

Avg. Velocity = 0.61 fps, Avg. Travel Time= 4.9 min

Peak Storage= 194 cf @ 12.25 hrs Average Depth at Peak Storage= 0.08', Surface Width= 17.76' Bank-Full Depth= 2.00' Flow Area= 220.0 sf, Capacity= 1,899.8 cfs

10.00' x 2.00' deep channel, n= 0.035 Earth, dense weeds Side Slope Z-value= 50.0 '/' Top Width= 210.00' Length= 180.0' Slope= 0.0389 '/' Inlet Invert= 129.00', Outlet Invert= 122.00'

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 10-Year Rainfall=4.83" Printed 8/16/2021

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Page 51

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Summary for Reach OF2: FROM WREP

31,226 sf, 0.00% Impervious, Inflow Depth = 2.40" for 10-Year event Inflow Area = 6,235 cf

1.4 cfs @ 12.25 hrs, Volume= Inflow

6,235 cf, Atten= 0%, Lag= 0.5 min 1.4 cfs @ 12.26 hrs, Volume= Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.20 fps, Min. Travel Time= 0.7 min Avg. Velocity = 1.45 fps, Avg. Travel Time= 1.4 min

Peak Storage= 55 cf @ 12.26 hrs Average Depth at Peak Storage= 0.38', Surface Width= 2.29' Bank-Full Depth= 2.00' Flow Area= 12.0 sf, Capacity= 115.9 cfs

0.00' x 2.00' deep channel, n= 0.035 Earth, dense weeds

Side Slope Z-value= 3.0 '/' Top Width= 12.00'

Length= 126.0' Slope= 0.0556 '/'

Inlet Invert= 122.00', Outlet Invert= 115.00'



Summary for Reach SWL1A:

280,391 sf, 0.31% Impervious, Inflow Depth = 0.51" for 10-Year event Inflow Area =

2.0 cfs @ 12.13 hrs, Volume= 11,842 cf

11,842 cf, Atten= 0%, Lag= 0.5 min Inflow 2.0 cfs @ 12.14 hrs, Volume= Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.30 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.57 fps, Avg. Travel Time= 1.7 min

Peak Storage= 72 cf @ 12.14 hrs Average Depth at Peak Storage= 0.18', Surface Width= 3.08' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 263.5 cfs

2.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 14.00' Length= 157.0' Slope= 0.1338 '/' Inlet Invert= 166.00', Outlet Invert= 145.00'

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 10-Year Rainfall=4.83"

Printed 8/16/2021 Page 52

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Summary for Reach SWL1B:

215,377 sf, 0.40% Impervious, Inflow Depth = 0.63" for 10-Year event Inflow Area = 11,228 cf

1.8 cfs @ 12.13 hrs, Volume=

11,228 cf, Atten= 0%, Lag= 0.1 min 1.8 cfs @ 12.13 hrs, Volume= Inflow Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.76 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.82 fps, Avg. Travel Time= 0.2 min

Peak Storage= 7 cf @ 12.13 hrs Average Depth at Peak Storage= 0.15', Surface Width= 2.91' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 322.2 cfs

2.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 1 Top Width= 14.00'

Length= 20.0' Slope= 0.2000 '/'

Inlet Invert= 170.00', Outlet Invert= 166.00'

Summary for Reach SWL1C:

187,541 sf, 0.17% Impervious, Inflow Depth = 0.52" for 10-Year event Inflow Area = 8,155 cf

1.3 cfs @ 12.12 hrs, Volume= Inflow

8,155 cf, Atten= 3%, Lag= 1.5 min 1.3 cfs @ 12.14 hrs, Volume= Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.06 fps, Min. Travel Time= 1.6 min

Avg. Velocity = 1.14 fps, Avg. Travel Time= 4.4 min

Peak Storage= 127 cf @ 12.14 hrs

Average Depth at Peak Storage= 0.17', Surface Width= 3.01'

Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 194.8 cfs

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2.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value = 3.0 '/' Top Width = 14.00' Length= 301.0' Slope= 0.0731 '/' Inlet Invert= 196.00', Outlet Invert= 174.00'



Summary for Reach SWL1D:

43,010 sf, 0.74% Impervious, Inflow Depth = 2.28" for 10-Year event Inflow Area =

1.3 cfs @ 12.11 hrs, Volume= 8,155 cf Inflow

8,155 cf, Atten= 1%, Lag= 0.2 min 1.3 cfs @ 12.12 hrs, Volume= Outflow

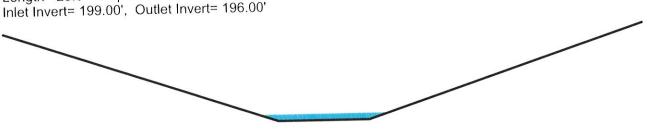
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.63 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.38 fps, Avg. Travel Time= 0.3 min

Peak Storage= 9 cf @ 12.12 hrs

Average Depth at Peak Storage= 0.15', Surface Width= 2.89' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 249.6 cfs

2.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 14.00' Length= 25.0' Slope= 0.1200 //



Summary for Reach SWL2:

46,738 sf, 0.00% Impervious, Inflow Depth = 0.86" for 10-Year event Inflow Area =

3,351 cf 0.2 cfs @ 12.12 hrs, Volume= Inflow

3,351 cf, Atten= 3%, Lag= 1.5 min 0.2 cfs @ 12.14 hrs, Volume= Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.58 fps, Min. Travel Time= 1.7 min Avg. Velocity = 1.56 fps, Avg. Travel Time= 2.8 min

Peak Storage= 18 cf @ 12.14 hrs

Average Depth at Peak Storage= 0.15', Surface Width= 0.90'

Bank-Full Depth= 2.00' Flow Area= 12.0 sf, Capacity= 173.6 cfs

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Page 54

0.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 12.00' Length= 265.0' Slope= 0.1245 '/' Inlet Invert= 178.00', Outlet Invert= 145.00'



Summary for Pond 24"-RCP: EX. 24" CULV

Inflow Area = 359,530 sf, 6.51% Impervious, Inflow Depth = 2.15" for 10-Year event

Inflow = 12.5 cfs @ 12.29 hrs, Volume= 64,355 cf

Outflow = 12.5 cfs @ 12.30 hrs, Volume= 64,353 cf, Atten= 0%, Lag= 0.1 min

Primary = 12.5 cfs @ 12.30 hrs, Volume= 64,353 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 100.11' @ 12.30 hrs Surf.Area= 45 sf Storage= 39 cf

Plug-Flow detention time= 0.8 min calculated for 64,353 cf (100% of inflow)

Center-of-Mass det. time= 0.1 min (881.9 - 881.8)

Volume	Invert /	Avail.Storage				
#1	98.00'	4,909 c	Custom Stage I	Data (Irregular)List	ed below (Recalc)	·
Elevation (feet)	Surf.Ar (sq			Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
98.00		1 3. 15 22.		0 7	1 41	
99.00 100.00		42 31.	0 27	34	87	
101.00	1	79 37. 89 60.		94 224	134 318	
102.00 103.00	8	120.	0 463	687	1,182	
104.00 105.00		937 205. 963 302.			3,387 7,308	

Device Routing Invert Outlet Devices

#1 Primary 98.54' **36.0" Round Culvert**

L= 81.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 98.54' / 98.04' S= 0.0062 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=12.4 cfs @ 12.30 hrs HW=100.10' TW=0.00' (Dynamic Tailwater) —1=Culvert (Barrel Controls 12.4 cfs @ 4.86 fps)

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Page 55

Summary for Pond 36"-RCP: EX. 36" CULV

Inflow Area = 777,113 sf, 1.45% Impervious, Inflow Depth = 1.46" for 10-Year event
Inflow = 15.8 cfs @ 12.25 hrs, Volume= 94,661 cf
Outflow = 15.8 cfs @ 12.25 hrs, Volume= 94,660 cf, Atten= 0%, Lag= 0.0 min
Primary = 15.8 cfs @ 12.25 hrs, Volume= 94,660 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 111.58' @ 12.25 hrs Surf.Area= 14 sf Storage= 16 cf

Plug-Flow detention time= 0.1 min calculated for 94,594 cf (100% of inflow) Center-of-Mass det. time= 0.0 min (921.3 - 921.3)

Volume	Invert	<u>Avail.S</u>	Storage 412 cf	Storage Description Custom Stage Dat	a (Irregular)Listed	below (Recalc)
#1 Elevation	109.00' Sui	rf.Area (sq-ft)	Perim.	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
(feet) 109.00 110.00 111.00 112.00 113.00 114.00 115.00		1 4 10 18 43 165 372	4.0 9.0 15.0 19.0 27.0 52.0 74.0	0 2 7 14 30 97 262	0 2 9 23 53 150 412	1 9 26 46 83 245 475
	outing rimary	Inv 109.	70' 36 (et Devices " Round Culvert	L - dwall k	(a= 0.900

L= 57.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 109.79' / 109.02' S= 0.0135 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=15.8 cfs @ 12.25 hrs HW=111.58' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 15.8 cfs @ 3.60 fps)

Summary for Pond CB1:

Outflow =	3,312 sf, 0.00% Impervious, 0.2 cfs @ 12.12 hrs, Volume= 0.2 cfs @ 12.13 hrs, Volume= 0.2 cfs @ 12.13 hrs, Volume=	614 cf, Atten= 0%, Lag= 0.5 min
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 166.18' @ 12.19 hrs

Device #1	Routing Primary	164.00'	Outlet Devices 12.0" Round Culvert L= 62.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 164.00' / 163.50' S= 0.0081 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
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Page 56

Primary OutFlow Max=0.0 cfs @ 12.13 hrs HW=166.16' TW=166.17' (Dynamic Tailwater) 1=Culvert (Controls 0.0 cfs)

Summary for Pond CB2:

66,052 sf, 0.00% Impervious, Inflow Depth = 2.07" for 10-Year event Inflow Area = 2.4 cfs @ 12.25 hrs, Volume= 11.382 cf 11,382 cf, Atten= 0%, Lag= 0.0 min Inflow = 2.4 cfs @ 12.25 hrs, Volume= Outflow 2.4 cfs @ 12.25 hrs, Volume= 11,382 cf Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 148.00' @ 0.00 hrs Surf.Area= 3 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= (not calculated: outflow precedes inflow)

Volume #1	Invert 148.00'	Avail.S	Storage 119 cf	Storage Description Custom Stage Dat	n t a (Irregular) Listed	below
Elevation (feet) 148.00 149.00 150.00	Sı	urf.Area (sq-ft) 3 50 154	Perim. (feet) 6.0 25.0 44.0	Inc.Store (cubic-feet) 0 22 97	Cum.Store (cubic-feet) 0 22 119	Wet.Area (sq-ft) 3 52 162
	outing rimary	1nve 144.3	0' 15.0	et Devices " Round Culvert 264.0' CMP, project	ing, no headwall,	Ke= 0.900 0.0049 '/'

Inlet / Outlet Invert= 144.30' / 143.00' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.0 cfs @ 12.25 hrs HW=148.00' TW=143.59' (Dynamic Tailwater) 1=Culvert (Passes 0.0 cfs of 6.7 cfs potential flow)

Summary for Pond CB3:

31,226 sf, 0.00% Impervious, Inflow Depth = 2.40" for 10-Year event 1.4 cfs @ 12.22 hrs, Volume= 6,235 cf, 1.4 cfs @ 12.22 hrs, Volume= 6,235 cf, Inflow Area = 6,235 cf, Atten= 0%, Lag= 0.0 min Inflow = Outflow 1.4 cfs @ 12.22 hrs, Volume= 6.235 cf Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 129.37' @ 12.22 hrs

#1 Primary 128.50'	Outlet Devices 12.0" Round Culvert L= 34.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 128.50' / 128.10' S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
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Page 57

Primary OutFlow Max=1.4 cfs @ 12.22 hrs HW=129.37' TW=129.08' (Dynamic Tailwater) —1=Culvert (Outlet Controls 1.4 cfs @ 2.59 fps)

Summary for Pond CLV1: HW#1

194,218 sf, 0.28% Impervious, Inflow Depth = 0.61" for 10-Year event Inflow Area = 1.8 cfs @ 12.13 hrs, Volume= 9,889 cf 9,889 cf, Atten= 0%, Lag= 0.0 min Inflow 1.8 cfs @ 12.13 hrs, Volume= Outflow 9,889 cf 1.8 cfs @ 12.13 hrs, Volume= Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 174.00' @ 12.15 hrs Surf Area= 274 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min (882.3 - 882.3)

Volume #1	Invert 174.00'	Avai	.Storage 1,585 cf	Storage Description Custom Stage Dat	a (Irregular)List	ed below
Elevation (feet) 174.00 175.00 176.00 177.00	Sul	rf.Area (sq-ft) 274 583 583 583	Perim. (feet) 91.0 126.0 126.0	Inc.Store (cubic-feet) 0 419 583 583	Cum.Store (cubic-feet) 0 419 1,002 1,585	Wet.Area (sq-ft) 274 888 1,014 1,140
	outing rimary		00' 150	et Devices " Round Culvert	ng no headwall	Ke= 0.900

L= 65.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 173.00' / 165.00' S= 0.1231 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=2.8 cfs @ 12.13 hrs HW=174.00' TW=170.15' (Dynamic Tailwater) 1=Culvert (Inlet Controls 2.8 cfs @ 2.69 fps)

Summary for Pond GS-A: Grassed Swales

Inflow Area = Inflow = Outflow = Primary =	61,702 sf, 0.00% Impervious, Inflow Depth = 2.23" for 10-Year event 3.5 cfs @ 12.12 hrs, Volume= 11,463 cf 0.0 cfs @ 0.00 hrs, Volume= 0 cf, Atten= 100%, Lag= 0.0 min 0.0 cfs @ 0.00 hrs, Volume= 0 cf
--------------------------------------------	---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 166.82' @ 24.35 hrs Surf.Area= 15,504 sf Storage= 11,463 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

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Page 58

Volume #1	Inve 165.50	2.7.2		Description Stage Data (Coni	ic)Listed below	x 4
Elevatio (feet 165.5 166.0 166.5 167.0 167.5	0 0 0 0	Surf.Area (sq-ft) 434 1,736 3,038 4,340 5,642	Inc.Store (cubic-feet) 0 506 1,178 1,835 2,488	Cum.Store (cubic-feet) 0 506 1,685 3,520 6,008	Wet.Area (sq-ft) 434 1,737 3,042 4,348 5,656	
Device #1	Routing Primary	Invert 167.00'	6.0' long x 2. Head (feet) 0	0' breadth Broad .20 0.40 0.60 0.8 50 a) 2.54 2.61 2.61	80 1.00 1.20 1	ingular Weir X 4.00 .40 1.60 1.80 2.00

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=165.50' TW=166.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond GS-B: Grassed Swales

Outflow	a = = = =	1.3 cfs @ 0.1 cfs @	1.51% Impervious, 12.12 hrs, Volume= 15.61 hrs, Volume= 15.61 hrs, Volume=	1,339 cf, Atten= 96%, Lag	
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 171.02' @ 15.61 hrs Surf.Area= 3,714 sf Storage= 3,100 cf

Plug-Flow detention time= 457.9 min calculated for 1,338 cf (31% of inflow) Center-of-Mass det. time= 291.8 min (1,146.8 - 855.0)

Volume	Invert	Avail.Stor			Description		
#1	169.50'	5,15	52 cf	Custom	Stage Data (P	rismatic)Listed below	₹2
Elevation (feet) 169.50 170.00 170.50 171.00 171.50		rf.Area (sq-ft) 184 736 1,288 1,840 2,392	(cubic-	Store -feet) 0 230 506 782 1,058	Cum.Store (cubic-feet) 0 230 736 1,518 2,576		
	Routing Primary	Invert 171.00'	6.0' le	(feet) 0	.0' breadth Bro .20 0.40 0.60	0.80 1.00 1.20 1.40 .61 2.60 2.66 2.70 2.	1.60 1.80 2.00

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Page 59

2.85 3.07 3.20 3.32

Primary OutFlow Max=0.1 cfs @ 15.61 hrs HW=171.02' TW=170.04' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.1 cfs @ 0.31 fps)

Summary for Pond GS-C: Grassed Swales

144,531 sf, 0.00% Impervious, Inflow Depth = 2.31" for 10-Year event 27,848 cf Inflow Area = 8.5 cfs @ 12.12 hrs, Volume= 0 cf, Atten= 100%, Lag= 0.0 min Inflow = 0.0 cfs @ 0.00 hrs, Volume= Outflow 0 cf 0.00 hrs, Volume= 0.0 cfs @ Primary =

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 196.95' @ 24.35 hrs Surf.Area= 34,592 sf Storage= 27,848 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Centor or					
Volume #1	Invert 195.50'	Avail.Stora 50,064	·	Description Stage Data (Pris	matic)Listed below x 8
Elevation (feet) 195.50 196.00 196.50 197.00 197.50		urf.Area (sq-ft) (447 1,788 3,129 4,470 5,811	Inc.Store cubic-feet) 0 559 1,229 1,900 2,570	Cum.Store (cubic-feet) 0 559 1,788 3,688 6,258	
<u> </u>	Routing Primary	Invert 197.00'	Head (feet)	2.0' breadth Broa 0.20	d-Crested Rectangular Weir X 7.00 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=195.50' TW=196.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

Summary for Pond GS-D: Grassed Swales

Inflow Area = 25,460 sf, 0.00% Impervious, Inflow Depth = 2.84" for 10-Year event 6,016 cf Inflow = 1.8 cfs @ 12.11 hrs, Volume= 0.5 cfs @ 12.35 hrs, Volume= 0.5	4.2 min
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 200.10' @ 12.35 hrs Surf.Area= 2,979 sf Storage= 2,601 cf

Plug-Flow detention time= 245.0 min calculated for 3,735 cf (62% of inflow)

#1

Primary

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Center-of-Mass det. time= 115.5 min (956.5 - 841.0)

Volume	Inv	ert Avail.Sto	orage Storage	Description		
#1	198.	50' 3,8	90 cf Custom	Stage Data (Coni	c)Listed below	
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
198.9 199.0		281 1,124	0 328	0 328	281 1,125	
199.9 200.0	00	1,967 2,810	763 1,188	1,091 2,279	1,971 2,818	
200.	50	3,653	1,611	3,890	3,667	
Device	Routing	Invert	Outlet Devices	s		
#1	Primary	200.00'	Head (feet) 0 2.50 3.00 3.5	1) 2.54 2.61 2.61	0 1.00 1.20 1.40	1.60 1.80 2.00

Primary OutFlow Max=0.5 cfs @ 12.35 hrs HW=200.10' TW=199.11' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.5 cfs @ 0.80 fps)

Summary for Pond GS-E: Grassed Swales

Inflow Area	a =	43,526 sf,	0.00% Impervious,	Inflow Depth = 3	2.23" for 10-Year ever	nt
Inflow	=	2.5 cfs @	12.12 hrs, Volume=	8,086 cf		
Outflow	=	0.1 cfs @	14.97 hrs, Volume=	2,754 cf	, Atten= 95%, Lag= 17 ⁻	1.2 min
Primary	=	0.1 cfs @	14.97 hrs, Volume=	2,754 cf		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 180.01' @ 14.97 hrs Surf.Area= 8,573 sf Storage= 5,429 cf

Plug-Flow detention time= 425.8 min calculated for 2,752 cf (34% of inflow) Center-of-Mass det. time= 262.2 min (1,127.2 - 865.0)

Volume	Invert	Avail.Storage	Storage [Description		
#1	178.50'	10,496 ct	Custom	Stage Data (Prisr	matic)Listed below	x 9
Elevation (feet)	Surf.Ar (sq		nc.Store pic-feet)	Cum.Store (cubic-feet)		
178.50	(54)	75 (cui	0	0		
179.00	1	35	53	53		
179.50	5	40	169	221		
180.00	9	45	371	593		
180.50	1,3	50	574	1,166		
Device Ro	outing	Invert Ou	ıtlet Devices			

6.0' long x 2.0' breadth Broad-Crested Rectangular Weir X 9.00 180.00' Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00

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Page 61

2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=0.1 cfs @ 14.97 hrs HW=180.01' TW=178.14' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.1 cfs @ 0.25 fps)

Summary for Pond SD: stone diaphragm

Inflow Are	a =	123,253 sf,	0.53% Impervious,	Inflow Depth = 2.12	" for 10-Year event
· ·	=	3.4 cfs @	12.29 hrs, Volume=	21,795 cf	ten= 0%, Lag= 0.1 min
Outflow	=	3.4 cfs @	12.29 hrs, Volume=		ten= 078, Lag= 0.1 min
Primary	=	3.4 cfs @	12.29 hrs, Volume=	21,588 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 110.03' @ 12.29 hrs Surf.Area= 200 sf Storage= 210 cf Flood Elev= 110.50' Surf.Area= 200 sf Storage= 247 cf

Plug-Flow detention time= 8.8 min calculated for 21,588 cf (99% of inflow) Center-of-Mass det. time= 3.1 min (885.9 - 882.8)

Volume	Invert	Avail.Storage	Storage Description (Description
#1	108 00'	169 cf	Custom Stage Data (Prismatic)Listed below (Recalc) 500 cf Overall - 79 cf Embedded = 421 cf x 40.0% Voids
#2	108.30'	79 cf	12.0" Round Pipe Storage Inside #1 L= 100.0'

247 cf Total Available Storage

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
108.00	200	0	0
110.50	200	500	500

Device_	Routing	Invert	Outlet Devices
#1	Primary		195.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Primary OutFlow Max=3.4 cfs @ 12.29 hrs HW=110.03' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 3.4 cfs @ 0.50 fps)

Summary for Pond WQS1: WQS1

Inflow = 4.9 cfs @ Outflow = 4.5 cfs @ Primary = 4.5 cfs @	0.23% Impervious, 12.15 hrs, Volume= 12.21 hrs, Volume= 12.21 hrs, Volume= 0.00 hrs, Volume=	26,846 cf, Atten= 8%, Lag= 3.4 min 26,846 cf
------------------------------------------------------------	----------------------------------------------------------------------------------------------------------	-------------------------------------------------

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Page 62

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 143.59' @ 12.21 hrs Surf.Area= 5,908 sf Storage= 2,944 cf Flood Elev= 143.10' Surf.Area= 4,391 sf Storage= 425 cf

Plug-Flow detention time= 79.2 min calculated for 26,827 cf (98% of inflow) Center-of-Mass det. time= 71.0 min (963.8 - 892.8)

<u>Volume</u>	<u>Inve</u>	ert Avail.	Storage	Storage Description		
#1	143.0	00' 14	1,736 cf			below (Recalc)
Elevati	et)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
143. 144. 145.	00	4,110 7,342 10,953	838.0 863.0 882.0	0 5,648 9,088	0 5,648 14,736	4,110 7,599 10,378
Device	Routing	Inve	rt_ Outle	et Devices		
#1	Primary	139.50	Inlet	Round Culvert OU Outlet Invert= 139.5	0' / 136.50' S= 0.0	1261 '/' Co- 0 000
#2	Device 1	143.10	J.U	013 Corrugated PE, Vert. LOW FLOW OL	JILET C=0600	low Area≃ 1.23 sf
#3	Device 1	143.40	48.0"	ed to weir flow at low x 48.0" Horiz. TOP	OVERFLOW WEIR	R C= 0.600
#4	Secondar	y 144.50)' 10.0' Head	ed to weir flow at low long x 10.0' breadtl (feet) 0.20 0.40 0.6 (English) 2.49 2.56	HEMERGENCY SI	1 1 10 1 60

Primary OutFlow Max=4.5 cfs @ 12.21 hrs HW=143.59' TW=111.54' (Dynamic Tailwater) -1=Culvert OUTLET (Passes 4.5 cfs of 11.0 cfs potential flow)

-2=LOW FLOW OUTLET (Orifice Controls 0.1 cfs @ 2.91 fps)

-3=TOP OVERFLOW WEIR (Weir Controls 4.3 cfs @ 1.42 fps)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=143.00' TW=109.00' (Dynamic Tailwater)

4=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS2: WQS2

Outflow = 0.3 cfs (sf, 0.00% Impervious, 2 12.13 hrs, Volume= 2 12.24 hrs, Volume= 3 12.24 hrs, Volume= 4 0.00 hrs, Volume=	4,511 cf, Atten= 46%, Lag= 7.0 min
---------------------	----------------------------------------------------------------------------------------------------------------------	------------------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 143.68' @ 12.24 hrs Surf Area= 1,061 sf Storage= 580 cf Flood Elev= 143.10' Surf.Area= 712 sf Storage= 69 cf

Plug-Flow detention time= 128.4 min calculated for 4,508 cf (98% of inflow) Center-of-Mass det. time= 122.7 min (1,146.8 - 1,024.1)

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3

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Pag	e	63

<u>Volume</u>	e Inv	ert Avail	.Storage	Storage Description				
#1	143.0		01		stom Stage Data (Irregular)Listed below (Recalc)			
Elevati (fe 143. 144. 145.	et) 00 00	Surf.Area (sq-ft) 659 1,283 1,984	Perim. (feet) 196.0 225.0 251.0	Inc.Store (cubic-feet) 0 954 1,621	Cum.Store (cubic-feet) 0 954 2,575	Wet.Area (sq-ft) 659 1,653 2,666		
Device	Routing	Inve		t Devices		-1,000		
#1	Primary	141.2	Inlet /	Round Culvert OU Outlet Invert= 141.2	5' / 139 50' S- 0 C	1400 1/1 0- 0 000		
#2	#2 Device 1 143		0' 1.0" \	1.0" Vert. LOW FLOW OUTLET C= 0.600				
#3	Device 1	143.6	Limite	ed to weir flow at low x 48.0" Horiz. TOP	heads	0 0-000		
#4 Secondary 144.50' 6.0' long x 1 Head (feet) 0		ed to weir flow at low ong x 10.0' breadth (feet) 0.20 0.40 0.6 (English) 2.49 2.56	heads EMERGENCY SPI 80-0-80-1-00-1-20	LLWAY				
					2.00 2.00 2	.00 2.07 2.04		

Primary OutFlow Max=0.3 cfs @ 12.24 hrs HW=143.68' TW=111.57' (Dynamic Tailwater)

1=Culvert OUTLET (Passes 0.3 cfs of 7.9 cfs potential flow)

-2=LOW FLOW OUTLET (Orifice Controls 0.0 cfs @ 3.53 fps) -3=TOP OVERFLOW WEIR (Weir Controls 0.3 cfs @ 0.56 fps)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=143.00' TW=109.00' (Dynamic Tailwater)

4=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS3: WQS3

Inflow Area = Inflow = Outflow = Primary = Secondary =	81,404 sf, 0.49% Impervious, Inflow Depth = 2.40" for 10-Year event 5.0 cfs @ 12.12 hrs, Volume= 1.3 cfs @ 12.35 hrs, Volume= 1.3 cfs @ 12.35 hrs, Volume= 0.0 cfs @ 0.00 hrs, Volume= 0.0 cfs @ 0.00 hrs, Volume=
--------------------------------------------------------	--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 182.53' @ 12.35 hrs Surf.Area= 3,919 sf Storage= 4,102 cf Flood Elev= 181.10' Surf.Area= 1,420 sf Storage= 134 cf

Plug-Flow detention time= 48.7 min calculated for 16,119 cf (99% of inflow) Center-of-Mass det. time= 43.4 min (901.7 - 858.3)

<u>Volume</u>	Invert	Avail.Storage	Storage Description
#1	181.00'	17,330 cf	Custom Stage Data (Irregular)Listed below (Recalc)

Wet.Area

181084-POST-REV 1.1

Elevation

#4

Device 1

(feet)

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(eq.ft)

Surf.Area

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Perim.

(foot)

Page 64

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(1661)		(54-11)	(leet)	(cubic-reet)	(cubic-reet)	(SQ-II)		
181.	00	1,261	147.0	0	0	1,261		
182.	00	3,271	245.0	2,188	2,188	4,324		
183.		4,534	296.0	3,885	6,073	6,537		
184.		5,604	338.0	5,060	11,133	8,679		
185.	00	6,810	396.0	6,197	17,330	12,087		
Device	Routing	Inve	ert Outlet [Devices				
#1	Primary	179.0	Inlet / C	18.0" Round Culvert OUTLET L= 89.1' Ke= 0.500 Inlet / Outlet Invert= 179.00' / 177.50' S= 0.0168 '/' Cc= 0.900				
#2	Device 1	181.1			smooth interior, FI			
,	237,03	101.1	+	3.0" Vert. LOW FLOW OUTLET X 3.00 C= 0.600 Limited to weir flow at low heads				
#3	Device 1	181.9	0' 3.0" V e	3.0" Vert. MIDDLE ORIFICES X 3.00 C= 0.600				

Inc.Store

(cubic foot)

Cum.Store

(cubic foot)

#5 Secondary Limited to weir flow at low heads
184.50' 10.0' long x 10.0' breadth EMERGENCY SPILLWAY
Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Limited to weir flow at low heads

48.0" x 48.0" Horiz. TOP OVERFLOW WEIR C= 0.600

Primary OutFlow Max=1.3 cfs @ 12.35 hrs HW=182.53' TW=111.41' (Dynamic Tailwater)

-1=Culvert OUTLET (Passes 1.3 cfs of 14.2 cfs potential flow)

-2=LOW FLOW OUTLET (Orifice Controls 0.8 cfs @ 5.51 fps)
-3=MIDDLE ORIFICES (Orifice Controls 0.5 cfs @ 3.43 fps)

-4=TOP OVERFLOW WEIR (Controls 0.0 cfs)

184.00"

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=181.00' TW=109.00' (Dynamic Tailwater)

5=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS4: WQS4

Inflow Area =	107,110 sf,	0.00% Impervious,	Inflow Depth = 2.22" for 10-Year event
Inflow =		12.18 hrs, Volume=	
Outflow =	3.2 cfs @	12.31 hrs, Volume=	19,816 cf, Atten= 32%, Lag= 7.7 min
Primary =	3.2 cfs @	12.31 hrs, Volume=	
Secondary =	0.0 cfs @	0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 113.12' @ 12.31 hrs Surf.Area= 2,601 sf Storage= 2,375 cf Flood Elev= 111.30' Surf.Area= 43 sf Storage= 2 cf

Plug-Flow detention time= 9.3 min calculated for 19,816 cf (100% of inflow) Center-of-Mass det. time= 8.9 min (880.9 - 872.0)

Volume	Invert	Avail.Storage	Storage Description
#1	111.20'	6,843 cf	Custom Stage Data (Irregular)Listed below (Recalc)

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HydroCAD® 10.10	4a s/n 01036	© 2020 Hyd	TOCAL SULWARD STA		Wet.Area
HydroCAD® 10.10	- 4d 0.11		Inc.Store	Cum Store	(sq-ft)
-i dian	Surf.Area	Perim.	(cubic-feet)	(cubic-feet)	10
Elevation	(sq-ft)	(feet)	(Cubic-1004)	0	624
(feet)	10	5.0	23	23	3,931
111.20	179	0.88	288	311	6,085
111.50	1,102	222.0	1,752	2,062	7.894
112.00	2,495	276.0	2,948	5,011	8,627
113.00	3,426	314.0	1.832	6,843	0,027
114.00	3,908	328.0	1,002		
114.50	5,500				

50 50	3,908 3	28.0
Routing Primary	109.60'	Outlet Devices 12.0" Round Culvert OUTLET L= 134.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 109.60' / 108.30' S= 0.0097 '/' Cc= 0.900 In= 0.013, Flow Area= 0.79 sf 6.0" W x 3.0" H Vert. LOW FLOW OUTLET C= 0.600
Device 1	111.30'	6.0" W x 3.0" H Vert. LOVI Lovi H Vert. LOVI Lovi H Vert. Lovi H Vert. MIDDLE WEIR C= 0.600 8.0" W x 15.0" H Vert. MIDDLE WEIR C= 0.600
Device 1	112.05	Limited to well flow at the WEIR C= 0.600
Device 1		
Secondary	, 114.00°	Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 4.50 3.00 3.50 4 00 4.50 5.00 5.50 4.50 2.66 2.65 2.66 2.65 2.66 2.65 2.66 2.65 2.66 2.67 2.70 2.70 2.70 2.70 2.70 2.70 2.70 2.7
	Routing Primary Device 1 Device 1 Device 1	Routing Invert Primary 109.60' Device 1 111.30' Device 1 112.05' Device 1 113.30'

Primary OutFlow Max=3.1 cfs @ 12.31 hrs HW=113.12' TW=110.03' (Dynamic Tailwater)

-1=Culvert OUTLET (Passes 3.1 cfs of 4.5 cfs potential flow)

2=LOW FLOW OUTLET (Orifice Controls 0.8 cfs @ 6.26 fps)

-3=MIDDLE WEIR (Orifice Controls 2.4 cfs @ 3.32 fps)

L_4=TOP WEIR (Controls 0.0 cfs)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=111.20' TW=108.00' (Dynamic Tailwater)

—5=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Link AP-2A: 36" RCP

777,113 sf, 1.45% Impervious, Inflow Depth = 1.46" for 10-Year event 94,660 cf, Atten= 0%, Lag= 0.0 min 15.8 cfs @ 12.25 hrs, Volume= Inflow Area = 15.8 cfs @ 12.25 hrs, Volume= Inflow = Primary

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2B: 24" RCP

359,530 sf, 6.51% Impervious, Inflow Depth = 2.15" for 10-Year event 64,353 cf, Atten= 0%, Lag= 0.0 min 12.5 cfs @ 12.30 hrs, Volume= Inflow Area = 12.5 cfs @ 12.30 hrs. Volume= Inflow Primary

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 10-Year Rainfall=4.83"

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Page 66

Summary for Link AP1: AP-1

Inflow Area = 142,959 sf, 0.65% Impervious, Inflow Depth = 2.24" for 10-Year event

Inflow = 4.2 cfs @ 12.20 hrs, Volume= 26,704 cf

Primary = 4.2 cfs @ 12.20 hrs, Volume= 26,704 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP3: AP-3

Inflow Area = 19,815 sf, 0.00% Impervious, Inflow Depth = 1.99" for 10-Year event

Inflow = 0.7 cfs @ 12.24 hrs, Volume= 3,284 cf

Primary = 0.7 cfs @ 12.24 hrs, Volume= 3,284 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94"

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Page 67

Time span=0.00-72.00 hrs, dt=0.05 hrs, 1441 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Redon redding by Dyn-Gto	r-ind method - Folid routing by Dyn-Stor-ind method
SubcatchmentP1: TO SD	Runoff Area=16,143 sf 4.08% Impervious Runoff Depth=4.54" Flow Length=204' Tc=8.3 min CN=64 Runoff=1.7 cfs 6,113 cf
Subcatchment P10: TO GS-B Flow Lengt	Runoff Area=21,159 sf 1.51% Impervious Runoff Depth=6.14" th=45' Slope=0.0667 '/' Tc=5.0 min CN=77 Runoff=3.2 cfs 10,832 cf
Subcatchment P11: TO GS-C	Runoff Area=144,531 sf 0.00% Impervious Runoff Depth=5.90" Flow Length=67' Tc=5.0 min CN=75 Runoff=21.3 cfs 71,029 cf
Subcatchment P12: TO GS-D	Runoff Area=25,460 sf 0.00% Impervious Runoff Depth=6.63" Flow Length=75' Tc=5.0 min CN=81 Runoff=4.1 cfs 14,075 cf
Subcatchment P13: TO SWL1D	Runoff Area=17,550 sf 1.82% Impervious Runoff Depth=6.88" Flow Length=327' Tc=5.0 min CN=83 Runoff=2.9 cfs 10,060 cf
Subcatchment P14: TO WQS3	Runoff Area=81,404 sf 0.49% Impervious Runoff Depth=6.02" Flow Length=385' Tc=5.0 min CN=76 Runoff=12.2 cfs 40,839 cf
Subcatchment P15: TO CB3	Runoff Area=31,226 sf 0.00% Impervious Runoff Depth=6.02" Flow Length=550' Tc=13.4 min CN=76 Runoff=3.6 cfs 15,666 cf
Subcatchment P16: TO AP-3	Runoff Area=19,815 sf 0.00% Impervious Runoff Depth=5.41" Flow Length=259' Tc=14.8 min CN=71 Runoff=2.0 cfs 8,925 cf
Subcatchment P17: TO GS-E	Runoff Area=43,526 sf 0.00% Impervious Runoff Depth=5.77" Flow Length=184' Tc=5.0 min CN=74 Runoff=6.3 cfs 20,944 cf
Subcatchment P18: TO SWL2	Runoff Area=3,212 sf 0.00% Impervious Runoff Depth=5.77" Tc=5.0 min CN=74 Runoff=0.5 cfs 1,546 cf
Subcatchment P19: TO WQS2 Flow Leng	Runoff Area=6,629 sf 0.00% Impervious Runoff Depth=5.77" ath=31' Slope=0.2260 '/' Tc=5.0 min CN=74 Runoff=1.0 cfs 3,190 cf
Subcatchment P2: TO WQS4	Runoff Area=75,884 sf 0.00% Impervious Runoff Depth=5.65" Flow Length=285' Tc=9.3 min CN=73 Runoff=9.3 cfs 35,737 cf
Subcatchment P3: TO AP1	Runoff Area=19,706 sf 1.38% Impervious Runoff Depth=7.00" Flow Length=498' Tc=6.6 min CN=84 Runoff=3.2 cfs 11,497 cf
Subcatchment P4: TO CB2	Runoff Area=66,052 sf 0.00% Impervious Runoff Depth=5.53" Flow Length=824' Tc=16.4 min CN=72 Runoff=6.4 cfs 30,429 cf
SubcatchmentP5A: TO EX.36"	Runoff Area=273,835 sf 3.65% Impervious Runoff Depth=5.53" Flow Length=691' Tc=16.5 min CN=72 Runoff=26.7 cfs 126,153 cf
Subcatchment P5B: TO EX.24"	Runoff Area=359,530 sf 6.51% Impervious Runoff Depth=5.65" Flow Length=783' Tc=19.6 min CN=73 Runoff=32.9 cfs 169,318 cf

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94"

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Page 68

Subcatchment P6: TO WQS1

Runoff Area=22,064 sf 0.00% Impervious Runoff Depth=5.77"

Flow Length=35' Slope=0.1700'/' Tc=5.0 min CN=74 Runoff=3.2 cfs 10,617 cf

Subcatchment P7: TO GS-A

Runoff Area=61,702 sf 0.00% Impervious Runoff Depth=5.77" Flow Length=308' Tc=5.0 min CN=74 Runoff=8.9 cfs 29,691 cf

Subcatchment P8: TO CB1

Runoff Area=3,312 sf 0.00% Impervious Runoff Depth=5.77"

Flow Length=119' Slope=0.1180 '/' Tc=5.0 min CN=74 Runoff=0.5 cfs 1,594 cf

Subcatchment P9: TO HW#1

Runoff Area=6,677 sf 3.29% Impervious Runoff Depth=7.00" Flow Length=267' Tc=5.0 min CN=84 Runoff=1.1 cfs 3,895 cf

Reach OF: TO WREP

Avg. Flow Depth=0.13' Max Vel=1.70 fps Inflow=3.6 cfs 15,666 cf

n=0.035 L=180.0' S=0.0389'/' Capacity=1,899.8 cfs Outflow=3.5 cfs 15,666 cf

Reach OF2: FROM WREP

Avg. Flow Depth=0.54' Max Vel=4.03 fps Inflow=3.5 cfs 15,666 cf

n=0.035 L=126.0' S=0.0556'/' Capacity=115.9 cfs Outflow=3.5 cfs 15,666 cf

Reach SWL1A:

Avg. Flow Depth=0.41' Max Vel=6.78 fps Inflow=9.0 cfs 92,280 cf n=0.035 L=157.0' S=0.1338'/' Capacity=263.5 cfs Outflow=9.0 cfs 92,280 cf

Reach SWL1B:

Avg. Flow Depth=0.36' Max Vel=7.75 fps Inflow=8.7 cfs 75,074 cf

n=0.035 L=20.0' S=0.2000'/' Capacity=322.2 cfs Outflow=8.7 cfs 75,074 cf

Reach SWL1C:

Avg. Flow Depth=0.39' Max Vel=4.89 fps Inflow=6.1 cfs 63,382 cf n=0.035 L=301.0' S=0.0731'/' Capacity=194.8 cfs Outflow=6.1 cfs 63,382 cf

Reach SWL1D:

Avg. Flow Depth=0.35' Max Vel=5.84 fps Inflow=6.1 cfs 21,856 cf n=0.035 L=25.0' S=0.1200'/' Capacity=249.6 cfs Outflow=6.2 cfs 21,856 cf

Reach SWL2:

Avg. Flow Depth=0.56' Max Vel=6.20 fps Inflow=6.0 cfs 17,158 cf n=0.035 L=265.0' S=0.1245 '/' Capacity=173.6 cfs Outflow=5.9 cfs 17,158 cf

Pond 24"-RCP: EX. 24" CULV

Peak Elev=101.54' Storage=150 cf Inflow=32.9 cfs 169,318 cf 36.0" Round Culvert n=0.011 L=81.0' S=0.0062 '/' Outflow=32.9 cfs 169,316 cf

Pond 36"-RCP: EX. 36" CULV

Peak Elev=114.18' Storage=182 cf Inflow=45.6 cfs 319,976 cf 36.0" Round Culvert n=0.011 L=57.0' S=0.0135 '/' Outflow=45.7 cfs 319,974 cf

Pond CB1:

Peak Elev=166.42' Inflow=0.5 cfs 1,594 cf 12.0" Round Culvert n=0.013 L=62.0' S=0.0081'/' Outflow=0.5 cfs 1,594 cf

Pond CB2:

Peak Elev=148.01' Storage=0 cf Inflow=6.4 cfs 30,429 cf

15.0" Round Culvert n=0.013 L=264.0' S=0.0049 '/' Outflow=6.4 cfs 30,430 cf

Pond CB3:

Peak Elev=130.55' Inflow=3.6 cfs 15,666 cf

12.0" Round Culvert n=0.013 L=34.0' S=0.0118'/' Outflow=3.6 cfs 15,666 cf

Pond CLV1: HW#1

Peak Elev=175.47' Storage=692 cf Inflow=7.1 cfs 67,278 cf

15.0" Round Culvert n=0.013 L=65.0' S=0.1231'/' Outflow=6.3 cfs 67,278 cf

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94"

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<u>Page 69</u> Pond GS-A: Grassed Swales Peak Elev=167.07' Storage=15,516 cf Inflow=8.9 cfs 29,691 cf

Outflow=1.2 cfs 15,612 cf

Pond GS-B: Grassed Swales Peak Elev=171.19' Storage=3,845 cf Inflow=3.2 cfs 10,832 cf

Outflow=2.5 cfs 7,796 cf

Pond GS-C: Grassed Swales Peak Elev=197.11' Storage=34,186 cf Inflow=21.3 cfs 71,029 cf

Outflow=4.1 cfs 41,526 cf

Pond GS-D: Grassed Swales Peak Elev=200.37' Storage=3,460 cf Inflow=4.1 cfs 14,075 cf

Outflow=3.5 cfs 11,796 cf

Pond GS-E: Grassed Swales Peak Elev=180.12' Storage=6,553 cf Inflow=6.3 cfs 20,944 cf

Outflow=5.6 cfs 15,612 cf

Pond SD: stone diaphragm Peak Elev=110.07' Storage=213 cf Inflow=10.8 cfs 57,513 cf

Outflow=10.8 cfs 57,306 cf

Pond WQS1: WQS1 Peak Elev=144.28' Storage=7,866 cf Inflow=16.8 cfs 133,326 cf

Primary=12.1 cfs 132,844 cf Secondary=0.0 cfs 0 cf Outflow=12.1 cfs 132,844 cf

Pond WQS2: WQS2 Peak Elev=143.90' Storage=835 cf Inflow=6.7 cfs 20,347 cf

Primary=6.7 cfs 20,276 cf Secondary=0.0 cfs 0 cf Outflow=6.7 cfs 20,276 cf

Pond WQS3: WQS3 Peak Elev=184.08' Storage=11,561 cf Inflow=12.2 cfs 40,839 cf

Primary=3.3 cfs 40,704 cf Secondary=0.0 cfs 0 cf Outflow=3.3 cfs 40,704 cf

Pond WQS4: WQS4 Peak Elev=114.33' Storage=6,177 cf Inflow=12.2 cfs 51,403 cf

Primary=5.3 cfs 48,705 cf Secondary=4.5 cfs 2,695 cf Outflow=9.8 cfs 51,400 cf

Link AP-2A: 36" RCP Inflow=45.7 cfs 319,974 cf

Primary=45.7 cfs 319,974 cf

Link AP-2B: 24" RCP Inflow=32.9 cfs 169,316 cf

Primary=32.9 cfs 169,316 cf Link AP1: AP-1

Inflow=12.2 cfs 68,803 cf

Primary=12.2 cfs 68,803 cf Link AP3: AP-3

Inflow=2.0 cfs 8,925 cf Primary=2.0 cfs 8,925 cf

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Page 70

Summary for Subcatchment P1: TO SD

Runoff =

1.7 cfs @ 12.15 hrs, Volume=

6,113 cf, Depth= 4.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

	Д	rea (sf)	CN [Description						
		370	98 F	Roofs, HSG A						
		288	98 F	Paved park	ing, HSG A	\				
		4,843	39 >	·75% Ġras	s cover, Go	ood, HSG A				
		0	96 (Gravel surfa	ace, HSG (
		7,790	74 >	75% Gras	s cover, Go	ood, HSG C				
		2,852	70 V	Voods, Go	od, HSG C					
		0	96 (Gravel surfa	ace, HSG A					
		16,143	64 V	Veighted A	verage					
		15,485	Ş	5.92% Pei	vious Area					
		658	4	.08% Impe	ervious Are	a				
	Tc	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	7.6	75	0.1540	0.16		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 3.15"				
	0.2	28	0.1540	1.96		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	0.1	46	0.1540	6.32		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0.4	55	0.0180	2.16		Shallow Concentrated Flow,				
_						Unpaved Kv= 16.1 fps				
	8.3	204	Total							

Summary for Subcatchment P10: TO GS-B

Runoff =

3.2 cfs @ 12.11 hrs, Volume=

10,832 cf, Depth= 6.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

Area (sf)	CN	Description
18,619	74	>75% Grass cover, Good, HSG C
2,220	96	Gravel surface, HSG C
320	98	Unconnected pavement, HSG C
21,159	77	Weighted Average
20,839		98.49% Pervious Area
320		1.51% Impervious Area
320		100.00% Unconnected

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			0 202	OTIVOCAL) Software Solutions LLC	Frinted 8/16/2021
(min)	ength (feet)	(1011)		_		Page 71
3.2	45	0.0667	0.23		Sheet Flow,	
1.8					Grass: Short n= 0.150 P2= 3.15"	
5.0	45	Total			Direct Entry, MIN. TC = 5.0 MIN	

Summary for Subcatchment P11: TO GS-C

Runoff

21.3 cfs @ 12.11 hrs, Volume=

71,029 cf, Depth= 5.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

					, at 0.00 ms
144,53 144,53	63 74 93 96 75 70 31 75	Descriptio >75% Gra Gravel sur Woods, Go Weighted / 100,00% P	ss cover, G face, HSG ood, HSG C		
Tc Leng (min) (fee 0.4		(ft/sec)	Capacity (cfs)	Description	
0.0	35 0.0570	1.23		Sheet Flow, GRVL DRV Smooth surfaces n= 0.011 P2= 3 Sheet Flow,	3.15"
1.8				Grass: Short n= 0.150 P2= 3.15"	
5.0 6	7 Total			Direct Entry, MIN. TC = 5.0 MIN	

Summary for Subcatchment P12: TO GS-D

Runoff

4.1 cfs @ 12.11 hrs, Volume=

14,075 cf, Depth= 6.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

			7 0.00 (1)3	
Area (sf) 17,020 7,895 442 103	70	Description >75% Grass cover, Good, HSG C Gravel surface, HSG C Woods, Good, HSG C >75% Grass cover C		-
25,460 25,460	٠,	>75% Grass cover, Good, HSG C Weighted Average 100.00% Pervious Area		_

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						<u> Page /2 </u>
Tc <u>(min)</u>	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	<u> </u>
0.3	28	0.0357	1.33		Charlet	
			1.00		Sheet Flow, grvl	
3.2	31	0.0322	0.40		Smooth surfaces n= 0.011 P2= 3.15"	
	0,	0.0322	0.16		Sheet Flow,	
0.5	4.0	0.0055			Grass: Short n= 0.150 P2= 3.15"	
0.5	16	0.0050	0.54		Sheet Flow,	
1.0					Smooth surfaces n= 0.011 P2= 3.15"	
5.0	75	Total			Direct Entry, 5.0 min.	
0.0	, ,	iolai				

Summary for Subcatchment P13: TO SWL1D

Runoff = 2.9 cfs @ 12.11 hrs, Volume=

10,060 cf, Depth= 6.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

	Area (sf) 10,471 6,726 320 33 17,550 17,230 320 320 320	74 96 98 74 83	Description >75% Grass cover, Good, HSG C Gravel surface, HSG C Unconnected pavement, HSG C >75% Grass cover, Good, HSG C Weighted Average 98.18% Pervious Area 1.82% Impervious Area 100.00% Unconnected					
To (min_ 0.3	(feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)				
		0.0630	1.70		Sheet Flow, grvl			
3.3	45	0.0630	0.23		Smooth surfaces n= 0.011 P2= 3.15" Sheet Flow,			
0.0	12	0.0630	4.04		Grass: Short n= 0.150 P2= 3.15" Shallow Concentrated Flow			
0.9	240	0.0750	4.41		Unpaved Kv= 16.1 fps Shallow Concentrated Flow,			
_ 0.5					Unpaved Kv= 16.1 fps			
5.0	327	Total	· · · · · · · · · · · · · · · · · · ·		Direct Entry, 5.0 min			

Summary for Subcatchment P14: TO WQS3

Runoff = 12.2 cfs @ 12.11 hrs, Volume=

40,839 cf, Depth= 6.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94" Printed 8/16/2021

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Page 73	Soliware Solutions LLC		Descriptio	CN	Area (sf)	-
					7,914	
		face, HSG	>75% Gra		70,819	
	od, HSG C	ss cover, Good, HSG (Woods G	70	2,271	
	1100 -	ed payoma	Unconnect	98	400	
	, HSG C	ed paveme ss cover, G	>75% Gras	74	0	
	o, HSG C	Verses	Neighted A	76	81,404	
		rvious Area	99.51% Pe		81,004	
		ervious Area	.49% Imp		400	
		nconnected	00.00% U		400	
				Slope	Length	Tc
	Pescription	Capacity (cfs)	Velocity (ft/sec)	(ft/ft)	(feet)	<u>(min)</u>
		(013)	1.29	0.0200	75	1.0
	heet Flow, GRASS		1120			4.0
	mooth surfaces n= 0.011 P2= 3.15"		2.28	0.0200	175	1.3
	rigitow Concentrator Elast.				405	0.4
	npaved Kv= 16.1 fps		5.19	0.1040	135	0.4
	nallow Concentrated Flow, npaved Kv= 16.1 fps					2.3
	rect Entry, 5.0 MIN.				205	5.0
	AND AND WALLY			Total	385	5.0

Summary for Subcatchment P15: TO CB3

Runoff 3.6 cfs @ 12.21 hrs, Volume=

15,666 cf, Depth= 6.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Area (sf) 12,202 4,836 14,188	70	Description >75% Grass cover, Good, HSG C Gravel surface, HSG C Woods, Good, HSG C
31,226 31,226	24.000	>75% Grass cover, Good, HSG C Weighted Average 100.00% Pervious Area

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94"

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				<u>.o riyuroCAL</u>	D Software Solutions LLC Page 74
Tc (min)	Length (feet)	(ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description Page 74
10.5	75	0.0680	0.12		Sheet Flow,
1.1	87	0.0680	1.30		Woods: Light underbrush n= 0.400 P2= 3.15" Shallow Concentrated Flow
0.3	114	0.1500	6.24		vvoodland Ky= 5.0 fps
0.2	81	0.1500	6.24		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Shallow Concentrated Flow, grvrl
1.0	115	0.1500	1.94		Onpaved Kv= 16.1 fps
0.3	78	0.1030	5.17		Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow,
13.4	550	Total		-	Unpaved Kv= 16.1 fps

Summary for Subcatchment P16: TO AP-3

Runoff = 2.0 cfs @ 12.23 hrs, Volume=

8,925 cf, Depth= 5.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

	Area (sf)	CN	<u>Description</u>	1						
	12,429	70	Voods, Go	Voods, Good, HSG C						
	7,386	<u> </u>	<u>>75</u> % Gras	s cover. Go	ood, HSG C					
	19,815	71 \	Veighted A	verage	50d, 1100 C					
	19,815	1	00.00% P	ervious Are	a					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
12.5	75	0.0440	0.10	(013)						
1.7	106	0.0440	1.05		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15" Shallow Concentrated Flow,					
0.6	78	0.1790	2.12		Shallow Concentrated Flow					
14.8	259	Total			Woodland Kv= 5.0 fps					
					— —					

Summary for Subcatchment P17: TO GS-E

Runoff = 6.3 cfs @ 12.11 hrs, Volume=

20,944 cf, Depth= 5.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94"

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	 -

Area (sf)	CN	Description Page 75
43,526 0	74 74	>75% Grass cover, Good, HSG C >75% Grass cover, Good, HSG C
43,526 43,526	74	Weighted Average 100.00% Pervious Area
To Longth	01.	

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.6	75	0.0800	2.24		Sheet Flow, GRVL DRV
0.3	49	0.0310	2.83		Smooth surfaces n= 0.011 P2= 3.15" Shallow Concentrated Flow CRM DRM
0.5	60	0.0170	2.10		Shallow Concentrated Flow
3.6					Unpaved Kv= 16.1 fps
5.0	184	Total			Direct Entry, 5.0 MIN

Summary for Subcatchment P18: TO SWL2

Runoff = 0.5 cfs @ 12.11 hrs, Volume=

1,546 cf, Depth= 5.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

Area (sf) 3,212 3,212	CN Description 74 >75% Grass cover, Good, HSG C 100.00% Pervious Area	-
Tc Length (min) (feet) 5.0	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs) Direct Entry, 5.0 MIN	

Summary for Subcatchment P19: TO WQS2

Runoff = 1.0 cfs @ 12.11 hrs, Volume=

3,190 cf, Depth= 5.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

Area (sf) 6,629	<u>CN</u>	Description 2759/ One
6,629		>75% Grass cover, Good, HSG C 100.00% Pervious Area

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94"

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P	age	_76

					TOTALIONIO LEO	Page 76
Tc (<u>min)</u>	(feet)	(ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
1.5	31	0.2260	0.35		Sheet Flow,	
3.5					Grass: Short n= 0.150 P2= 3.15"	
5.0	31	Total			Direct Entry, MIN TC = 5.0 MIN	
						 _

Summary for Subcatchment P2: TO WQS4

Runoff 9.3 cfs @ 12.16 hrs, Volume=

35,737 cf, Depth= 5.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

	Area (sf) 55,955 13,098 6,831 75,884 75,884	70 74 96 73	Description Woods, Go >75% Gras Gravel surf Weighted A 100.00% Po	od, HSG C s cover, G ace, HSG (verage	ood, HSG C C
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.4	75	0.1660	0.17	(0.0/	Sheet Flow,
0.4	55	0.1660	2.04		Woods: Light underbrush n= 0.400 P2= 3.15" Shallow Concentrated Flow
1.5	142	0.0950	1.54		vvoodland Kv= 5.0 fps
0.0	13	0.3300	9.25		Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow,
9.3	285	Total			Unpaved Kv= 16.1 fps

Summary for Subcatchment P3: TO AP1

Runoff 3.2 cfs @ 12.14 hrs, Volume=

11,497 cf, Depth= 7.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

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Page 7	AD Software Solutions LLC			CNI	<u>Area (sf)</u>	
			Descriptio			
	Good, HSG A	SS cover (>75% Gra		1,002	
	Λοου, 113G Α	face, HSG	Gravel sur	00	4,040	
	^	face, HSG	Gravel sur	96	6,422	
	ood, HSG C	SS COVER C	>75% Gra	74	5,625	
	, , , , , , , , , , , , , , , , , , ,	ood, HSG	Woods G	70	2,270	
	,	ood, HSG A	Woods G	30 1	76	
		od povez	Inconnect	98 l	256	
	nt, HSG C	eu paveme	Roofs, HS		15	
		3 A	Mojabta d. (19,706	
		werage	Weighted A		19,435	
		rvious Area	70.02% Pe	1	271	
	a	ervious Are	.30% Impe	1	256	
		connected	4.46% Un	9	200	
		_	1/-1- 1/	Slope	Length	Tc
	Description	Capacity	Velocity	(ft/ft)	(feet)	(min)
	,	(cfs)	(ft/sec)			4.1
	Sheet Flow,		0.30	0.1000	75	7.1
	Grass: Short n= 0.150 P2= 3.15"			0.400-	10	0.0
	Shallow Consented 1 72 3.15"		5.09	0.1000	12	0.0
	Shallow Concentrated Flow,				50	Λ 2
	Unpaved Kv= 16.1 fps		4.41	0.0750	53	0.2
L	Shallow Concentrated Flow, GRVL					2.0
	Olipaved KV= in 1 fne		2.55	0.0250	358	2.3
	Shallow Concentrated Flow,					
	Unpaved Kv= 16.1 fps			Total	498	6.6

Summary for Subcatchment P4: TO CB2

Runoff = 6.4 cfs @ 12.25 hrs, Volume= 30,429 cf, Depth= 5.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

36,514 7 29,013 7 525 9	74 70 <u>96</u> 72	Description >75% Grass cover, Good, HSG C Woods, Good, HSG C Gravel surface, HSG C Weighted Average 100.00% Pervious Area
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C Length (min) (feet) Slope (ft/ft) (ft/sec) Capacity (cfs)					OTTYGIOCAL	D Software Solutions LLC Page 78
8.3 40 0.0350 0.08 Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.15" 3.4 35 0.0350 0.17 Sheet Flow, Grass: Short n= 0.150 P2= 3.15" 2.3 290 0.0170 2.10 Shallow Concentrated Flow, Unpaved Kv= 16.1 fps 0.4 90 0.0560 3.81 Shallow Concentrated Flow, Unpaved Kv= 16.1 fps 1.4 105 0.0670 1.29 Shallow Concentrated Flow, Woodland Kv= 5.0 fps 0.5 211 0.1660 6.56 Shallow Concentrated Flow, Unpaved Kv= 16.1 fps 0.1 50 0.1500 Representation of the concentrated Flow, Unpaved Kv= 16.1 fps			- 1			
3.4 35 0.0350 0.17 Woods: Light underbrush n= 0.400 P2= 3.15" Sheet Flow, Grass: Short n= 0.150 P2= 3.15" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 16.1 fps Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	8.3	40	0.0350		(0.0)	Sheet Flow
0.4 90 0.0560 3.81 Unpaved Kv= 16.1 fps 1.4 105 0.0670 1.29 Unpaved Kv= 16.1 fps Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Unpaved Kv= 16.1 fps	3.4	35	0.0350	0.17		Woods: Light underbrush n= 0.400 P2- 3.45"
0.4 90 0.0560 3.81	2.3	290	0.0170	2.10		Grass: Short n= 0.150 P2= 3.15" Shallow Concentrated Flow
1.4 105 0.0670 1.29	0.4	90	0.0560	3.81		Unpaved Kv= 16.1 fps
0.5 211 0.1660 6.56 Voodland Kv= 5.0 fps Shallow Concentrated Flow, Unpayed Kv= 16.1 fps	1.4	105	0.0670	1.29		Unpaved Kv= 16.1 fps
0.1 FD 0.1-1	0.5	211	0.1660	6.56		Woodland Ky= 5.0 fps
Shallow Concentrated Flow	0.1	53	0.1510	6.26		Onpaved Kv= 16.1 fps Shallow Concentrated Flow
16.4 824 Total Unpaved Kv= 16.1 fps	16.4	824	Total			Unpaved Kv= 16.1 fps

Summary for Subcatchment P5A: TO EX.36"

Runoff 26.7 cfs @ 12.25 hrs, Volume=

126,153 cf, Depth= 5.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Area (sf)	CN	Description
0 187,867 75,981 9,587 400 273,835 263,848 9,987 400	96 70 74 98 98 72	Gravel surface, HSG C Woods, Good, HSG C >75% Grass cover, Good, HSG C Paved parking, HSG C Unconnected pavement, HSG C Weighted Average 96.35% Pervious Area 3.65% Impervious Area 4.01% Unconnected

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					Solutions LLC	
Tc (min)	Length (feet)	(ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	Page 79
1.1	27	0.3300	0.40		Sheet Flow,	
8.4	48	0.0490	0.10		Grass: Short n= 0.150 P2= 3.15" Sheet Flow.	
0.8	54	0.0490	1.11		Woods: Light underbrush n= 0.400 P2= 3.15 Shallow Concentrated Flow	5"
1.6	130	0.0770	1.39		Shallow Concentrated Flow	
2.5	305	0.1640	2.02	;	Shallow Concentrated Flow	
2.1	127	0.0390	0.99	;	Shallow Concentrated Flow	
16.5	691	Total		\	Woodland Kv= 5.0 fps	

Summary for Subcatchment P5B: TO EX.24"

Runoff 32.9 cfs @ 12.29 hrs, Volume= 169,318 cf, Depth= 5.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Area (sf)	CN	Description
5,494 277,852 52,653 20,671 2,721 139	96 70 74 98 98 74	Gravel surface, HSG C Woods, Good, HSG C >75% Grass cover, Good, HSG C Paved parking, HSG C Roofs, HSG C
359,530 336,138 23,392		>75% Grass cover, Good, HSG C Weighted Average 93.49% Pervious Area 6.51% Impervious Area

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Tc (min)	Length (feet)	(ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	<u>Page 80</u>	
2.1	57	0.3300	0.46	<u>-</u> -/	Sheet Flow,		
2.0	18	0.2500	0.15		Grass: Short n= 0.150 P2= 3.15" Sheet Flow,		
0.3	52	0.2500	2.50		Woods: Light underbrush n= 0.400 P2= 3.15 Shallow Concentrated Flow,	•	
5.9	209	0.0140	0.59		woodland Kv≈ 5.0 fps Shallow Concentrated Flow		
5.5	221	0.0180	0.67		Woodland Kv= 5.0 fps Shallow Concentrated Flow,		
2.4	117	0.0260	0.81		Woodland Kv= 5.0 fps Shallow Concentrated Flow,		
1.4	109	0.0700	1.32	;	vvoodland Kv= 5.0 fps Shallow Concentrated Flow		
19.6	783	Total			Woodland Kv= 5.0 fps		

Summary for Subcatchment P6: TO WQS1

Runoff = 3.2 cfs @ 12.11 hrs, Volume=

10,617 cf, Depth= 5.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

	Area (sf)	CN	<u>Description</u>)						
	21,626 <u>438</u>	74	>75% Grass cover, Good, HSG C Gravel surface, HSG C							
	22,064 22,064	74	Weighted A 100.00% Po	verage						
Tc (min)	Length (feet)	Slope (ft/ft)	(ft/sec)	Capacity (cfs)	Description					
1.8	35	0.1700	0.32		Sheet Flow,					
3.2					Grass: Short n= 0.150 P2= 3.15"					
5.0	35	Total			Direct Entry, MIN. TC = 5.0 MIN					

Summary for Subcatchment P7: TO GS-A

Runoff = 8.9 cfs @ 12.11 hrs, Volume=

29,691 cf, Depth= 5.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

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		<u>u .u.u.</u>	1030 @ 202	20 HydroCA	D Software Solutions LLC	Page 81
	rea (sf)	CN [<u>Description</u>	<u>1</u>		
	60,550 1,152 0	96 (3ravel surf.	s cover, Gace, HSG (ed paveme	ood, HSG C C nt. HSG C	
	61,702 61,702	74 V	Veighted A	verage ervious Are		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
0.5	75	0.1050	2.50	·/_	Sheet Flow, GRVL DRV	
0.1	39	0.1050	5.22		Smooth surfaces n≈ 0.011 P2= 3.15" Shallow Concentrated Flow, GRVI DRV	
0.1	30	0.1000	5.09		Unpaved Kv= 16.1 fps Shallow Concentrated Flow, GRVL DRV	
0.3	86	0.0700	4.26		Shallow Concentrated Flow, GRVI DRV	
0.0	19	0.3330	9.29		Unpaved Kv= 16.1 fps Shallow Concentrated Flow.	
0.2	59	0.1530	6.30		Unpaved Kv= 16.1 fps Shallow Concentrated Flow,	
3.8					Unpaved Kv= 16.1 fps	
5.0	308	Total ·			Direct Entry, MIN TC = 5.0 MIN	

Summary for Subcatchment P8: TO CB1

Runoff ≈

0.5 cfs @ 12.11 hrs, Volume=

1,594 cf, Depth= 5.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs NRCC 24-hr D 100-Year Rainfall=8.94"

	Area (sf) 3,312 3,312	74 >	Description 75% Gras 00.00% Pe		pod, HSG C
To <u>(min</u>		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.9	75	0.1180	0.32	(0.0)	Sheet Flow,
0.1	44	0.1180	5.53		Grass: Short n= 0.150 P2= 3.15" Shallow Concentrated Flow.
1.0	<u>) </u>				Unpaved Kv= 16.1 fps
5.0	119	Total			Direct Entry, MIN. TC = 5.0 MIN

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Page 82

Summary for Subcatchment P9: TO HW#1

Runoff

1.1 cfs @ 12.11 hrs, Volume=

3,895 cf, Depth= 7.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

/	Area (sf)		Description									
	3,729	74	7 V Oldss Cover, Good HSG C									
	0 2,728	90	Unconnect	Inconnected pavement HSG C								
	220	30 (Gravei surf	ace, HSG	C							
	6,677		Molarita	ed paveme	ent, HSG C							
	6,457		Weighted A 96.71% Pe	(Verage								
	220	3	3.29% Impe	rvious Area	3							
	220	1	100.00% U	nconnecte	ta d							
Τ.,	1 0				u .							
Tc (min)	Length	Slope	Velocity	Capacity	Description							
0.5	(feet)	(ft/ft)	(ft/sec)	(cfs)								
0.5	75	0.0950	2.40		Sheet Flow, GRVL DRV							
0.2	. 61	0.0660	4 4 4		Smooth surfaces n= 0.011 P2- 3.15"							
	σ,	0.0000	4.14		Stration Concentrated Flow CDVI DDV							
0.1	28	0.1430	6.09		Onpaved KV= 16.1 fps							
0.0					Shallow Concentrated Flow, Unpaved Kv= 16.1 fps							
0.2	103	0.2040	7.27		Shallow Concentrated Flow,							
_ 4.0					Unpaved Kv= 16.1 fps							
5.0	267	Total			Direct Entry, MIN. TC = 5.0 MIN							
0.0	201	Total										

Summary for Reach OF: TO WREP

Inflow Area ≈ 31,226 sf, 0.00% Impervious, Inflow Depth = 6.02" for 100-Year event Inflow 3.6 cfs @ 12.21 hrs, Volume= Outflow 15,666 cf

3.5 cfs @ 12.24 hrs, Volume= 15,666 cf, Atten= 2%, Lag= 1.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.70 fps, Min. Travel Time= 1.8 min Avg. Velocity = 0.67 fps, Avg. Travel Time= 4.5 min

Peak Storage= 371 cf @ 12.24 hrs

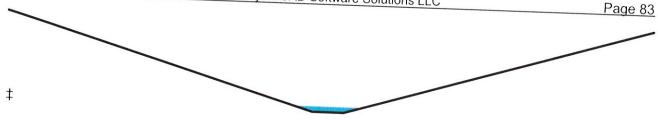
Average Depth at Peak Storage= 0.13', Surface Width= 22.62' Bank-Full Depth= 2.00' Flow Area= 220.0 sf, Capacity= 1,899.8 cfs

10.00' x 2.00' deep channel, n= 0.035 Earth, dense weeds Side Slope Z-value= 50.0 '/' Top Width= 210.00' Length= 180.0' Slope= 0.0389 '/' Inlet Invert= 129.00', Outlet Invert= 122.00'

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Summary for Reach OF2: FROM WREP

Inflow Area = 31,226 sf, 0.00% Impervious, Inflow Depth = 6.02" for 100-Year event Inflow

3.5 cfs @ 12.24 hrs, Volume= Outflow 15,666 cf

3.5 cfs @ 12.24 hrs, Volume= 15,666 cf, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.03 fps, Min. Travel Time= 0.5 min Avg. Velocity = 1.73 fps, Avg. Travel Time= 1.2 min

Peak Storage= 110 cf @ 12.24 hrs Average Depth at Peak Storage= 0.54', Surface Width= 3.23' Bank-Full Depth= 2.00' Flow Area= 12.0 sf, Capacity= 115.9 cfs

0.00' x 2.00' deep channel, n= 0.035 Earth, dense weeds Side Slope Z-value= 3.0 '/' Top Width= 12.00' Length= 126.0' Slope= 0.0556 '/' Inlet Invert= 122.00', Outlet Invert= 115.00'



Summary for Reach SWL1A:

Inflow Area = 280,391 sf, 0.31% Impervious, Inflow Depth = 3.95" for 100-Year event Inflow

9.0 cfs @ 12.18 hrs, Volume= 92,280 cf Outflow

9.0 cfs @ 12.19 hrs, Volume= 92,280 cf, Atten= 0%, Lag= 0.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.78 fps, Min. Travel Time= 0.4 min Avg. Velocity = 2.05 fps, Avg. Travel Time= 1.3 min

Peak Storage= 208 cf @ 12.19 hrs Average Depth at Peak Storage= 0.41', Surface Width= 4.46' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 263.5 cfs

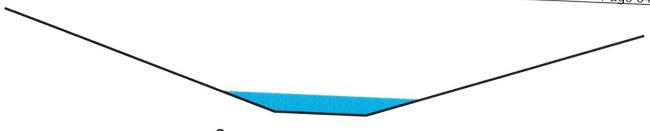
 $2.00' \times 2.00'$ deep channel, n= 0.035Side Slope Z-value= 3.0 '/' Top Width= 14.00' Length= 157.0' Slope= 0.1338 '/' Inlet Invert= 166.00', Outlet Invert= 145.00'

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Page 84



Summary for Reach SWL1B:

Inflow Area = 215,377 sf, 0.40% Impervious, Inflow Depth = 4.18" Inflow for 100-Year event

8.7 cfs @ 12.19 hrs, Volume= 75.074 cf

Outflow 8.7 cfs @ 12.19 hrs, Volume= 75,074 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.75 fps, Min. Travel Time= 0.0 min Avg. Velocity = 2.35 fps, Avg. Travel Time= 0.1 min

Peak Storage= 22 cf @ 12.19 hrs

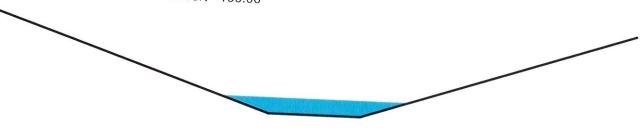
Average Depth at Peak Storage= 0.36', Surface Width= 4.18' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 322.2 cfs

2.00' x 2.00' deep channel, n= 0.035

Side Slope Z-value= 3.0 '/' Top Width= 14.00'

Length= 20.0' Slope= 0.2000 '/'

Inlet Invert= 170.00', Outlet Invert= 166.00'



Summary for Reach SWL1C:

Inflow Area = 187,541 sf, 0.17% Impervious, Inflow Depth = 4.06" Inflow 6.1 cfs @ 12.15 hrs, Volume= for 100-Year event

Outflow

63,382 cf 6.1 cfs @ 12.16 hrs, Volume= 63,382 cf, Atten= 0%, Lag= 0.7 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.89 fps, Min. Travel Time= 1.0 min

Avg. Velocity = 1.49 fps, Avg. Travel Time= 3.4 min

Peak Storage= 377 cf @ 12.16 hrs

Average Depth at Peak Storage= 0.39', Surface Width= 4.36'

Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 194.8 cfs

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Page 85

2.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 14.00' Length= 301.0' Slope= 0.0731 '/' Inlet Invert= 196.00', Outlet Invert= 174.00'

Summary for Reach SWL1D:

Inflow Area = 43,010 sf, 0.74% Impervious, Inflow Depth = 6.10" for 100-Year event Inflow Outflow

6.1 cfs @ 12.14 hrs, Volume= 21,856 cf

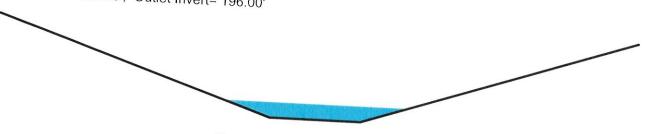
6.2 cfs @ 12.14 hrs, Volume= 21,856 cf, Atten= 0%, Lag= 0.1 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 5.84 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.66 fps, Avg. Travel Time= 0.3 min

Peak Storage= 26 cf @ 12.14 hrs Average Depth at Peak Storage= 0.35', Surface Width= 4.08' Bank-Full Depth= 2.00' Flow Area= 16.0 sf, Capacity= 249.6 cfs

2.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 14.00' Length= 25.0' Slope= 0.1200 '/' Inlet Invert= 199.00', Outlet Invert= 196.00'



Summary for Reach SWL2:

Inflow Area = 46,738 sf, 0.00% Impervious, Inflow Depth = 4.41" for 100-Year event Inflow 6.0 cfs @ 12.15 hrs, Volume= Outflow

5.9 cfs @ 12.16 hrs, Volume= 17.158 cf 17,158 cf, Atten= 1%, Lag= 0.6 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.20 fps, Min. Travel Time= 0.7 min Avg. Velocity = 1.97 fps, Avg. Travel Time= 2.2 min

Peak Storage= 252 cf @ 12.16 hrs Average Depth at Peak Storage= 0.56', Surface Width= 3.38' Bank-Full Depth= 2.00' Flow Area= 12.0 sf, Capacity= 173.6 cfs

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Page 86

0.00' x 2.00' deep channel, n= 0.035 Side Slope Z-value= 3.0 '/' Top Width= 12.00' Length= 265.0' Slope= 0.1245 '/' Inlet Invert= 178.00', Outlet Invert= 145.00'



Summary for Pond 24"-RCP: EX. 24" CULV

Inflow Area = 359,530 sf, 6.51% Impervious, Inflow Depth = 5.65" for 100-Year event 32.9 cfs @ 12.29 hrs, Volume= 169,318 cf 12.29 hrs, Volume= 32.9 cfs @ 12.29 hrs, Volume= 32.9 cfs @ 12.29 hrs, Volume= 169,316 cf, Atten= 0%, Lag= 0.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 101.54' @ 12.29 hrs Surf.Area= 132 sf Storage= 150 cf

Plug-Flow detention time= 0.8 min calculated for 169,316 cf (100% of inflow) Center-of-Mass det. time= 0.1 min (845.9 - 845.9)

Volume #1	Invert Av 98.00'	vail.Storage 4,909 cf	Storage Descriptio Custom Stage Da	n ta (Irregular)) ista		
Elevation (feet) 98.00 99.00 100.00 101.00 102.00 103.00 104.00 105.00 Device Rout	Surf.Area (sq-ft 15 42 79 189 809 1,937 3,963	(feet) 3.0 2.0 31.0 37.0 60.0 120.0 205.0 302.0	Inc.Store (cubic-feet) 0 7 27 60 130 463 1,333 2,890	Cum.Store (cubic-feet) 0 7 34 94 224 687 2,019 4,909	Wet.Area (sq-ft) 1 41 87 134 318 1,182 3,387 7,308	

#1 Primary 98.54' 36.0" Round Culvert

L= 81.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 98.54' / 98.04' S= 0.0062 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=32.7 cfs @ 12.29 hrs HW=101.51' TW=0.00' (Dynamic Tailwater)

1=Culvert (Inlet Controls 32.7 cfs @ 4.64 fps)

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Summary for Pond 36"-RCP: EX. 36" CULV

Inflow Area ≈ 777,113 sf, 1.45% Impervious, Inflow Depth = 4.94" for 100-Year event Inflow 45.6 cfs @ 12.24 hrs, Volume= Outflow 319,976 cf 45.7 cfs @ 12.24 hrs, Volume= Primary 319,974 cf, Atten= 0%, Lag= 0.5 min

45.7 cfs @ 12.24 hrs, Volume= 319,974 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 114.18' @ 12.24 hrs Surf.Area= 196 sf Storage= 182 cf

Plug-Flow detention time= 0.1 min calculated for 319,974 cf (100% of inflow) Center-of-Mass det. time= 0.0 min (887.0 - 887.0) Volume

<u>Volume</u> #1	Invert Ava 109.00'	ail.Storage	Storage Description	<u>1</u>		
Elevation (feet) 109.00 110.00 111.00 112.00 113.00 114.00 115.00 Device Rou	Surf.Area (sq-ft) 1 4 10 18 43 165 372 ting	412 cf Perim. (feet) 4.0 9.0 15.0 19.0 27.0 52.0 74.0	Inc. Store (cubic-feet) 0 2 7 14 30 97 262	Cum.Store (cubic-feet) 0 2 9 23 53 150 412	below (Recalc) Wet.Area (sq-ft) 1 9 26 46 83 245 475	

Outlet Devices #1 Primary 109.791 36.0" Round Culvert

L= 57.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 109.79' / 109.02' S= 0.0135 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 7.07 sf

Primary OutFlow Max=45.5 cfs @ 12.24 hrs HW=114.16' TW=0.00' (Dynamic Tailwater)
1=Culvert (Inlet Controls 45.5 cfs @ 6.44 fps)

Summary for Pond CB1:

Inflow Area = 3,312 sf, 0.00% Impervious, Inflow Depth ≈ 5.77" for 100-Year event Inflow 0.5 cfs @ 12.11 hrs, Volume= Outflow 0.5 cfs @ 12.11 hrs, Volume= 1.594 cf Primary 0.5 cfs @ 12.11 hrs, Volume= 1,594 cf, Atten= 0%, Lag= 0.0 min 1,594 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 166.42' @ 12.23 hrs

164.00' 12.0 L= 6 Inlet	let Devices "Round Culvert 52.0' CMP, projecting, no headwall, Ke= 0.900 / Outlet Invert= 164.00' / 163.50' S= 0.0081 '/' Cc= 0.900 .013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
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Page 88

Primary OutFlow Max=0.0 cfs @ 12.11 hrs HW=166.33' TW=166.37' (Dynamic Tailwater)

Summary for Pond CB2:

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 148.01' @ 12.25 hrs Surf.Area= 3 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.0 min (845.6 - 845.6)

Volume #1	Inv 148.0		Storage 119 cf	Storage Descriptio Custom Stage Da	on I ta (Irregular) l istor	1 holow	
	outing	Surf.Area (sq-ft) 3 50 154	Perim. (feet) 6.0 25.0 44.0	Inc.Store (cubic-feet) 0 22 97 t Devices	Cum.Store (cubic-feet) 0 22 119	Wet.Area (sq-ft) 3 52 162	
	rimary	144.30 Max=6 7 of a)' 15.0" L= 26 Inlet / n= 0.0	Round Culvert 4.0' CMP, projectin Outlet Invert= 144.3 013 Corrugated PE			

Primary OutFlow Max=6.7 cfs @ 12.25 hrs HW=148.00' TW=144.10' (Dynamic Tailwater)
1=Culvert (Barrel Controls 6.7 cfs @ 5.48 fps)

Summary for Pond CB3:

Inflow Are Inflow Outflow Primary	= =	3.6 cfs @	0.00% Impervious, 12.21 hrs, Volume= 12.21 hrs, Volume= 12.21 hrs, Volume=	45.000	for 100-Year event en= 0%, Lag= 0.0 min
--------------------------------------------	-----	-----------	-------------------------------------------------------------------------------------	--------	--------------------------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 130.55' @ 12.21 hrs

Device #1	Routing Primary	128.50'	Outlet Devices 12.0" Round Culvert L= 34.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 128.50' / 128.10' S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
			real of E, smooth interior, Flow Area = 0.79 sf

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Page 89

Primary OutFlow Max=3.5 cfs @ 12.21 hrs HW=130.51' TW=129.12' (Dynamic Tailwater)

1=Culvert (Inlet Controls 3.5 cfs @ 4.47 fps)

Summary for Pond CLV1: HW#1

Inflow Area = 194,218 sf, 0.28% Impervious, Inflow Depth = 4.16" for 100-Year event
Outflow = 6.3 cfs @ 12.35 hrs, Volume= 6.3 cfs

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 175.47' @ 12.35 hrs Surf.Area= 583 sf Storage= 692 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 0.4 min (918.1 - 917.7)

#1	174.00'		1,585 cf	Storage Descriptio Custom Stage Da	ita (Irregular)Listed	below	
(feet) 174.00 175.00 176.00 177.00		Area sq-ft) 274 583 583 583	Perim. (feet) 91.0 126.0 126.0 126.0	Inc.Store (cubic-feet) 0 419 583 583	Cum.Store (cubic-feet) 0 419 1,002 1,585	Wet.Area (sq-ft) 274 888 1,014 1,140	
Device Rou #1 Prim		173.0		Round Culvert	g. no headwall Ko		

L= 65.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 173.00' / 165.00' S= 0.1231 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=6.3 cfs @ 12.35 hrs HW=175.47' TW=170.34' (Dynamic Tailwater)
1=Culvert (Inlet Controls 6.3 cfs @ 5.16 fps)

Summary for Pond GS-A: Grassed Swales

Inflow Area = 61,702 sf, 0.00% Impervious, Inflow Depth = 5.77" for 100-Year event 29,691 cf 12.73 hrs, Volume= 1.2 cfs @ 12.73 hrs, Volume= 15,612 cf, Atten= 87%, Lag= 37.1 min 15,612 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 167.07' @ 12.73 hrs Surf.Area= 18,112 sf Storage= 15,516 cf

Plug-Flow detention time= 302.7 min calculated for 15,601 cf (53% of inflow) Center-of-Mass det. time≈ 162.5 min (992.2 - 829.7)

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					7 5 67 10 0	John Solutio	ns LLC			Page 90
Volume	<u>ir</u>	vert	Avail.St	orage	Storago F)oposis-ti-				<u> </u>
#1	165	5.50'		032 cf	Curt	Description				
			۷-۲,۱	332 CI	Custom	Stage Data (C	onic)Liste	d below x	4	
Elevati (fe. 165.9 166.9 167.0 167.5	et) 50 00 50 00	1, 3,0 4,3	Area q-ft) 434 736 038 340 542	(cubid	Store c-feet) 0 506 1,178 1,835 2,488	Cum.Store (cubic-feet) 0 506 1,685 3,520 6,008		et.Area (sq-ft) 434 1,737 3,042 4,348 5,656	7	
Device #1	Routing		Invert	Outle	t Devices					
#1	Primary		167.00'	6.0' lo Head 2.50 Coef.	ong x 2.0' (feet) 0.20 3.00 3.50	breadth Broa 0.40 0.60 0 2.54 2.61 2.6 3.32	7.00	1.20 1.40	1.60 1.80	2.00
Primary (OutFlow	May-1	2 of a (2)	40 -0.						

Primary OutFlow Max=1.2 cfs @ 12.73 hrs HW=167.07' TW=166.35' (Dynamic Tailwater)
1=Broad-Crested Rectangular Weir (Weir Controls 1.2 cfs @ 0.68 fps)

Summary for Pond GS-B: Grassed Swales

Outflow :	= = =	2.5 cfs @	1.51% Impervious, 12.11 hrs, Volume= 12.17 hrs, Volume= 12.17 hrs, Volume=	7.702 0	00-Year event 6, Lag= 3.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 171.19' @ 12.17 hrs Surf.Area= 4,102 sf Storage= 3,845 cf

Plug-Flow detention time= 194.2 min calculated for 7,796 cf (72% of inflow) Center-of-Mass det. time= 83.0 min (904.4 - 821.4)

Volume #1	Invert 169.50'	Avail.St		Description Stage Data (Pr	rismatic)Listed bel	low 2	
Elevation (feet) 169.50 170.00 170.50 171.00 171.50	1,	Area 5 <u>q-ft)</u> 184 736 ,288 840 392	Inc.Store (cubic-feet) 0 230 506 782 1,058	Cum.Store (cubic-feet) 0 230 736 1,518 2,576	audjinited bei	IOW X Z	
Device Rou #1 Prim		Invert	Outlet Devices				

#1 Primary Outlet Devices

#2 Primary 171.00' 6.0' long x 2.0' breadth Broad-Crested Rectangular Weir X 2.00 Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50

Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88

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2.85 3.07 3.20 3.32

Primary OutFlow Max=2.4 cfs @ 12.17 hrs HW=171.19' TW=170.36' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 2.4 cfs @ 1.09 fps)

Summary for Pond GS-C: Grassed Swales

Inflow Area = 144,531 sf, 0.00% Impervious, Inflow Depth = 5.90" for 100-Year event Inflow 21.3 cfs @ 12.11 hrs, Volume= Outflow 71,029 cf 4.1 cfs @ 12.47 hrs, Volume= 41,526 cf, Atten= 81%, Lag= 21.1 min Primary 4.1 cfs @ 12.47 hrs, Volume= 41,526 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 197.11' @ 12.47 hrs Surf.Area= 38,204 sf Storage= 34,186 cf

Plug-Flow detention time≃ 272.8 min calculated for 41,497 cf (58% of inflow) Center-of-Mass det. time= 140.1 min (967.0 - 826.9)

Volume Invert Avail.Storage Storage Description #1 195.501 50,064 cf Custom Stage Data (Prismatic)Listed below x 8 Elevation Surf.Area Inc.Store Cum.Store

(feet)	(sq-ft)	Inc.Store (cubic-feet)	Cum.Store
195.50 196.00 196.50 197.00 197.50	447 1,788 3,129 4,470 5,811	0 559 1,229 1,900 2,570	(cubic-feet) 0 559 1,788 3,688 6,258

Device Routing Invert Outlet Devices #1 Primary 6.0' long x 2.0' breadth Broad-Crested Rectangular Weir X 7.00 197.001 Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=4.1 cfs @ 12.47 hrs HW=197.11' TW=196.38' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 4.1 cfs @ 0.86 fps)

Summary for Pond GS-D: Grassed Swales

Inflow Area = 25,460 sf, 0.00% Impervious, Inflow Depth = 6.63" for 100-Year event Inflow 4.1 cfs @ 12.11 hrs, Volume= Outflow 14,075 cf 3.5 cfs @ 12.16 hrs, Volume= 11,796 cf, Atten= 16%, Lag= 2.8 min Primary 3.5 cfs @ 12.16 hrs, Volume= 11,796 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 200.37' @ 12.16 hrs Surf.Area= 3,428 sf Storage= 3,460 cf

Plug-Flow detention time= 140.1 min calculated for 11,796 cf (84% of inflow)

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Center-of-Mass det. time= 61.0 min (870.9 - 809.8)

<u>Volume</u>			,	*.0 003	.0)		
	ln	vert Avail:	Storage	0.			
#1	198.			Storage	Description		
			3,890 cf	Custom	Stage Date (a	nic)Listed below	
Elevatio	n	Court A			orage Data (Co	nic)Listed below	
(fee		Surf.Area	Inc	.Store			
		<u>(sq</u> -ft)	(cubic	<u>:5tore</u> <u>:-fe</u> et)	Cum.Store	Wet.Area	
198.5		281	Todbic		(cubic-feet)		
199.0		1,124		0	0	(sq-ft)	
199.5(1,967		328	328	281	
200.00)			763		1,125	
200.50)	2,810		1,188	1,091	1,971	
-		3,653		1,611	2,279	2,818	
Device F	Routing			,	3,890	3,667	
		Invert	Outlet	Devices		0,007	
#1 -	Primary	200.00'	E ALL	Devices			
		100,00	~·~ 10	ng x 2.0'	breadth Broad	Crash	
			riead ((feet) 0.2(0.40 0.60 0.00	Crested Rectangula 0 1.00 1.20 1.40 1.	r Weir
			Coef. (English)	254 261 22	2.60 2.66 2.70 2.77	20 1.00 2.00
			2.85 g	.07 3 20 °	3 22	2.60 2.66 2.70 2.77	200 000
Primary O	ifElou. A			5.20	3.32)0.36' TW-100.0	2.70 2.77	2.09 2.88
1=Broom	aru.1OM I∆	¹ax=3.4 cfs @	12.16 hr	re HIM-oc	10.04		
· Proat	パレFeste で	1 Pooton		3 11VV=2(/U 36' TW-100 o		

Primary OutFlow Max=3.4 cfs @ 12.16 hrs HW=200.36' TW=199.34' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 3.4 cfs @ 1.56 fps)

Summary for Pond GS-E: Grassed Swales

Inflow Are	a =	10 500		Grassed Swal	
Inflow Outflow Primary	~ = =	6.3 cfs @ 5.6 cfs @	0.00% Impervious, 12.11 hrs, Volume= 12.16 hrs, Volume= 12.16 hrs, Volume=	15,612 cf. Atte	for 100-Year event n= 12%, Lag= 2.5 min
Routing by	Dyn-S	Stor-Ind method	Timo Change	15,612 cf	1270, Lay- 2.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 180.12' @ 12.16 hrs Surf.Area= 9,367 sf Storage= 6,553 cf

Plug-Flow detention time= 177.1 min calculated for 15,612 cf (75% of inflow) Center-of-Mass det. time= 71.4 min (901.1 - 829.7)

<u>Volume</u>	InvertAvail S	· ·	,		
#1	170 504	Storage Storage	Description		
C 1	10,	,496 cf Custom	Stage Data (Price	matic)Listed below x 9	
Elevation	Surf.Area	l 04	0 410 (1 115)	matic)Listed below x 9	_
(feet)	(sq-ft)	iric.Store	Cum.Store		
178.50	75	(cubic-feet)	(cubic-feet)		
179.00	135	0	0		
179.50	540	53	53		
180.00	945	169	221		
180.50	1,350	371 574	593		
Device Rout		574	1,166		
		Outlet Devices			
#1 Prim.	ary 180.00'	6.0' long × 2 or			
		Head (feet) 0.20	breadth Broad-C	Prested Rectangular Weir V 0.00	

6.0' long x 2.0' breadth Broad-Crested Rectangular Weir X 9.00 Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00

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_____ Page 93

2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=5.5 cfs @ 12.16 hrs HW=180.12' TW=178.56' (Dynamic Tailwater)

1=Broad-Crested Rectangular Weir (Weir Controls 5.5 cfs @ 0.87 fps)

Summary for Pond SD: stone diaphragm

Inflow Area = 123,253 sf, 0.53% Impervious, Inflow Depth = 5.60" for 100-Year event Inflow = 10.8 cfs @ 12.26 hrs, Volume= Outflow 57,513 cf 10.8 cfs @ 12.26 hrs, Volume= 57,306 cf, Atten= 0%, Lag= 0.0 min Primary = 10.8 cfs @ 12.26 hrs, Volume= 57,306 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 110.07' @ 12.26 hrs Surf.Area= 200 sf Storage= 213 cf Flood Elev= 110.50' Surf.Area= 200 sf Storage= 247 cf

Plug-Flow detention time= 4.2 min calculated for 57,306 cf (100% of inflow) Center-of-Mass det. time= 1.8 min (850.9 - 849.1)

Volume #1	Invert 108.00'	169 cf	Custom Stage Data (Prismatic) istad by (2)
#2 	108.30'		= = = = = = = = = = = = = = = = = = =
		247 cf	Total Available Storage

247 cf Total Available Storage

Elevatio (fee 108.0 110.5	t) O	Surf.Area (sq-ft) 200 200	Inc.Store (cubic-feet) 0 500	Cum.Store (cubic-feet) 0 500

<u>Device</u> #1	Routing Primary	110.00'	Outlet Devices 195.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32
D'			

Primary OutFlow Max=10.5 cfs @ 12.26 hrs HW=110.07' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 10.5 cfs @ 0.73 fps)

Summary for Pond WQS1: WQS1

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_____Page 94

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 144.28' @ 12.45 hrs Surf.Area= 8,294 sf Storage= 7,866 cf Flood Elev= 143.10' Surf.Area= 4,391 sf Storage= 425 cf

Plug-Flow detention time= 23.5 min calculated for 132,751 cf (100% of inflow) Center-of-Mass det. time= 22.1 min (923.9 - 901.8)

				,			
<u>Volum</u> #1	e Inv	, (Vall.)	Storage	Storage Description			
		70 14	,736 cf	Custom Stage Data	a (Irregular)Listed	below (Recalc)	
Elevat (fe 143 144. 145.	eet) .00 .00	Surf.Area (sq-ft) 4,110 7,342 10,953	Perim. (feet) 838.0 863.0 882.0	Inc.Store (cubic-feet) 0 5,648 9,088	Cum.Store (cubic-feet) 0 5,648 14,736	Wet.Area (sq-ft) 4,110 7,599	
Device	Routing	Inver	t Outle	t Devices	11,730	10,378	
#1	Primary	139.50	' 15.0" Inlet /	Round Culvert OUT			
#2	Device 1	143.10	' 3.0" \	ert. LOW FLOW OU	TIET C-000	0251 7° Cc≈ 0.900 ow Area= 1.23 sf	
#3	Device 1	143.40'	48.0"	X 48.0" Horiz, TOP (neads NEBELOW MEN	C= 0 600	
#4	Secondary	/ 144.50'	10.0' I Head	d to weir flow at low hong x 10.0' breadth (feet) 0.20 0.40 0.60 (English) 2.49 2.56	EMERGENCY SP	ILLWAY	
Primary	OutFlow N	10v=10 0 -c	O 45 .		2.00	2.07 2.04	

Primary OutFlow Max=12.0 cfs @ 12.45 hrs HW=144.28' TW=112.63' (Dynamic Tailwater) 1=Culvert OUTLET (Inlet Controls 12.0 cfs @ 9.82 fps)

-2=LOW FLOW OUTLET (Passes < 0.2 cfs potential flow)

-3=TOP OVERFLOW WEIR (Passes < 43.4 cfs potential flow)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=143.00' TW=109.00' (Dynamic Tailwater) -4=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS2: WQS2

Inflow Area = Inflow = Outflow = Primary = Secondary =	6.7 cfs @ 6.7 cfs @ 6.7 cfs @ 0.0 cfs @	0.00% Impervious, 12.16 hrs, Volume= 12.16 hrs, Volume= 12.16 hrs, Volume= 0.00 hrs, Volume=	20,276 cf, Att	for 100-Year event en= 0%, Lag= 0.5 min
--------------------------------------------------------	--------------------------------------------------	----------------------------------------------------------------------------------------------------------	----------------	--------------------------------------------

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 143.90' @ 12.16 hrs Surf.Area= 1,215 sf Storage= 835 cf Flood Elev= 143.10' Surf.Area= 712 sf Storage= 69 cf

Plug-Flow detention time= 33.3 min calculated for 20,276 cf (100% of inflow) Center-of-Mass det. time= 30.9 min (916.4 - 885.6)

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Page 95

Volum			Storage	Storago Događaji		
#1	143.0		,575 cf	Storage Description Custom Stage Date	2 (lyna mal)	
Elevat		Surf.Area	Perim.	Custom Stage Data Inc.Store		below (Recalc)
143.		<u>(sq-ft)</u> 659	(feet) 196.0	(cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
144. 145.		1,283 1,984	225.0 251.0	0 954 1,621	0 954 2,575	659 1,653
Device	Routing	Inver	Outle	t Devices	2,070	2,666
#1	Primary	141.25	15.0"	Round Culvert OU	TLET L= 35.1' Ke	e= 0.500
#2	Device 1	143.10'	n= 0.(1.0" \	013 Corrugated PE, s	Smooth interior, Flo	
#3	Device 1	143.65'	48.0"	X 48.0" Horiz TOP	neads	_
#4	Secondary	144.50'	6.0' lo	ng x 10.0' breadth s	reads	
Primary	OutFlow M	1av=6 5 of @	Coef.	(feet) 0.20 0.40 0.60 (English) 2.49 2.56		

Primary OutFlow Max=6.5 cfs @ 12.16 hrs HW=143.90' TW=113.69 (Dynamic Tailwater) -1=Culvert OUTLET (Passes 6.5 cfs of 8.4 cfs potential flow)

-2=LOW FLOW OUTLET (Orifice Controls 0.0 cfs @ 4.19 fps)

-3=TOP OVERFLOW WEIR (Weir Controls 6.5 cfs @ 1.63 fps)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=143.00' TW=109.00' (Dynamic Tailwater) 4=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS3: WQS3

_				
Outflow : Primary : Secondary :	= 12.2 cfs @ = 3.3 cfs @ = 3.3 cfs @	0.49% Impervious, 12.11 hrs, Volume= 12.34 hrs, Volume= 12.34 hrs, Volume= 0.00 hrs, Volume=	40,704 cf, Atte	for 100-Year event n= 73%, Lag= 13.4 min
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	N/n Ctor In - I II I			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 184.08' @ 12.34 hrs Surf.Area= 5,691 sf Storage= 11,561 cf Flood Elev= 181.10' Surf.Area= 1,420 sf Storage= 134 cf

Plug-Flow detention time= 57.2 min calculated for 40,675 cf (100% of inflow) Center-of-Mass det. time= 55.5 min (879.6 - 824.2)

			··- /
Volume #1	Invert 181.00'	Avail.Storage 17,330 cf	Storage Description Custom Stage Data (Irregular)Listed below (Recalc)

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EL a				HARIOTIS EEC	
Elevation (feet) 181.00 182.00 183.00 184.00 185.00	Surf.Area (sq-ft) 1,261 3,271 4,534 5,604 6,810	Perim. (feet) 147.0 245.0 296.0 338.0 396.0	Inc.Store (cubic-feet) 0 2,188 3,885 5,060 6,197	Cum.Store (cubic-feet) 0 2,188 6,073 11,133 17,330	Wet.Area (sq-ft) 1,261 4,324 6,537 8,679 12,087
—					

				0,107	17,330	12,087	
Device	Routing	Invert	Outlet Devices	_		12,007	
#1	Primary	179.00'	CVICES	Cut. 4 Cut			
					LET L= 89.1' Ke		
#2	Device 1	181.10'	n= 0.013 Corr 3.0" Vert. LOV	ugated PE, sr	mooth interior, FIGURET X 3.00 $C=0$	ow Area= 1.77 sf	
#3	Device 1	181,90'	Limited to weir	flow at low bo	rei x 3.00 C= (0.600	
#4	Device 1	_	TO MEIL	HUM STIOM NA	ads S X 3.00 C= 0.6 ads		
	- 37100 1	184.00'	40.0 X 48.0" F	loriz TOP OV	/EDELOW/LAVELE	C= 0.600	
#5	Secondary	184.50'	10.0' long x 10	now at low ne.	ads		
. .			(5)	2.49 2.56 2.	.70 2.69 2.68 2.6	69 2.67 2.64	
Primary	OutFlow Max=	33 cfc @ 2	10.04			2.04	

Primary OutFlow Max=3.3 cfs @ 12.34 hrs HW=184.07' TW=113.60' (Dynamic Tailwater)

-1=Culvert OUTLET (Passes 3.3 cfs of 17.7 cfs potential flow)

-2=LOW FLOW OUTLET (Orifice Controls 1.2 cfs @ 8.13 fps)

-3=MIDDLE ORIFICES (Orifice Controls 1.0 cfs @ 6.89 fps)

-4=TOP OVERFLOW WEIR (Weir Controls 1.1 cfs @ 0.89 fps)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=181.00' TW=109.00' (Dynamic Tailwater) -5=EMERGENCY SPILLWAY (Controls 0.0 cfs)

Summary for Pond WQS4: WQS4

Inflow Area = Inflow = Outflow = Primary = Secondary =	107,110 sf, 0.00% Impervious, 12.2 cfs @ 12.18 hrs, Volume= 9.8 cfs @ 12.27 hrs, Volume= 5.3 cfs @ 12.27 hrs, Volume= 4.5 cfs @ 12.27 hrs, Volume=	51,403 cf 51,400 cf, Atten= 20%, Lag= 5.5 min
Position to p	_	4,000 0

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 114.33' @ 12.27 hrs Surf.Area= 3,736 sf Storage= 6,177 cf Flood Elev= 111.30' Surf.Area= 43 sf Storage= 2 cf

Plug-Flow detention time= 12.0 min calculated for 51,400 cf (100% of inflow) Center-of-Mass det. time= 11.6 min (848.0 - 836.3)

Volume	Invert	Avail.Storage	Storage Description Custom Stage Data (Irregular)Listed below (Recalc)
#1	111.20'	6,843 cf	

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Page 97

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Elevation (feet)	Surf.Area (sg-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area
111.20	10	5.0	0	(capic-leet)	(sq-ft)
111.50	179	88.0	0	0	10
112.00	1,102	222.0	23	23	624
113.00	2,495	276.0	288	311	3,931
114.00	3,426		1,752	2,062	6,085
114.50	3,908	314.0	2,948	5,011	7,894
	0,300	328.0	1,832	6,843	8,627
- .				,	0,027

- .	_		0,027
<u>Device</u>	Routing	Invert	Outlet Devices
#1	Primary	109.60'	12.0" Round Culvert OUTLET L= 134.0' CPP, projecting, no headwall, Kee 0.000
#2	Device 1	111.30'	n= 0.013, Flow Area= 0.79 sf 6.0" W x 3.0" H Vert. LOW FLOW OUTLET. C= 0.000
#3	Device 1	112.05'	8.0" W x 15.0" H Vert. MIDDLE WEID Co. 0.000
#4	Device 1	113.30'	48.0" x 48.0" Horiz. TOP WEIR C= 0.600
#5	Secondary	114.00'	10.0' long x 7.0' breadth EMERGENCY SPILLWAY Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.40 2.52 2.70 2.68 2.68 2.67 2.66 2.65 2.65 2.66 2.68 2.70 2.73 2.78

Primary OutFlow Max=5.2 cfs @ 12.27 hrs HW=114.31' TW=110.07' (Dynamic Tailwater)

1=Culvert OUTLET (Outlet Controls 5.2 cfs @ 6.68 fps)

-2=LOW FLOW OUTLET (Passes < 1.0 cfs potential flow)

-3=MIDDLE WEIR (Passes < 5.1 cfs potential flow)

-4=TOP WEIR (Passes < 53.0 cfs potential flow)

Secondary OutFlow Max=4.2 cfs @ 12.27 hrs HW=114.31' TW=110.07' (Dynamic Tailwater) 5=EMERGENCY SPILLWAY (Weir Controls 4.2 cfs @ 1.37 fps)

Summary for Link AP-2A: 36" RCP

Inflow Area = 777,113 sf, 1.45% Impervious, Inflow Depth = 4.94" for 100-Year event Inflow

45.7 cfs @ 12.24 hrs, Volume= 319,974 cf Primary

45.7 cfs @ 12.24 hrs, Volume= 319,974 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span≈ 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP-2B: 24" RCP

Inflow Area = 359,530 sf, 6.51% Impervious, Inflow Depth = 5.65" for 100-Year event Inflow = 32.9 cfs @ 12.29 hrs, Volume= 169,316 cf

Primary = 32.9 cfs @ 12.29 hrs, Volume= 169,316 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

139 Amesbury Line Road, Haverhill, MA NRCC 24-hr D 100-Year Rainfall=8.94"

Prepared by Goldsmith, Prest & Ringwall, Inc.

Printed 8/16/2021

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Page 98

Summary for Link AP1: AP-1

Inflow Area ≈ 142,959 sf, 0.65% Impervious, Inflow Depth = 5.78" for 100-Year event Inflow 12.2 cfs @ 12.26 hrs, Volume= Primary

68,803 cf 12.2 cfs @ 12.26 hrs, Volume= 68,803 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Summary for Link AP3: AP-3

Inflow Area = 19,815 sf, 0.00% Impervious, Inflow Depth = 5.41" for 100-Year event Inflow

2.0 cfs @ 12.23 hrs, Volume= Primary 8,925 cf

2.0 cfs @ 12.23 hrs, Volume= 8,925 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Pre-Development Conditions

139 Amesbury Line Road Haverhill, MA Project No. 181084

				Project No. 18108
Total Subcatchment Areas		Area (sf)	Area (Ac)	
Total Subcatchment Areas On-Site		1,299,417	29.8	
Total Area of Hydrolic Soil Groups On-Site		1,013,784	23.3	
James Con Croups On Site		1,013,784	23.3	
	A B	5,320 0	0.1	
	С	1,008,464	0.0 23.2	
Surface Type Areas	D	0	0.0	
Pavemen	t	30,546	0.7	
	٨			
	A C	288 30,258	0.0	
Roofs			0.7	
Rous		3,106	0.1	
	A C	385	0.0	· · · · · · · · · · · · · · · · · · ·
	C	2,721	0.1	
Gravel		4,836	0.1	
	А	0	0.0	
	С	4,836	0.1	
Grass Cover_		59,820	1.4	
	A	9,812	0.2	
)A(I	С	50,008	1.1	
Woods_		1,201,109	27.6	
	A	149	0.0	
otal Impervious Area	С	1,200,960	27.6	
		33,652	0.8	
filtration Volume				
ches of Recharge per Storm Event	۸	0.00		
	A B	0.60 0.35		
	С	0.25		
	D	0.10		
Itration Volume = \sum {[(Total Subcatchment Area	within HSG	i) - (Total Impervio	IIS Aroa within Lie are	
		. 1 milpervio	inches of Recharge Po	

20,555

CF

Infiltration Volume

Post Development Conditions

139 Amesbury Line Road Haverhill, MA Project No. 181084

Total Subcatchment Areas	Area (sf)	Area (Ac)	
Total Subcatchment Areas On-Site	1,299,417	29.8	
	1,013,784	23.3	
Total Area of Hydrolic Soil Groups On-Site	1.013,784	23.3	
A	5,320	0.1	
В	0	0.0	
C D	1,008,464 0	23.2	
	U	0.0	
Surface Type Areas			
Grass Cover	617,045	14.2	
A	E 0.45		
Ĉ	5,845 611,200	0.1	
<u> </u>	071,200	14.0	
Gravel	61,214	1.4	
А	4,040		
Ĉ	57,174	0.1 1.3	
	. 37,174	1.3	
Pavement	30,546	0.7	
А	200		
C	288 30,258	0.0	
	30,230	0.7	
Roofs	3,106	0.1	
A	385	0.0	
С	2,721	0.1	
Unconnected Pavement	1,916	0.0	
A C	0	0.0	
C	1,916	0.0	
Woods	585,590	13.4	
А	76	0.0	
C	585,514	13.4	
etal Impervious Area	35,568	0.8	

Post Development Conditions

139 Amesbury Line Road Haverhill, MA Project No. 181084

				Project No. 18108
Infiltration Volume				
Inches of Recharge per Storm Event	A B C D	0.60 0.35 0.25 0.10		
Infiltration Volume = $\sum \{[(Total Subcatchr)]$	nent Area w	rithin HSG) - (1	Total Imne	ervious Area within UCCN
		, ,	x (inc	hes of Recharge Per Storm)}
Natural Infiltration Volume		20,684	CF	
Pre-Development Infiltration Volume		20,555	CF	
Required Iniltration Volume		-129	CF	
Provided Infiltration Volume				
VQS1		425		
VQS2 VQS3		69	CF CF	Volume below 143.10' Orifice Volume below 143.10' Orifice
VQS4		134 2	CF CF	Volume below 181.10' Orifice Volume below 111.30' Orifice
otal Provided Iniltration Volume		630	CF	

Stormwater Management Standard 4 WATER QUALITY RETENTION VOLUME

139 Amesbury Line Road Haverhill, MA Project No. 181084

Parameter	Unit	Quantity	_
Watershed area		- activity	Remarks
Predevelopment impact	sf	1,013,784	
Total impervious area added Total impervious area Total impervious area Total impervious area required for retention	sf sf sf sf	33,652 1,916 35,568 1,916	
Runoff depth over impervious area			
Required Water Quality Volume	CF	1.0	
Provided Water Quality Volume	4 <u>======</u>	========	
WQS1			
WQS2 WQS3 WQS4		425 CF 69 CF 134 CF	Volume below 143.10' Orifice Volume below 143.10' Orifice
		² CF	Volume below 181.10' Orifice Volume below 111.30' Orifice
ESIGN VOLUME PROVIDED	CF	630	Onfice

Stormwater Management Standard 4 TSS REMOVAL

139 Amesbury Line Road Haverhill, MA Project No. 181084

Process Train No.	Impervious Area (SF)	BMP Type	TSS Removal Rate	TSS Remaining at Discharge	TSS Removed at Discharge
P6, P7, P10, P11, P12, P13*	880	Grass Swale (Dry) WQS1	50% 70%	50% 30%	50% 85%
P19*	00	(Dry) WQS2	70%	30%	100%
P14, P15*	00	(Dry) WQS3	70%	30%	100%
P2*	0	(Wet) WQS4	70%	30%	100%

^{* -} Impervious areas within Subcatchments P2.P6.P7,P10.P11.P12,P13,P14,P15 and P19 are limited to proposed unconnected concrete pad that will not produce sediment. Any runoff produced by these areas must flow through long stretches of existing grass and water quality swales prior to reaching a design analysis point and have been considered

ABBREVIATIONS:

TSS=total suspended solids; SF-square feet; SC-subcatchment; GC=grassed channel; BMP=best management practices; CB=deep CB=deep sump hooded catch basin; FB = Sediment Forebay; INF=infiltration basin; WB=wet basin; SP=Silt Prison Catch Basin

Stormwater Management Standard 4 TSS REMOVAL

139 Amesbury Line Road Haverhill, MA Project No. 181084

Process Train No.	Impervious Area (SF)	BMP Type	TSS Removal Rate	TSS Remaining at Discharge	TSS Removed at Discharge
5, P7, P10, P11, P12, P13*	880	Sediment Forebay WQS1	50% 70%	50% 30%	50%
P19*	0	WQS2	70%	30%	100%
P14, P15*	0	WQS3	70%	30%	100%
P2*	0	WQS4	70%	30%	100%

Total Development Weighted Average



^{* -} Impervious areas within Subcatchments P2,P6,P7,P10,P11,P12,P13,P14,P15 and P19 are limited to proposed unconnected concrete pad that will not produce sediment. Any runoff produced by these areas must flow through long stretches of existing grass and water quality swales prior to reaching a design analysis point and have been considered

ABBREVIATIONS:

TSS=total suspended solids; SF=square feet; SC=subcatchment; GC=grassed channel; BMP=best management practices: CB=deep CB=deep sump hooded catch basin; FB = Sediment Forebay; INF=infiltration basin: WB=wet basin; SP=Silt Prison Catch Basin

Infiltration Area Requirements

139 Amesbury Line Road Haverhill, MA Project No. 181084

Drawdown Time

(Per Massachusetts Stormwater regulations, infiltration areas must completely drain within 72 hours)

		mast complet
Infiltration Area Storage Volume		WQS1
Design infiltration Rate	cf	425
Infiltration Bottom Area	in/hr	0.27
D	sf	4,110

Drawdown Time = Infiltration Area Storage Volume / [Design Infiltration Rate x Infiltration Area Bottom Area]

Drawdown Time (Hrs)	
(113)	4.6

Infiltration Area Requirements

139 Amesbury Line Road Haverhill, MA Project No. 181084

Drawdown Time

(Per Massachusetts Stormwater regulations, infiltration areas must completely drain within 72 hours)

I m		WQS2
Infiltration Area Storage Volume	cf	69
Design infiltration Rate	in/hr	0.27
Infiltration Bottom Area	sf	659

Drawdown Time = Infiltration Area Storage Volume / [Design Infiltration Rate x Infiltration Area Bottom Area]

Drawdown Time (Hrs) 4.7

Infiltration Area Requirements

139 Amesbury Line Road Haverhill, MA Project No. 181084

Drawdown Time

(Per Massachusetts Stormwater regulations, infiltration areas must completely drain within 72 hours)

		WQS3
Infiltration Area Storage Volume	cf	134
Design infiltration Rate	in/hr	0.27
Infiltration Bottom Area	sf	1,261

Drawdown Time = Infiltration Area Storage Volume / [Design Infiltration Rate x Infiltration Area Bottom Area]

Drawdown Time (Hrs)	4.7
	=== <u>-</u>

Infiltration Area Requirements

139 Amesbury Line Road Haverhill, MA Project No. 181084

Drawdown Time

(Per Massachusetts Stormwater regulations, infiltration areas must completely drain within 72 hours)

	, anon area	as must completi
Infiltration Area Storage Volume	_	WQS4
Design infiltration Rate	cf	2
Infiltration Bottom Area	in/hr	0.27
Drawdown T	sf	10

Drawdown Time = Infiltration Area Storage Volume / [Design Infiltration Rate x Infiltration Area Bottom Area]

	 _	Ü	mardaon Rate X
Drawdown Time	(Hrs)		8.9

LONG TERM POLLUTION PREVENTION PLAN & STORMWATER SYSTEM OPERATION AND MAINTENANCE PLAN

Haverhill Solar Project 139 Amesbury Line Road Haverhill, MA

> April 2021 Revised August 2021

Submitted to:
City of Haverhill Department of Public Works
City of Haverhill Conservation Commission
4 Summer Street
Haverhill, MA 01830

<u>Submitted by:</u> Solar Smart, LLC 1207 Congressional BLVD Summerville, SC 29483

PREPARED BY:
GOLDSMITH, PREST & RINGWALL, INC.
39 MAIN STREET, SUITE 301
AYER, MA 01432

PROJECT No: 181084



Long Term Pollution Prevention Plan & Stormwater System Operation and Maintenance Plan Haverhill Solar Project 139 Amesbury Line Road, Haverhill, MA

Preface:

The goal of this manual is to improve water quality by initiating performance standards for the operation and maintenance of stormwater management structures, facilities, and recognized practices. The stormwater performance standards are set up to meet the stormwater management regulations under 974 CMR 4.08 and the Department of Environmental Protection, including the Wetland Protection Act, surface water discharge permits under the Clean Waters Act, and the 401 certification of federal permits based on the water quality standards.

The local Conservation Commission and the Department of Environmental Protection are responsible for ensuring the protection of wetlands through the issuance of permits for activities in flood plains and in or near wetlands, as per the Wetlands Protection Act, MGL c.131 s. 40. Proposed work within a resource area or a one hundred (100') foot buffer zone requires an order of conditions. Local wetland bylaws require a 35' no-disturbance zone be preserved around wetlands.

This manual is set up to explain how to operate and maintain Best Management Practices that control erosion and minimize delivery of sediment and other pollutants to surrounding water and wetland resource areas.

Chapter 1	is an introduction to the site and describes the Best Management Practices used on this site.
Chapter 2	outlines the inspection and maintenance schedules for the site.
Chapter 3	is an 11x17 drawing showing the location of the Best Management Practices used on-site.
Chapter 4	outlines the operation and function of the Best Management Practices.
Chapter 5	describes how and when the Best Management Practices should be inspected and how frequently they must be maintained and cleaned.
Chapter 6	describes the interface with parallel maintenance practices for the solar facility itself.

1. Introduction:

The subject site area measures 18.40± acres and is within the 26.81± acre subject property shown on the City of Haverhill Assessors Map 430, Parcel 11. The subject site area is being leased for a Large-Scale Ground-Mounted Solar Energy System, and this 18.40± acre portion of Map 430, Parcel 11 is referred to as the "Solar Lease Area," and is the only area to which this O&M Plan applies.

The leased area at 139 Amesbury Line Road contains a Large-Scale Ground-Mounted Solar Energy System anticipated to produce 2± MW electrical power utilizing solar photovoltaic (PV) modules/panels. The project consists of solar panel modules secured to galvanized steel racking fastened to driven steel posts for support and anchorage. The facility is ringed by chain link fencing with locked access gates. A single 22' wide gravel access driveway from Amesbury Line Road passes through the main gate of the facility and proceeds inside the fence line to two rack-mounted equipment such as wiring, conduits, inverters, transformers, etc, are also located within the fence line.

It is a potentially hazardous electrical area inside the fenceline that must be entered and maintained carefully with knowledge of all systems that are in operation.

Other environmental amenities such as an apiary and special seeding areas may also exist and like the electrical equipment, may have other maintenance requirements and restrictions listed elsewhere, not addressed in this Long Term Pollution Prevention Plan and Stormwater System Operations and Maintenance Plan – seek out proper guidance-elsewhere-for-maintaining-electrical-systems or other non-stormwater-related systems.

Most of the stormwater facilities requiring maintenance are inside the fence line, but some maintenance items are outside the fenced perimeter, as noted on the BMP Locus Map.

This manual is designed to help responsible parties become aware of urban non-point pollution problems and to provide detailed information about operating and maintaining stormwater management practices. The success of the Best Management Practices is dependent on their continued operations and maintenance.

2. Maintenance Requirements:

BMP's Owners:

 The OWNERS of the BMP's shall be the person, persons, trust, corporation, etc., or their successors who hold the long term lease on the land on which the BMP is located. It is anticipated that all BMP's will be owned and maintained by <u>Solar Smart, LLC</u>, or its designees, under a land lease from the land owner, Mr. Theodore Xenakis.

Operation and Maintenance Responsibilities:

- The party or parties responsible for the funding, operation and maintenance of the BMP's shall be the OWNER or their designees.
- BMP's each have specific maintenance requirements to ensure long-term effectiveness.
 These stormwater management systems will be operated, inspected and maintained on
 a regular basis by normal maintenance personnel. Any repair or replacement of the onsite BMP's, or any questions relating to required maintenance of stormwater BMP's
 should be observed/answered by a qualified professional with expertise in inspecting
 drainage system components. All of the stormwater BMP's shall be kept in good
 working order at all times.
- A maintenance agreement providing for the funding, operation and maintenance of all the stormwater management BMP's shall be provided.
- Snow storage areas have been indicated on the BMP Locus Plan, however, the site will
 only receive limited traffic from solar maintenance, and it is not anticipated that disposal
 of snow from the site will be required.
- Gravel access driveway shall receive regrading or repairing as needed in order to maintain grading and properly convey runoff without causing channeling or erosion of slopes and drainage swales. Access driveway shall be inspected every spring and fall of every year. Note evidence of rutting or uneven areas and make grading adjustments or repairs as needed.

Source of Funding for Operation and Maintenance:

- The party or parties responsible for the funding, operation and maintenance of the BMP's shall be the OWNER or their designees.
- Approximate estimated annual maintenance costs for the site BMP's are:

	Cultion I I and III	the site biving sare
-	Culvert Headwalls	\$50
-	Catch Basins	'
_	Grass Swales	\$50 each
		\$300
-	Stone Overflows	\$300
-	Conveyance Channels	\$300
-	Check Dams	
_	Sediment Forebay	\$250
		\$50
-	Water Quality Swales	\$150 each
-	Level Spreaders	
_	Stone Diaphragms	\$50 each
		\$50
-	Stone-Armored Channel	\$50
		400

Schedule for Inspection and Maintenance:

- Routine site inspections will be performed monthly for the first year and no less than annually thereafter.
- BMP's each have specific maintenance requirements to ensure long-term effectiveness.
 These stormwater management systems will be operated, inspected and maintained on a regular basis in accordance with this manual. All of the stormwater BMP's shall be kept in good working order at all times.
- As a minimum, the OWNER shall follow the general guidelines outlined herein for the BMP's provided on this site.
- An Operation and Maintenance log must be maintained in perpetuity, outlining inspections, repairs, replacement and/or disposal of each Best Management Practice (BMP). In the case of disposal of debris materials removed from BMP's that are to be disposed off-site, the log shall indicate the type of material being disposed of, and the disposal location. This rolling log shall be made available to the Mass DEP and/or the Haverhill Conservation Commission upon request.

3. Location of Best Management Practices (see plans sheet abbreviated BMP Locus Map in this document)	s or the

4. Operation of Best Management Practices:

The collective functions of all the Stormwater BMP measures include:

- Promoting groundwater recharge by providing pockets of storage volume that allow some water to infiltrate into soil;
- Providing distributed detention across the property;
- Controlling flow velocities with numerous energy breaks;
- Preventing erosion by limiting flow lengths of any localized rivulets;
- Lengthening total flow length and time of concentration, resulting in greater groundwater recharge and reduced peak discharges.

Stormwater BMP's on this site, and their specific functions consist of:

- 1. Culvert Headwall Protect pipe ends from wear and maintenance damage.
- 2. Catch Basin Collect concentrated surface flow and convey to piped outlet.
- 3. Grass Swales Convey flow and temporarily store runoff to promote recharge.
- 4. Stone Overflows & Spillways Provide a stable outlet for flows that exceed a storage volume.
- **5. Conveyance Channels** Provide a stable, concentrated flow path for drainage, particularly when combined with check dams, turf stabilization or other fabric and stone armoring combinations.
- **6. Check Dams-** Provide energy dissipation of flowing water and slowly releases flow through the uncompacted stone.
- 7. Sediment Forebay Provides coarse removal of total suspended solids, and in conjunction with other BMP's improves water quality.
- 8. Water Quality Swales (with Outlet Control Structures) Provide larger defined storage volumes that are slowly released via control structures and outlet pipes to reduce peak flow discharges.
- 9. Level Spreaders Provide a maintainable structural outlet from piped discharges or overflows, in order to produce non-erosive sheet flow discharges.
- **10.Stone Diaphragm** Provide a relatively small storage volume, flush to grade that can provide a measure of groundwater recharge and conveyance, and also serve as a level spreader outlet device.
- **11.Stone-Armored Channel** Functions as an erosion and sedimentation control measure for concentrated flow.

5. Inspection and Maintenance of Best Management Practices:

Upon the completion of construction, inspections must be conducted monthly for the first year to ensure adequate stabilization and function with appropriate adjustments and repairs made in a timely fashion to avoid excessive degradation. Regular maintenance thereafter is as listed below.

For all maintenance practices that involve the removal of debris from the subject Solar Lease Area, collected sediment and debris will be properly disposed of per local, state and federal requirements. Any sediment and debris removed from a catch basin deemed to be contaminated must be evaluated in accordance with the Hazardous Waste Regulations, 310 CMR 30.000, and handled as hazardous waste.

Culverts and Culvert Headwalls- are pipe connections to convey water from one open flow condition to another. The inspection and maintenance procedures for this measure include:

- Inspect twice a year, Spring and Fall, after 1st year.
- Remove collected debris and sediments from inlet and outlets.
- Repair rutting or erosion at the inlet or outlet.
- · Observe any deformations in the pipe and headwalls and if the pipe is crushed or structurally damaged, repair or replace as appropriate.

Catch Basins- are drainage structures topped with a grate that has the function of collecting stormwater and transporting it via underground piping to other areas on site. There are two catch basins along the entry driveway, both outside the fence line. The inspection and maintenance procedures for this measure include:

- Inspect twice a year, Spring and Fall, after 1st year.
- Remove collected debris and sediments from sump.
- Observe any deformations or damage in structure. Repair or replace as

Grass Swales- are nearly level, flat sloped (<0.5%) ditches set parallel to grade contours, or perpendicular to the gradient of the hillside slopes, intended to capture sheet flow from limited upland areas, and temporarily hold the water for recharging to groundwater. Each Grass Swale slopes towards a single Stone Overflow that discharges a controlled flow to a Conveyance Channel.

The inspection and maintenance procedures for this measure include:

- Inspect annually, after 1st year.
- Remove sediment from grass channel annually.
- Mow once a month during growing seasons, or as warranted by site
- Revegetate as needed for permanent cover.
- Inspect Stone Overflow See Stone Overflows & Check Dams.

Stone Overflows & Check Dams- are barriers to slow concentrated flow in swales, ditches and channels consisting of a core of stone (in Check Dams) or soil (in Stone Overflow), overlaid with geotextile fabric and a covering later of larger stone. The inspection and maintenance procedures for this measure include:

- Inspect annually, after 1st year.
- Remove accumulated sediments and debris at the upstream base.
- Remove collected debris from the topping stone.
- Repair rutting or erosion at the stone edges where the Overflow or Check Dam is keyed into the adjacent earthen areas.
- Restore or replace shifted rock or stone for proper erosive armoring or
- Water Quality Swale #4 has a wider (10' width) stone overflow that activates at the 100-year storm event and should be maintained in a similar fashion as the remainder of the stone overflows and check dams.

Conveyance Channels- are sloped ditches intended to convey a range of flows and control erosive velocities and sediment transport with multiple check dams. The inspection and maintenance procedures for this measure include:

- Inspect annually, after 1st year.
- Remove debris and accumulated sediments annually.
- Mow annually or as needed during growing seasons to prevent shading.
- Revegetate as needed for permanent cover.
- Inspect Check Dams See Stone Overflows & Check Dams.

Sediment Forebay – is a small stormwater runoff impoundment to capture coarse debris and suspended solids for pre-treatment in a water quality treatment train, with a check dam outlet. The inspection and maintenance procedures for this

- Inspect twice a year, after 1st year.
- Remove debris and accumulated sediments.
- Repair rutting or erosion, particularly at the Check Dam outlet.
- Cut out and remove woody growth and stems.

Water Quality Swales (with Outlet Control Structures) - are stormwater runoff impoundments with outlet control structures that slow the release of the impoundment volume. The inspection and maintenance procedures for this

- Inspect twice a year, Spring and Fall, after 1st year.
- Remove debris and accumulated sediments from inside the swales and from surrounding stone-armored areas.

- Repair rutting or erosion, particularly at the outlet control structure.
- Cut out and remove woody growth and stems, inside the impoundment, from the top of the embankment, and on the embankment itself.
- Mow once a month during growing seasons, or as warranted by site conditions.

Level Spreaders— consist of large, perforated pipes set parallel to the receiving grade, partially buried and stone covered to dissipate energy and convert concentrated flow to non-erosive sheet flow. The inspection and maintenance procedures for this measure include:

- Inspect annually, after 1st year.
- Remove accumulated debris sufficiently to expose the stone armoring.
- Repair rutting or erosion at the stone edges.
- Restore or replace shifted rock or stone for proper erosive armoring.
- Revegetate as needed.

Stone Diaphragms and Swales— are excavated trenches lined with geotextile fabric and filled with stone, set flush to surrounding grades. The Stone Diaphragms on this project have perforated pipes embedded in the stone to promote capture, flow and recharge or overflow of captured surface waters. The inspection and maintenance procedures for this measure include:

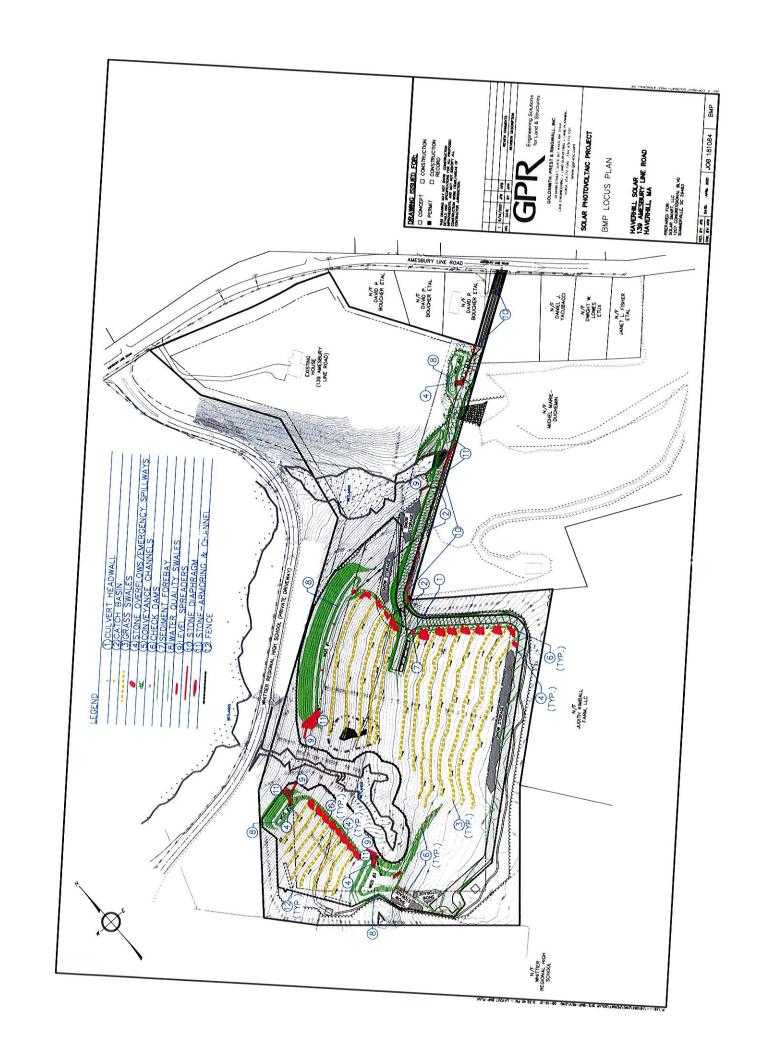
- Inspect annually, after 1st year.
- Remove accumulated debris sufficiently to expose the surficial stone.
- Repair rutting or erosion at the stone edges.
- Restore or replace transported rock or stone on top of the diaphragm limits.

Stone Armored Channel— is a basic erosion control measure consisting of stone on geotextile fabric to promote non-erosive flow in a ditch. There is only a short section of this treatment along the entry driveway. The inspection and maintenance procedures for this measure include:

- Inspect annually, after 1st year.
- Remove accumulated debris sufficiently to expose the surficial stone.
- Repair rutting or erosion at the stone edges.
- Restore or replace transported rock or stone on top of the diaphragm limits.

6. Solar Facility Maintenance Notes:

Solar Facility Maintenance is detailed in other documents by Solar Smart, LLC, which includes a schedule for solar equipment inspection and maintenance, fence maintenance, driveway maintenance, and may include maintenance of other environmental features such as observation platforms, apiary and specialty seeding areas. Caution and care must be exercised in all use of hand tools and mechanical maintenance equipment so as not to damage any portion of the solar facility equipment or amenities. If any damage occurs to any portion of the land or solar facility equipment, or if suspected damage of any kind is identified or suspected upon observance, the Owner must be notified immediately.



Best Management Practices (BMP) Inspection Log

Project Name	General Information
Location	Traverilli Solar Smart Solar Busi
Date of Inspection	139 Amesbury Line Rd. Haverhill, MA
Inspector's Name(s)	Start/End Time
Inspector's Title(s)	
Inspector's Contact Information	
Inspector's Qualifications	
Type of Inspection: ☐ Regular ☐ Emergency	
Weather at time of this inspection?	Weather Information
I Clear I Cloudy I Rain I Other: re there any discharges at the time of yes, describe:	Sleet 17 C
Site-specific BMPs	

- The structural BMPs are identified on the BEST MANAGEMENT PRACTICES LOCUS included within the LONG TERM POLLUTION PREVENTION & STORMWATER SYSTEM OPERATION & MAINTENANCE PLAN. Carry a copy of the Locus map with you during your inspections. This list will ensure that you are inspecting all required BMPs at your site.
- Describe corrective actions initiated, date completed, and note the person that completed the work in the

BMP	BMP	BMP	l. and note the person that completed the work in the	
	Installed?	Maintenance	Corrective Action Needed and Notes	
)	□Yes □No	Required?		
	□Yes □No			
	UYes UNo	QYes QNo		
	UYes UNo	□Yes □No		
	UYes UNo	UYes UNo		
	UYes INO	UYes UNo		
	UYes DNo	UYes UNo		
	OYes ONo	□Yes □No		
	OYes ONo	□Yes □No	·	
	UYes JNo	UYes UNo		
	Ures JNo	□Yes □No		

Overall Site Issues

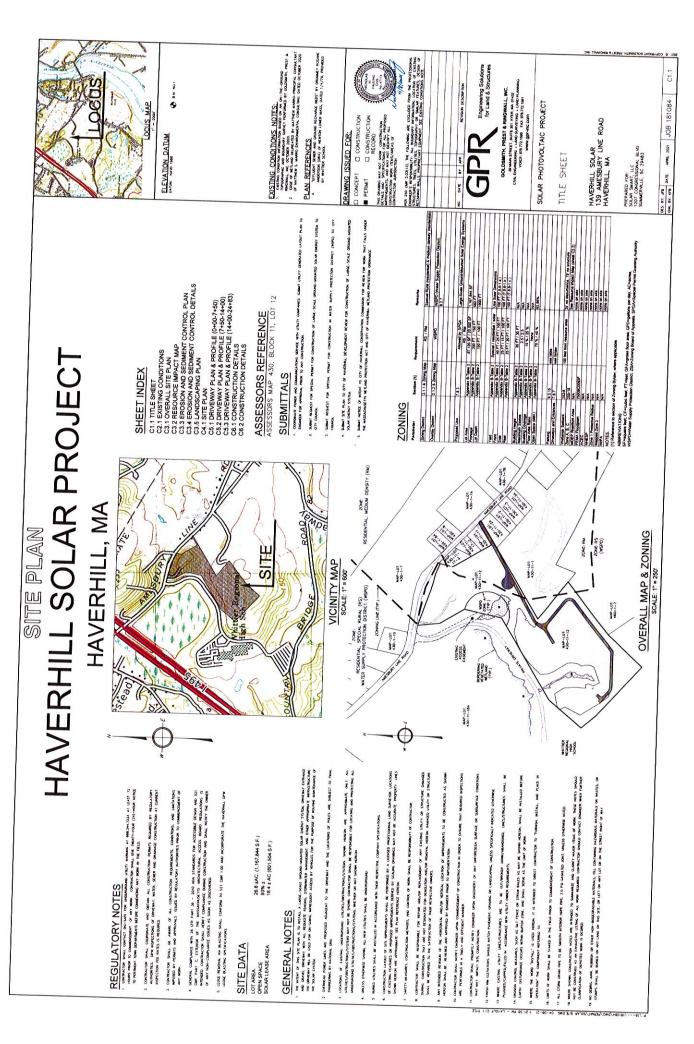
Below are some general site issues that should be assessed during inspections. Customize this list as needed for conditions at your site.

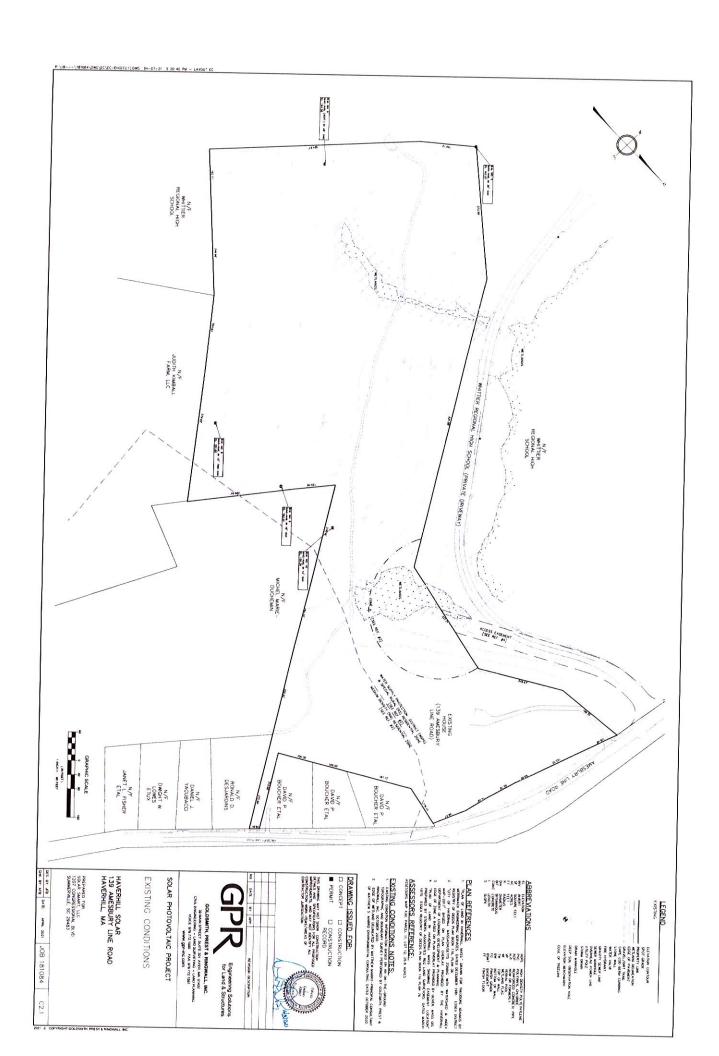
	BMP/activity	Implemented?	Maintenance Required?	Corrective Action Needed and Notes
1	Are discharge points and receiving waters free of any sediment deposits?	□Yes □No	□Yes □No	
2	Are storm drain inlets properly working?	□Yes □No	□Yes □No	
3	Is trash/litter from site areas collected and placed in covered dumpsters?	□Yes □No	□Yes □No	
4	Are vehicle and equipment fucling, cleaning, and maintenance areas free of spills, leaks, or any other deleterious material?	□Yes □No	Yes No	
5	Are materials that are potential stormwater contaminants stored inside or under cover?	UYes INo	□Yes □No	
5	Are non-stormwater discharges (e.g., wash water, dewatering) properly controlled?	□Yes □No	□Yes □No	- · · · · · · · · · · · · · · · · · · ·
,	(Other)	□Yes ¬No	□Yes □No	
 Jesei	ribe any incidents of non-con	npliance not descr	Non-Complian	ce

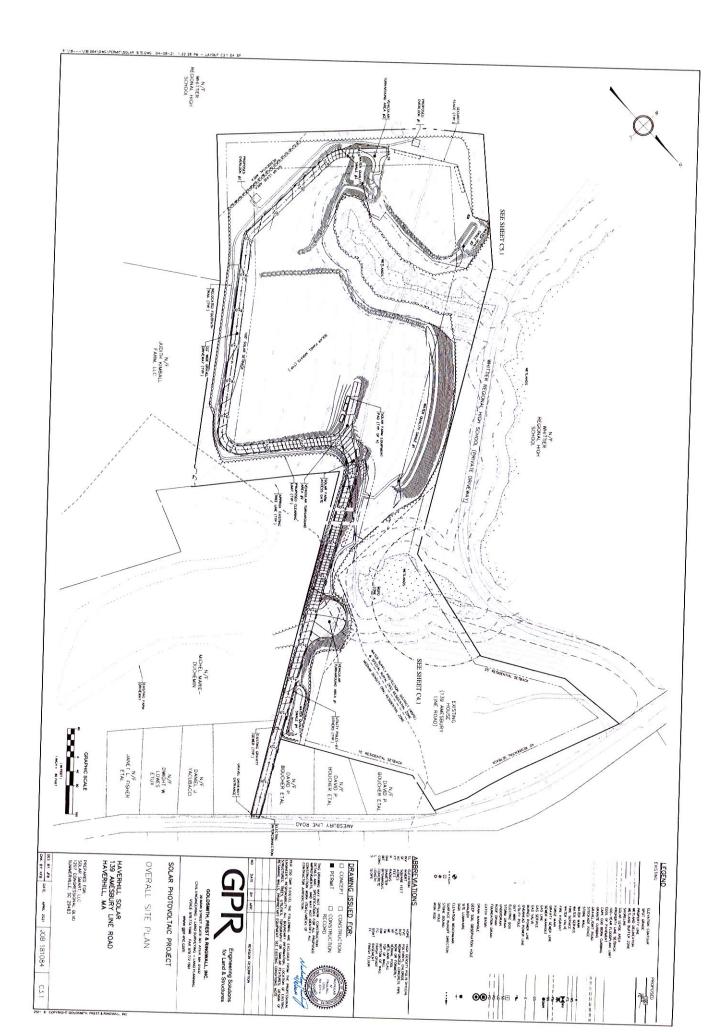
CERTIFICATION STATEMENT

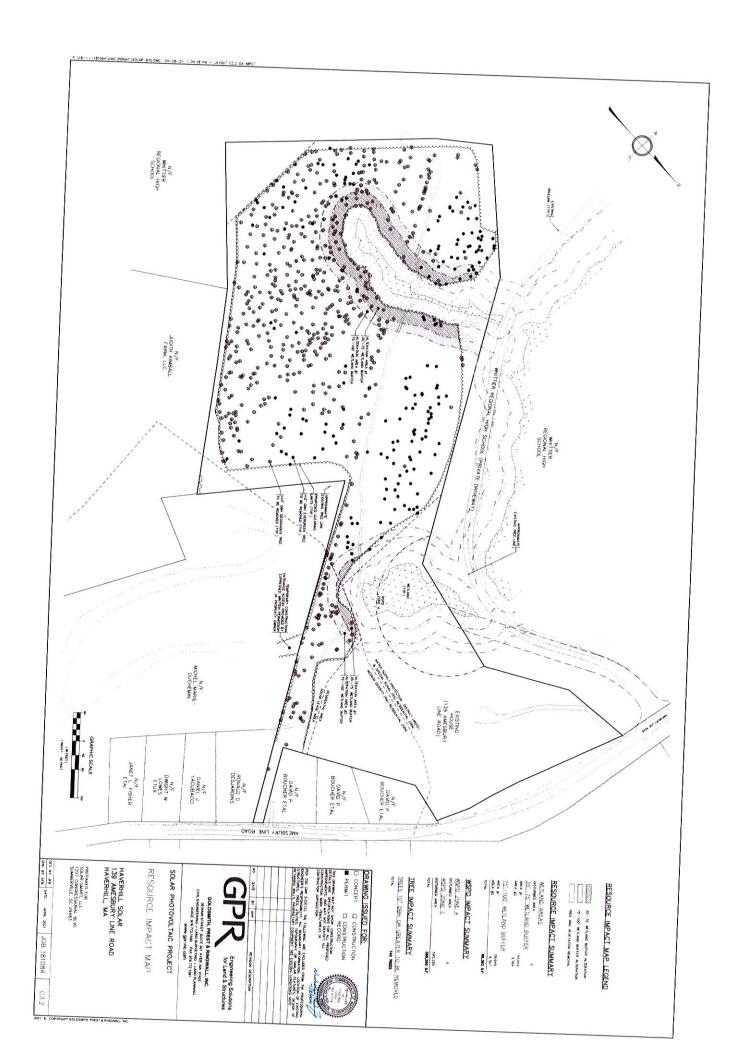
"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations."

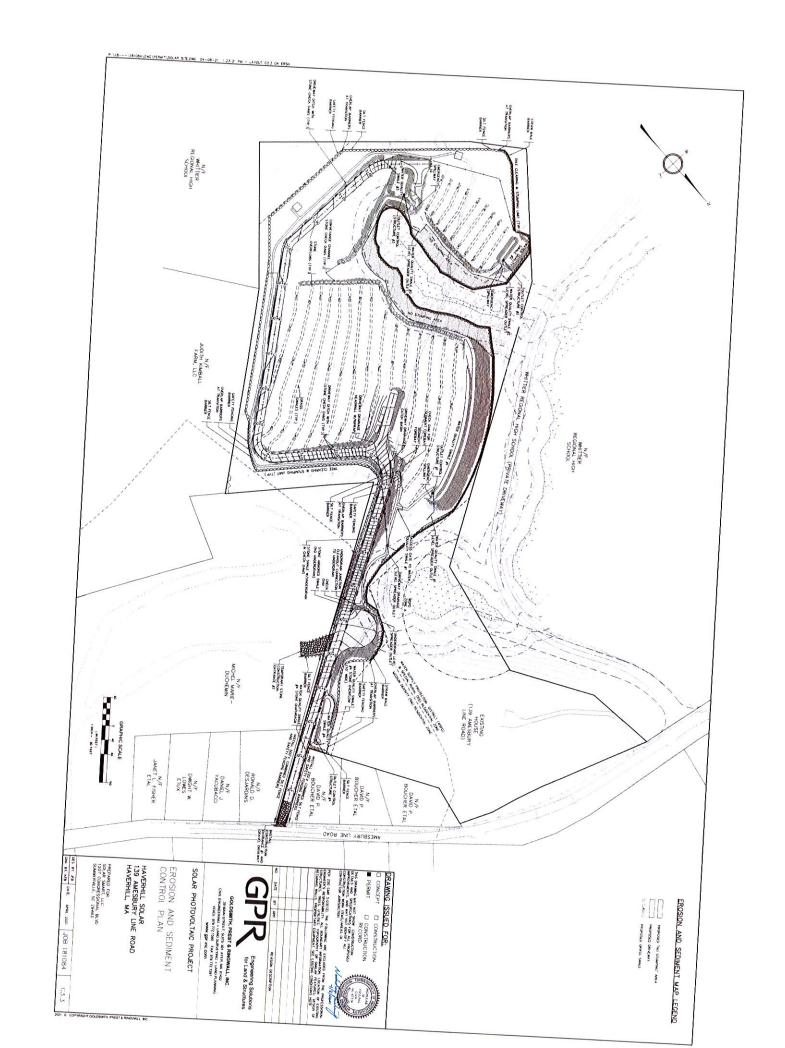
Print name and title:	
Signature:	Date:

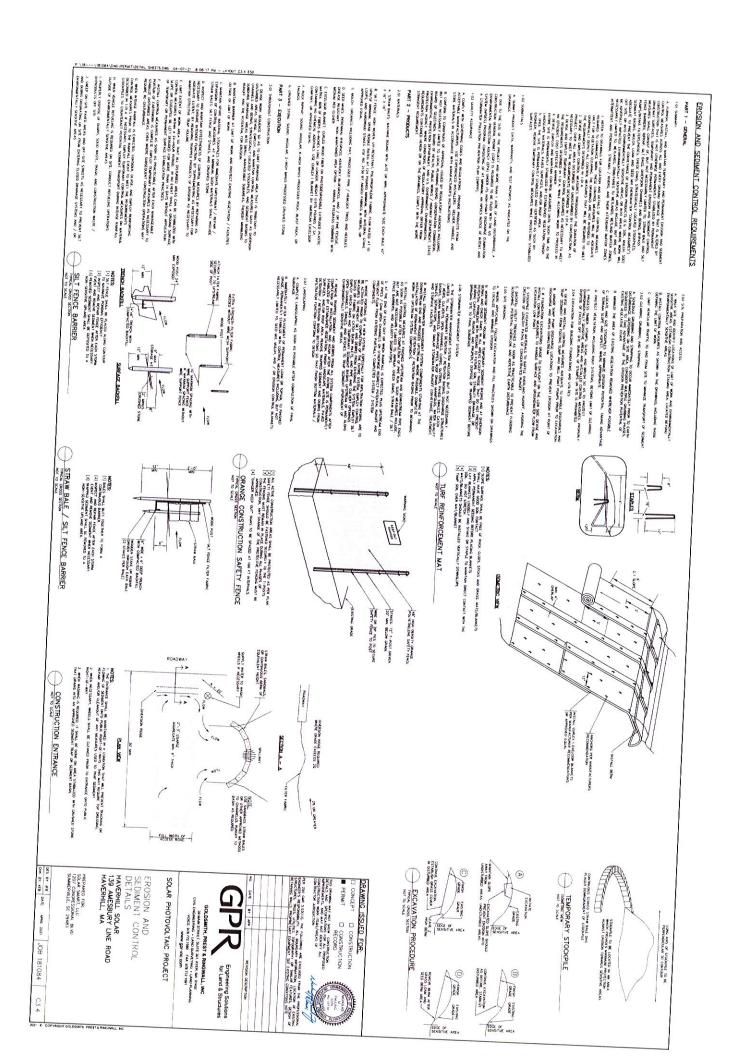


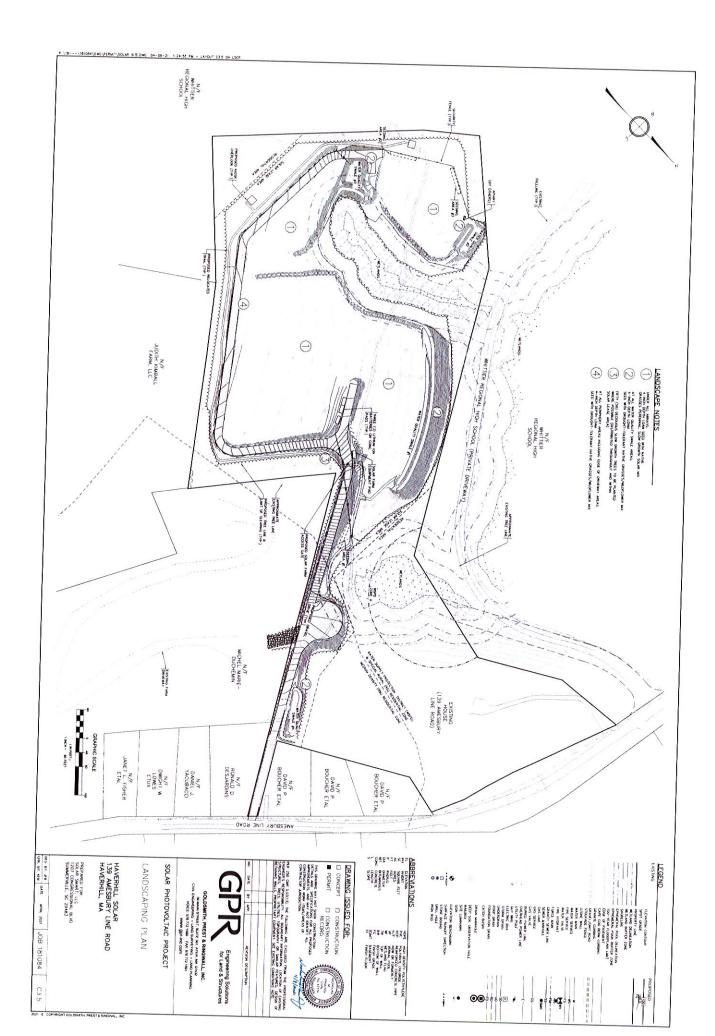


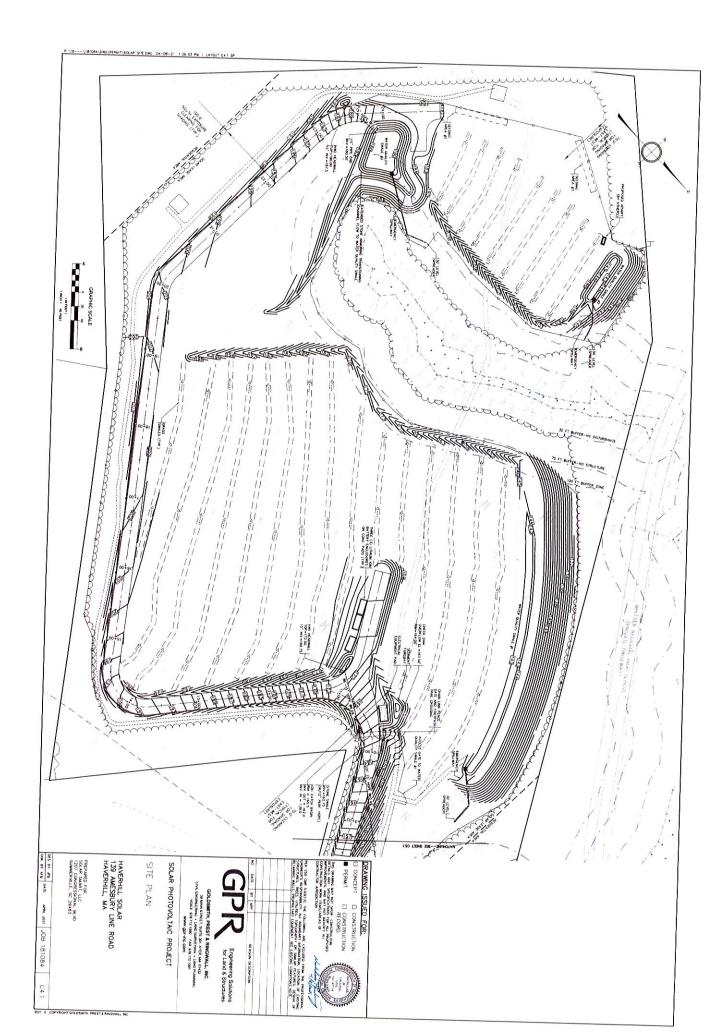


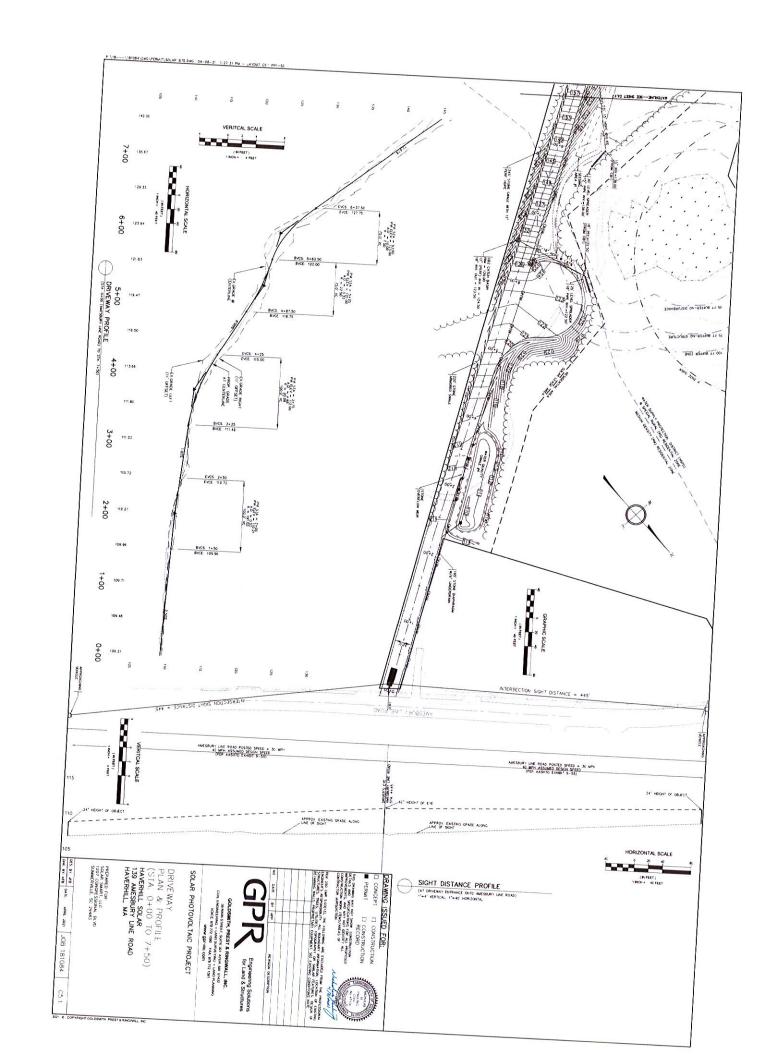


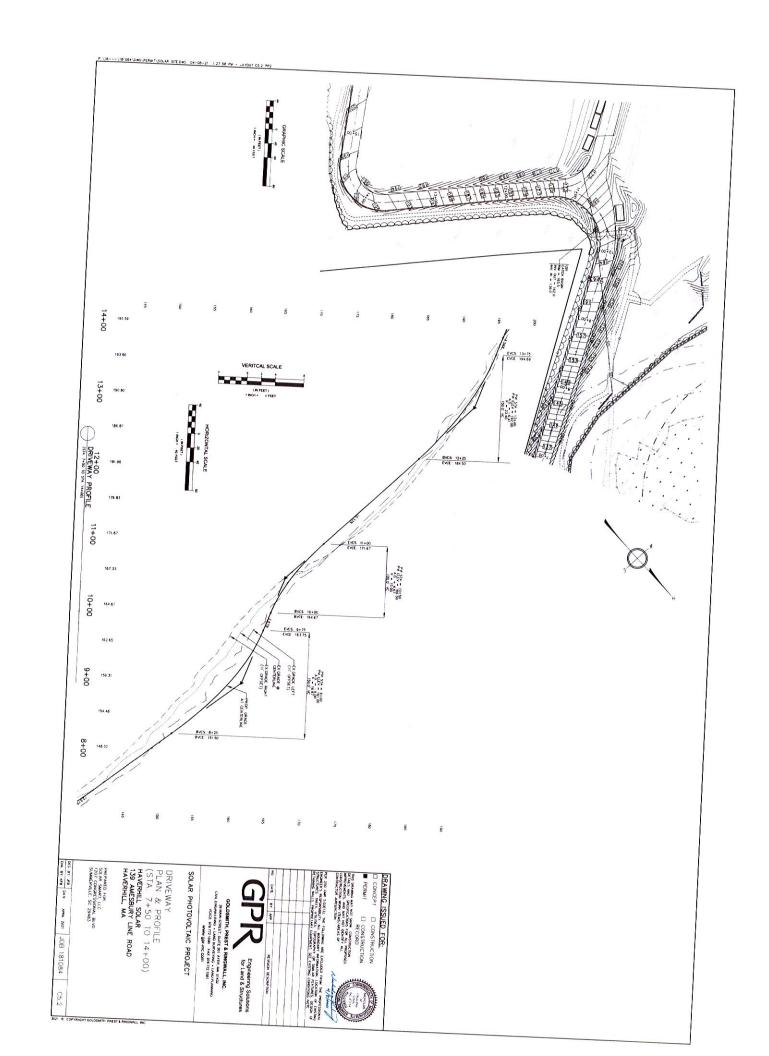


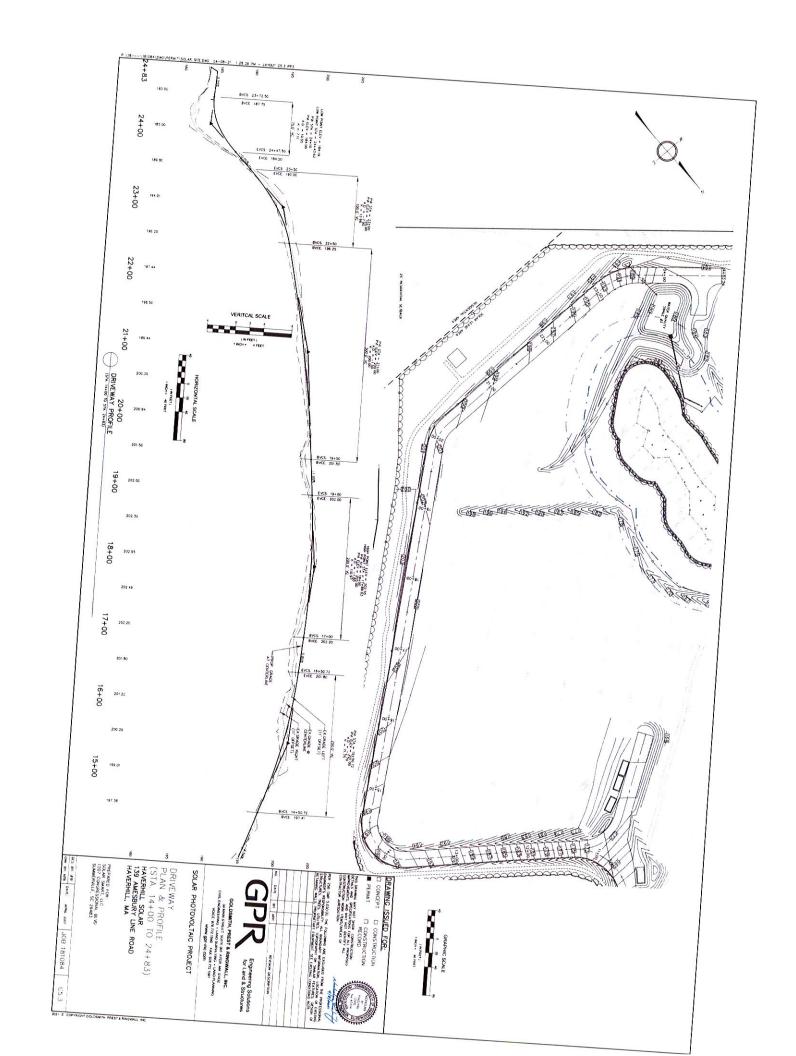


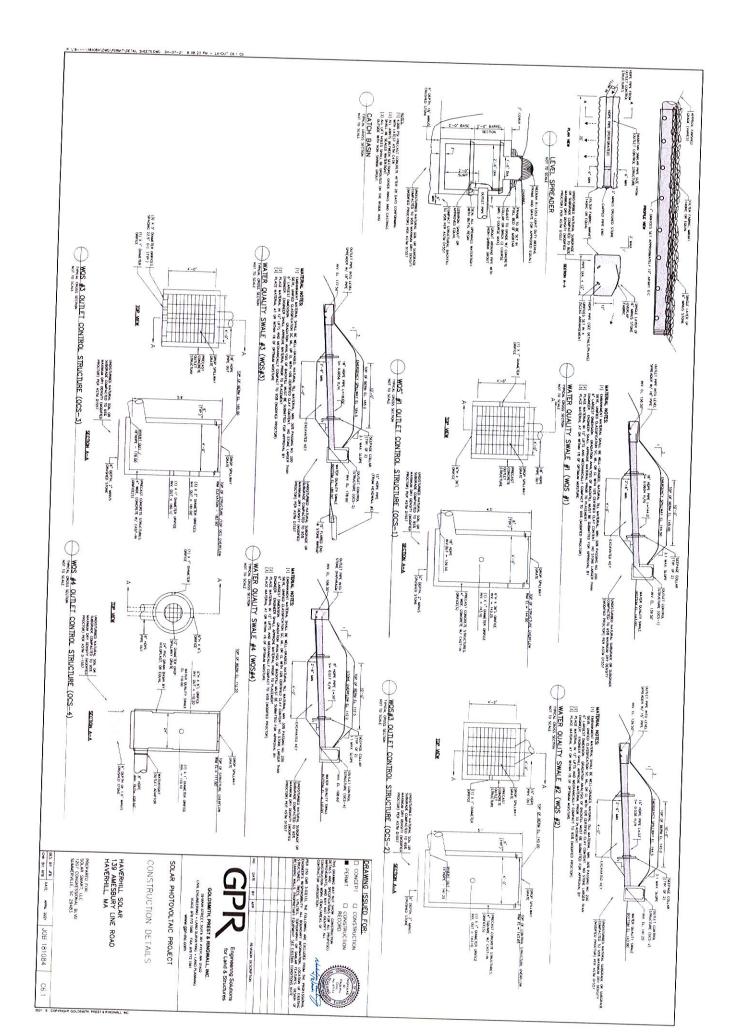


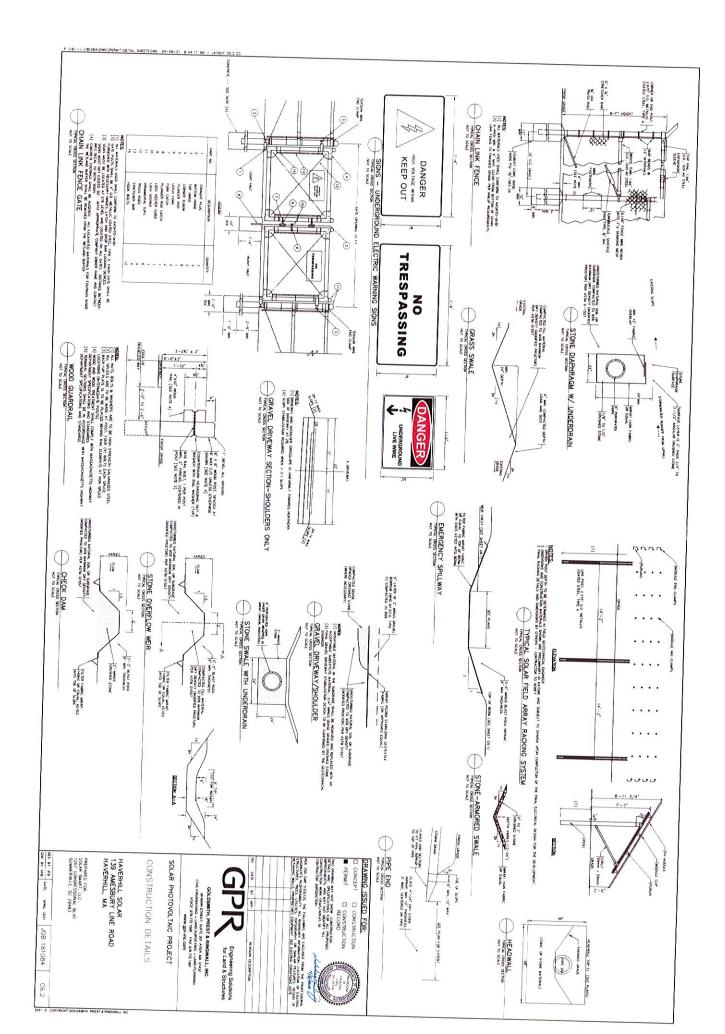












HAVERHILL SOLAR FARM 139 AMESBURY LINE ROAD

SOLAR SYSTEM COMPONENTS

- -CANADIAN SOLAR MODULES
- -DCE SOLAR RACKING
- -SAMSUNG LITHIUM ION BATTERIES
- -SUNGROW BATTERY HOUSING
- -ANSUL FM200 CLEAN FIRE SUPPRESSION



Andrew to Update



BiHiKu6 Mono

BIFACIAL MONO PERC

520 W ~ 540 W

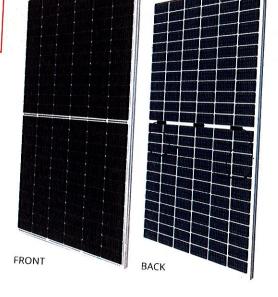
UP TO 30% MORE POWER FROM THE BACK SIDE

CS6W-520 | 525 | 530 | 535 | 540MB-AG

Dimensions: 2266 × 1135 × 35 mm (89.2 × 44.7 × 1.38 in)

Weight: 32.4 kg (71.4 lbs)

Max. System Voltage: 1500 V (IEC/UL) or 1000 V (IEC/UL)



MORE POWER



Module power up to 540 W Module efficiency up to 21.0 %



Up to 12.3 % lower LCOE Up to 5.2 % lower system cost



Comprehensive LID / LeTID mitigation technology, up to 50% lower degradation



Compatible with mainstream trackers, cost effective product for utility power plant



Better shading tolerance

MORE RELIABLE



Minimizes micro-crack impacts



Heavy snow load up to 5400 Pa, wind load up to 2400 Pa* 12 Years

Enhanced Product Warranty on Materials and Workmanship*



Linear Power Performance Warranty*

1st year power degradation no more than 2% Subsequent annual power degradation no more than 0.45%

*According to the applicable Canadian Solar Limited Warranty Statement.

MANAGEMENT SYSTEM CERTIFICATES*

ISO 9001:2015 / Quality management system ISO 14001:2015 / Standards for environmental management system OHSAS 18001:2007 / International standards for occupational health & safety

PRODUCT CERTIFICATES*

* As there are different certification requirements in different markets, please contact your local Canadian Solar sales representative for the specific certificates applicable to the products in the region in which the products are to be used

CANADIAN SOLAR INC. is committed to providing high quality solar products, solar system solutions and services to customers around the world. No. 1 module supplier for quality and performance/price ratio in IHS Module Customer Insight Survey. As a leading PV project developer and manufacturer of solar modules with over 43 GW deployed around the world since 2001

^{*} For detailed information, please refer to the Installation Manual



Elevating the Future for Solar Made in America

Contour™ DB-II

ASSEMBLY MANUAL



INSPECTION OPERATION AND MAINTENANCE PROCEDURE INSPECTIONS DURING THE SYSTEM WARRANTY PERIOD

SNOW REMOVAL

 Substantial snow accumulation that completely fills the gap between front of the panels and ground must be removed immediately to prevent excessive snow drift and ice dam formation. DCE Solar should be notified immediately of any structural issues and the issues should be documented with photos.

The following inspections should be performed at a minimum of every year of the warranty period.

CHECK CONNECTIONS

- Visually inspect all bolted connections and verify that connections have not visually loosened (torque marks should be inline). Also look for any instance of slippage or part movement.
- Check the torque on 10% of the bolted connections to 80% of the torque value given in the installation manual. If 10% of the of the inspected hardware does not meet the 80% torque value, perform a site-wide inspection and retorque all similar connections.
- If any of the connections require re-torqueing, reinspect in 6 and notify DCE Solar. DCE solar should be notified on any instances where such corrective action is required.

INSPECT FOUNDATIONS

- Check for ground erosion and settlement around the foundation of the system and correct any site issues where excessive erosion, standing water, or other factors that could inhibit foundation performance.
- Ground screw system; check the height of the inside tube connected to the N/S beam to ensure no vertical moved has occurred.

CORROSION

Perform a visual inspection for evidence of corrosion on all structural components. Excessive corrosion is defined

- Any instance where red rust covers more than 5% of the total surface area
- Any localized or pitting corrosion where the structural performance of a component may be impeded.

Note: It is common to observe white rust on galvanized components, this does not present any structural concern and requires no corrective action. It is common on pre-galvanized materials to observe red rust on cut edges or holes. This is typical and does not present any structural concern and requires no corrective action.

Any component where the structural integrity has been compromised must be replaced immediately. Where the integrity of structural components has not been impacted, the galvanized coating should be repaired in accordance

CONTACT

If any corrective action is required on a site, or if there are any questions or causes for concern from the site inspection, contact DCE Solar at 704 659-7477 or info@dcesolar.com.



SAMSUNG SDI

Battery Business Energy Storage System

Global Network

TAIWAN JAPAN CHINA USA KOREA (HQ) TEL +886-2-8178-5974 E-mail allen01.chen@samsung.com TEL +81-5-6369-6414 E-mail m.goto@samsung.com TEL +86-551-6532-7500 E-mail hgleo.ryu@samsung.com 7F-1, No. 399, Ruiguang Rd., Neihu Dist., Taipei City 114, Taiwar (108-0075) Shinagawa Grand Central Tower 9F, 2-16-4, Konan, Minato-ku, Tokyo, Japan No./88, Mingchuan Rd. Boyan Science & Technology Park Hefel State Hi-tech Zone, P.R. China 5655 North 1st Street, San Jose, CA 95154, USA TEL+1-408-544-4491 E-mail hk1.kim@samsung.com TEL +49-89-9292-7799(19) E-mail sintaek.yim@samsung.com Reichenbachstrasse 2, 85737 Ismaning, Germany TEL+82-31-210-8209 E-mail energy.storage@samsung.com 150-20 Gongse (O, Giheung-gu, Yongin-si, Gyeonggi-do 17084, Korea

www.samsungsdi.com

Feb. 2019

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Legal Notice and Disclaimer



ESS Batteries by Samsung SDI

Top Safety & Reliability Solutions

SAMSUNG SDI

SAMSUNG SDI

& Materials Solution Leader **Creative Energy**

Samsung SDI is leading the change of a new era with lithium-ion batteries.

we led with the technological superiority of our innovative IT devices In addition, we are contributing to the expansion of an eco-friendly and expanded into electric cars which have now become reality. environment by the deployment of batteries for energy storage. Through our constant innovation towards excellence,

Samsung SDI Battery Solution for Energy Storage

Powering Tomorrow,

Samsung SDI's technology supplies eco-friendly energy solutions for the present and the future.

ESS projects are deployed using Samsung SDI's battery solutions optimized for a range from residential to

We provide safe, reliable and long-lasting performance with our Energy Storage solutions.

We are all dreaming of a better future with BoT (Battey of Things) in which Samsung SDI will provide solutions for the world.

2000 Established Samsung SDI 1970

Expanded Business

into Energy Storage Expanded Business into Automotives

Utility & Commercial Battery Platform

Optimized Battery Platforms Based on High-Density Design Fechnology



B

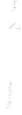
Proven High-Voltage LIB Solutions Compatible with Premium UPS



Residential & Telecom Barrente

Scalable Standard Battery Pack for Customized ESS







Why Samsung SDI

Samsung SDI optimizes battery systems with advanced cell technology.

Safety First

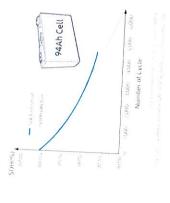


Multi-Layered **Protection** Safety first is Samsung SDI priority. Pr**ismatic cell has multi-layered protection at the cell level** resulting in best in class safety. In addition, the aluminum exterior has excellent thermal conductivity and cooling performance, and it releases high temperature safely and efficiently from the inside to

Long Cycle Life



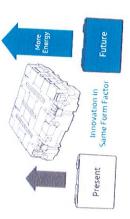
Samsung SDI ESS leverages our manufacturing experience in II and automotive battery cells resulting in superior and adaptive technology. Samsung SDI FSS is recognized as the industry leader in the market, providing our customers with the safest and long lasting batteries.



Sustainable Design

Easy to Upgrade Capacity without

Design Change



We are continuously innovating to increase the energy density while maintaining the same form factor and cell dimensions, thus facilitating future upgrades to higher capacity, higher energy density, ESS with no change to pack design.

Accurate Lifetime Simulation



Optimal Battery Solution Samsung SDI offers optimal battery solution with its superior lifetime prediction technology.
We design and propose a battery system with analyzing the various parameter such as purpose, operation period and installation environment.

Standard Platform

Energy Platform New































than 16% with upgrades to Samsung

SDI's new advanced module

Energy density has increased more











Operating Voltage

Dimension (W x D x H)

Cell Capacity







The Highest Lifetime Performance in

a Continuous Charge/Discharge

Optimized Solution for around One

hour of Grid Service

Unique Platform in the ESS Industry

+hour up to 45 minutes Medium Platform

with Mid-range Capabilities

1





P5 R0/6	×	9/	818 1,083	87.1.x.1.1/2	7.50
P4 R076	(9)		(50, 05)	458×7.1×7,12.5 458×7.11×2.78	
P.5 ×055.7	139		x - 4 0	854 1777 855	999
PS MU65	×		7.06-7.89	570 x 6530 x 160	24
	All	KWB	>	3000	6¥
Model	Cell Capacity	Energy	Operating Voltage	Dimension (W \times D \times H)	Weight

High Power Platform Optimized for

Less than 50 minutes of Use

30 minutes up to 20 minutes

Power Platform

Applications such as F/R, Railway,

Optimized Solution for Power

Utility & Commercial ESS Battery Platform for

Utility & Commercial ESS

Optimized Battery Platforms Based on High-Density Design Technology

Special Platform





Grid (Substation)

High Efficiency Battery Solution for 1,500V PCS

1,500 High Voltage Platform (New)































































































by Enabling High PowerOutput









Product Lineup



Backup Imre
Cell Capacity
Energy
Operating Voltage
Omension (W x D x H)
Vergitt

Americas

California 150MWh Deployed 2017~



ESS market, based on best in class battery technology and strong partnerships. Today, Samsung SDI continues to make history by leading the growing global

Since 2010, Samsung SDI's ESS products have been successfully

operating in over 30 countries.

Global Track Record

El Cajon/Escondido, CA 37.5MW / 150MWh Indianapolis, IN 20MW / 20MWh Punta Gorda, FL 10MW / 40MWh El Centro, CA 30MW / 20MWb Pomona, CA 20MW / 80MWh Austin, TX 36MW / 14MWh Tucson, AZ 10MW / SMWh

Canada

Sault Sainte Marie, Ontario 8MW / 8MWn

Europe

Schwerin 15MWh Deployed 2014/17-

Germany



Chemnitz 10MW / 10MMB Hassfurth 10MW / 10MWh Schwerin 15MW 15MWh

¥

Leighton Buzzard 10MWh Deployed 2014-



Barrow in Furness 49MW / 25MWh Leighton Buzzard 6MW 10MWh Port of Tyne SaMW / 28MWh Tynemouth 75MW / 17MWh Petham SOMW / SOMWh Broxburn 20MW / 22MWh

Italy

Potenza ZMW / ZMWH

Zeeland 10MW/ 10MWh Netherlands

Spain

Carboneras 20MW / 12MWh

Asia & Oceania

KEPCO F/R 38MWh Deployed 2015-

Korea



KEPCO(5 Sites) 128MW / 38MWn KOEN(3 Sites) 22MW / 63MWin PyeongChang 6MW / 18MWh Utsan 24MW / 51MWh

China



Tibet Shuanghu 414W / 14MWh Tibet Gaize 4MW / 14MWh

Japan

Hokkaido 25+MWht3 Sites) Deployed 2017~



Hokkaido Shinhidaka 17MW 2MWh Hokkaido Chitose 17MW / 14MWh

Australia

Western Australia AMW / 2MWn Alice Spring AMW / ZMWn Adelaide 30MW/35MWh

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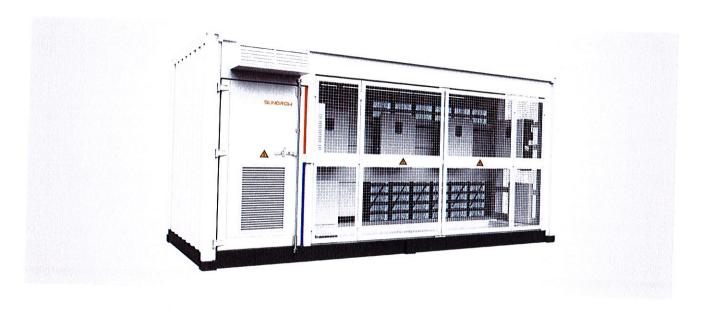
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ST548KWH-D250HV +4xSG125HV

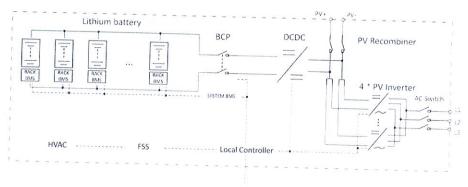
Storage System



SYSTEM FEATURES

- ESS system integrated with PV inverter
- 1500V DC coupled PV+ESS system
- Compact mechanical design,minimized footprint
- High efficient system with safe and long lifecycle lithiun-ion battery
- Integrated local controller, HVAC and FSS to enable unified communication and ensure system safety

CIRCUIT DIAGRAM



System Type	ST548KWH-D250HV+4xSG125HV
PV Data	
Max PV input voltage	1.500 v
MPPT voltage range at nominal power	860 - 1.250 V
Number of DC Inputs	3
Max. PV input current	1.250 4
DCDC Data	
Working voltage range	500 ~ 1,500 V
Nominal power	250 KW
Max current	344 A
Battery Data	
Cell type	Samsung SDI Mega E2, 3,68 V / 94 Ah
Configuration of system	264S6P
Battery capacity (BOL)	548 kWh
Battery voltage range	844 -1,095 V
AC Data	
AC output power	500kVA @ 50 °C
Max, AC output surrent	480 A
Nominal AC voltage	3 / PE. 600 V
AC voltage range	480 × 690 V
Nominal grid frequency / Orio frequency range	60 Hz 55 × 65 Hz
Power factor at nominal power / Adjustable power factor	> 0.99 / 0.8 leading - 0.8 lagging
Feed-in phases / connection phases	3/3
General Data	
Dimensions (W * H * D)	6,058 * 2,896 * 2,438 mm / 238 S * 114.0 * 96.0
Weight (with , without pattery)	12.5 f / 8.6 f 27.558 lbs / 18.960 lbs
Degree of protection	IP 54 / NEMA 3R
Operating temperature range	-30 to 50 °C / -22 to 122 °E
Relative humidity	0 ~ 95 % (non-condensing)
Max. working altitude	2,000 m (6,562 ft
Sooting concept of battery chamber	Heating, ventilation and Air Conditioning
Fire suppression system of battery unit	FM4200 extinguishment system
Sommur idation interfaces	RS485, Ethernet
Communication protocols	Modbus RTU Modbus ICP
Som pilance	o L95 40







Power Generation

CHALLENGE:

Protecting sub-stations, electrical switch rooms, control rooms, data communications and other critical areas

SOLUTION:

ANSUL_® FM-200[™] Clean Agent Fire Suppression System

APPLICATION:

Protecting critical operational infrastructure in cramped conditions

Power stations and power generation facilities incorporate a wide range of critical and ancillary services and buildings to ensure continued operations and plant uptime. Away from the primary power circuit, boiler and turbine system; vital facilities such as sub-stations, cable voids, control rooms, data communications and backup systems must be effectively protected against fire risk. Selecting the right solution to protect this critical plant infrastructure is key.

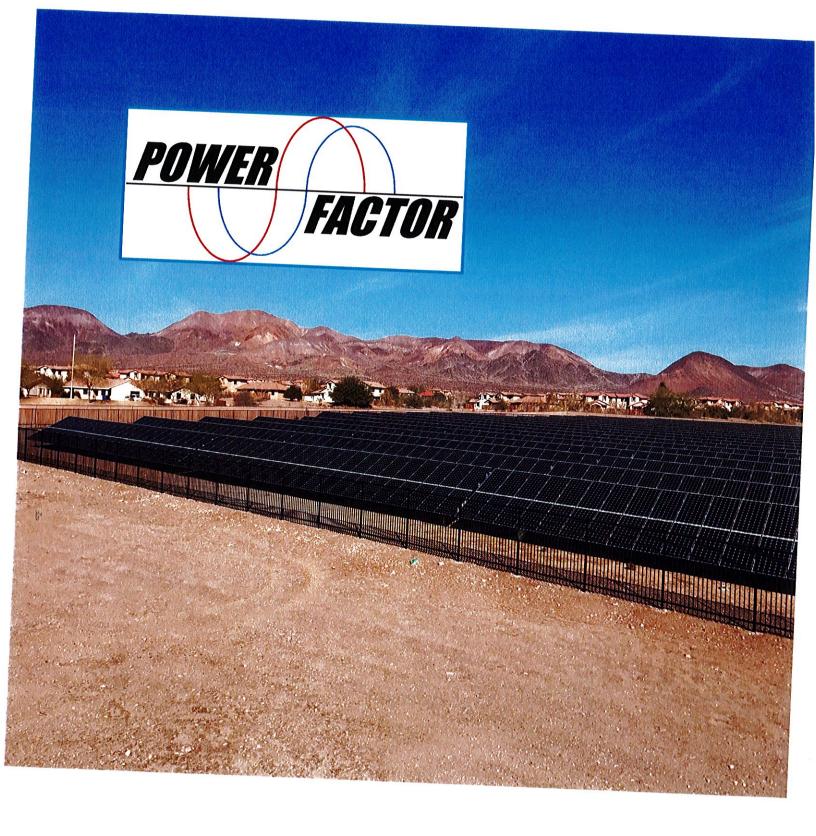
The ANSUL FM-200 Clean Agent Fire Suppression System has zero ozone depletion potential (ODP). The system uses FM-200 (HFC-227ea) fire extinguishant which vaporizes upon discharge and absorbs heat to rapidly suppress fire. This results in less damage to critical equipment, facilitating a much shorter recovery time and reducing downtime. Safe for use in occupied areas at the design concentration, the system helps protect critical infrastructure and delivers effective asset protection for power generation facilities.

The ANSUL FM-200 system is most effective when used with the automatic AUTOPULSE Detection and Control System to introduce the clean agent rapidly. This detection system is used to actuate a single, fixed fire suppression or alarm system based on inputs received from fire detection devices. The detection circuits can be configured using cross, counting, independent or priority-zone concepts.

Both automatic and manual actuators are available for release of the agent into the hazard area through fixed piping and nozzles. Seven nozzle sizes are available to provide the correct flow of agent in either 180 or 360 horizontal discharge patterns. For large hazards, cylinders can be connected to a common manifold.

The ANSUL FM-200 system carries UL, FM and ULC, as well as marine approvals. The system can be designed to meet the requirements of EN 15004, ISO 14520 and NFPA 2001 with components approved to provide the highest quality fire suppression system.





O&M PROPOSAL

George Lang IV

O&M Proposal



Part 1: Bidder Contact Information

Bidder Contact Info Corporate Name: P		
Corporate Address	240 Beachwood road, Dundalk MD 21222	
	240 Beachwood road, Dundalk MD 21222	
Parent's Corporate	ame: Power Factor LLC	
Parent's Corporate	ldress: 8240 Beachwood road, Dundalk MD 21222	
	aress. 6240 Beachwood road, Dundalk MD 21222	
Legally Authorized F	presentative	
Name: George Lang		
Title: Managing Dire	or	
Phone: (443) 827 754		
ax:		
-mail: george@pow	factorco.com	
ignature:		
rimary Contact:		
imary Contact:		
ame: Andrew Streit		
tle: Director of Busin	SS Develonment	
none: (803) 665-6688		
x:		
mail: andrew@powe	actorco com	
gnature:		

Part 2: Executive Summary

Power Factor is honored to submit our qualifications for solar photovoltaic operations and maintenance services to Amesbury Line Solar LLC. Our company is ideally situated to deliver professionalism, excellence, efficiency and durability to Amesbury Line Solar in its efforts to successfully deploy solar projects on its properties. Due to a decade of involvement in developing customized renewable energy projects for public and private clients, Power Factor has an intimate understanding of the energy market in the southeastern United States. Our previous work with public entities has demonstrated that an elevated level of execution and delivery are the minimum standard for every government contract. We

- Power Factor brings with it an experienced team of solar professionals that have successfully completed a large portfolio of projects ranging from rooftop solar arrays to solar parking canopies to utility scale solar farms.
- Power Factor has successfully deployed solar systems for a number of public entities, including various military and municipal installations.
- Power Factor has worked hand-in-hand with utilities, electric cooperatives, regulators, and private and public-sector entities to find economic, clean energy solutions that satisfy the aesthetic and sustainability goals of the client.
- Power Factor has amassed the professional capacity to manage projects on time and on budget even in the midst of challenging circumstances.
- Power Factor's reputation and history of successful solar project management should provide Amesbury Line Solar with the confidence it needs when selecting an experienced, knowledgeable operations and maintenance firm for this project.

Sustainability is not a catch phrase. It is the foundation of successful organizations. Power Factor recognizes that inventing and deploying the nation's utility grid was the single most important investment of the 20th century. Improving efficiency and eliminating waste will be primary drivers for the public and private sectors during the years to come. Given Power Factor's expertise and passion for the advancement of solar as a mainstream component of our country's energy portfolio, we are well prepared to lead in the realization and execution of these maintenance agreements. We are confident that our services will bring with them maximum value to Amesbury Line Solar and will result in a durable sustainability commitment. Power Factor is genuinely excited about our potential role in this process. We are proposing to provide all the preventative and corrective maintenance options requested, as well as providing training of any interested on-site personnel.



O&M Proposal

Preventive Maintenance Requirements and Costs

List of services:

Standard

Preventative Maintenance Work Scope	
Array Balance System	Yes/No
Array visual inspection-wire management, connector tightness, and insulation inspection	Ye
Array ground/racking debris removal and vegetation inspection	Ye
Verify fence condition and grounding	Ye
Inspect system and site drainage	Ye
Module Visual Inspection	Yes/No
Inspect 100% of glass side for cleanliness and obvious defects	Ye
Inspect 100% of back-sheet a J-Boxes	Yes
Inspect 100% of module clamps for looseness	Yes
String Inverters (Central Inverters vary by Size/Band)	Yes/No
Inspect for corrosion, labelling and basic condition of housing	Yes
Verify functionality of display and operation of PV system	Yes
Inspect base of inverter and conduit entry points	Yes
Clean inverter interior and inspect for moisture intrusion	Yes
Check string fuse functionality	Yes
Check ground straps and ensure all grounds are intact and tight to the enclosure	Yes
Clean heat sink and filters (replace filters if necessary)	Yes
Torque AC and DC conductors connections to manufacturers specs	Yes
IR scan all string terminations	Yes
AC/DC Disconnections & Panel Boards	Yes/No
Cycle all movable parts in AC/DC disconnect & Panel Boards	Yes
Torque all conductor connections to manufacturers specs	Yes
IR scan all string terminations	
DAS & MET Stations	Yes/No
nspect cabinet for labelling, corrosion, moisture intrusion and basic conditions of housing	Yes
Ensure all conductors and wires are routed in a neat and clean manner	Yes
orque data terminations to manufacturers specs	
Clean reference cell and/or pyranometer (Replace desiccant)	Yes
/erify functionality of all DAS Components	Yes
Other Services (Please list below)	Yes/No

Corrective Maintenance Requirements and Costs

Corrective Maintenance (CM) Services are generally triggered by a monitoring alert reporting an issue at the site. Certain alerts can be corrected remotely, while more severe alerts can require an emergency response due to safety concerns, or (far more typically) permit the on-site service call to be scheduled.

Please indicate which services your company provides and the respective costs associated with typical corrective maintenance service visit in the O&M bid below. The preferred cost structure can be in terms of Hourly, Half Day, or Full Day Rate.

Standard

Corrective Maintenance Work Scope	
Common Corrective Maintenance Task	Yes/No
Inverter troubleshooting and warranty management	Ye
String and Connector repairs	Ye
Panel Replacements	Ye
Panel manufacturer defect identification and tracking	Ye
Monitoring troubleshooting and repair	Ye:
Fuse replacements	
Breaker tightening and replacement	Ye:
Transformer Oil Sampling	Yes
Ground fault identification	Yes
System wide IV Curve testing	Yes
Aerial or customized IR thermal imaging	Yes
Power Quality Analysis	Yes
Additional Services May Include	Yes
Auditing/correcting sites installed by others	Yes/No
Commissioning of sites installed by others	Yes
Medium Voltage and Fiber Optic Services	Yes
Other Services (Diagonal Land Land Land Land Land Land Land Land	Yes
Other Services (Please list below)	Yes/No

Cost Structure for Above	Indicated Services (Fill in all that apply)
nourly kate	\$75/hr
Half Day Rate Full Day Rate	\$250
Tan Day Nate	\$500



O&M Proposal

	Service Levels and Rates	
Service	Description	Rate
	Electrical fault repair, upgrades and modifications, field	
Medium Voltage	engineering, transformer testing, underground fault	
Electrician	location, site management	\$100/hr
	Electrical fault repair, upgrades and modifications, field	
	engineering, transformer testing, underground fault	
Master Electrician	location, site management	\$75/hr
Level 3 Datacom	Advanced Datacom troubleshooting, fiber repair, level 1 and	
Electrician	2 capable	\$50/hr
	Inverter and Datacom second level troubleshooting, panel	
	testing, fuse and cable replacement. Captures IV Curves, IR	
Level 2 Technician	Images and Power Quality measurements. OEM repairs	\$36/hr
	Inverter and Datacom resets. Primary troubleshooting,	
	records site data and fault codes. Replaces solar panels, was	
	panels, and completes basic electrical and mechanical	
Level 1 Technician	repairs	\$25/hr
	Performance engineering, integration services, system	
Professional	designs, commissioning review, project management and	
Services	services oversight	\$47/hr
Travel Charges	For teams of 2: Labor + Mileage	
Per Diem	For teams of 2: Overnight Accommodations	\$250
Overtime	Workdays exceeding 8 hours	
Emergency		
Response	Deploy within 4 hours of notification	
	Specialized Site Services	
Service	Description	Rate
Transformer	Sample of transformer fluid for DGA, refill nitrogen, includes	
Service	all labor, laboratory and material costs	
	Underground Fault Location (UFL), Infra-Red Imaging	
	Diagnostics (IR Imaging), Module and String level I-V	
	Characterization (IV Curves), DC/AC Power Quality Analysis	
Technical Services	(PQA)	
	Other Services (Please list below)	
Service	Description	Rate

Onsite training for Amesbury Line Solar

Power Factor is happy to offer Amesbury Line Solar training services.

Training Services and Rates		
Training	Description	Rate
1-Day Training	Training to be held for Points of Contacts at a location provided by AMESBURY LINE SOLAR	\$25/hr
Customize in-class training	Half Day training(s) on specific topics of need for AMESBURY LINE SOLAR	\$50/hr
Field Shadowing	On-site, hands-on training	\$25/hr
Not Applicable	Our company does not provide specific training	

Credibility

References:

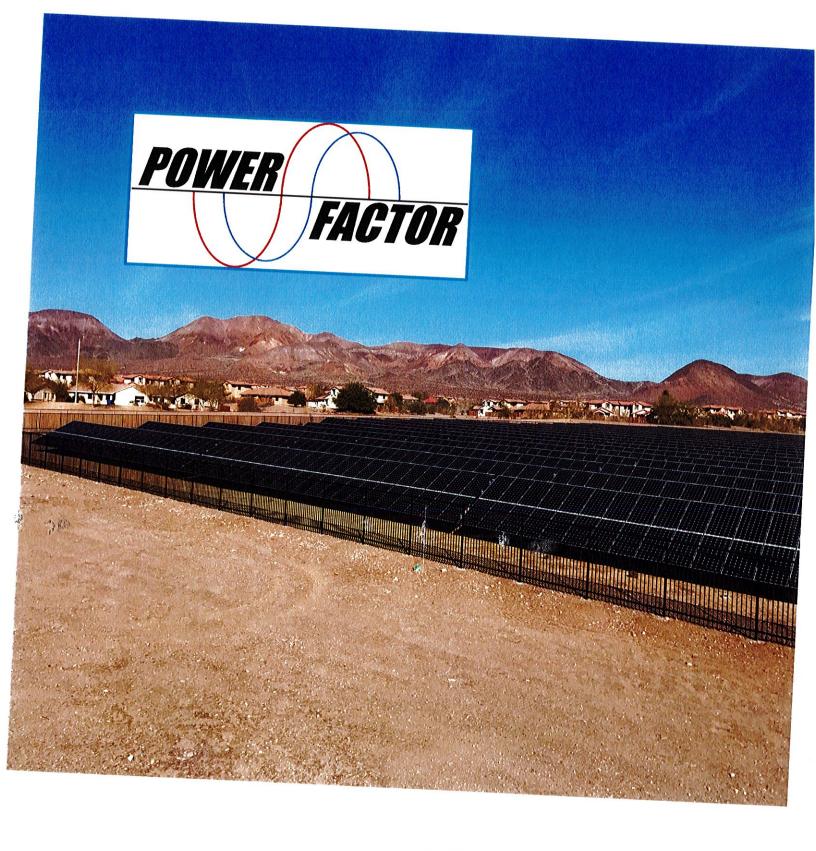
- Maryland Management Christopher Dimario
 Rental Property Owner/Manager
 Cdimario@Marylandmgmt.com
- URI (Unlimited Restoration Inc) Rodney O'Neal Co-Owner
 ROneal@urinow.com
- Onyx renewable Partners Greg Cousoulas
 Sr VP of Construction
 On file
- Uhaul
 Jim Dickerson
 Owner Representative
 jim dickerson@uhaul.com

Planning Board Decision not required for Application.

Approved Site Plan not required for Application.

No Zoning Waivers required.

Applicant is seeking Two Special permits Only



O&M PROPOSAL

George Lang IV

O&M Proposal



Part 1: Bidder Contact Information

Corporate Name	
Corporate Name: Power Factor, LLC	C
Corporate Address: 8240 Beachwoo	od road, Dundalk MD 21222
Parent's Corporate Name: Power Fa	actor LLC
Parent's Corporate Address: 8240 Be	eachwood road, Dundalk MD 21222
Legally Authorized Representative	
Name: George Lang	
Title: Managing Director	
Phone: (443) 827 7543	
ax:	
-mail: george@powerfactorco.com	
ignature:	
	₹ 76
rimary Contact:	
ame: Andrew Streit	
tle: Director of Business Developmer	nt.
none: (803) 665-6688	TIC
1X:	
mail: andrew@powerfactorco.com	
gnature:	

Part 2: Executive Summary

Power Factor is honored to submit our qualifications for solar photovoltaic operations and maintenance services to Amesbury Line Solar LLC. Our company is ideally situated to deliver professionalism, excellence, efficiency and durability to Amesbury Line Solar in its efforts to successfully deploy solar projects on its properties. Due to a decade of involvement in developing customized renewable energy projects for public and private clients, Power Factor has an intimate understanding of the energy market in the southeastern United States. Our previous work with public entities has demonstrated that an elevated level of execution and delivery are the minimum standard for every government contract. We are prepared to meet and exceed those standards.

- Power Factor brings with it an experienced team of solar professionals that have successfully completed a large portfolio of projects ranging from rooftop solar arrays to solar parking canopies to utility scale solar farms.
- Power Factor has successfully deployed solar systems for a number of public entities, including various military and municipal installations.
- Power Factor has worked hand-in-hand with utilities, electric cooperatives, regulators, and private and public-sector entities to find economic, clean energy solutions that satisfy the aesthetic and sustainability goals of the client.
- Power Factor has amassed the professional capacity to manage projects on time and on budget even in the midst of challenging circumstances.
- Power Factor's reputation and history of successful solar project management should provide Amesbury Line Solar with the confidence it needs when selecting an experienced, knowledgeable operations and maintenance firm for this project.

Sustainability is not a catch phrase. It is the foundation of successful organizations. Power Factor recognizes that inventing and deploying the nation's utility grid was the single most important investment of the 20th century. Improving efficiency and eliminating waste will be primary drivers for the public and private sectors during the years to come. Given Power Factor's expertise and passion for the advancement of solar as a mainstream component of our country's energy portfolio, we are well prepared to lead in the realization and execution of these maintenance agreements. We are confident that our services will bring with them maximum value to Amesbury Line Solar and will result in a durable sustainability commitment. Power Factor is genuinely excited about our potential role in this process. We are proposing to provide all the preventative and corrective maintenance options requested, as well as providing training of any interested on-site personnel.

O&M Proposal



Preventive Maintenance Requirements and Costs

List of services:

Standard

Preventative Maintenance Work Scope	
Array Balance System	V (a)
Array visual inspection-wire management, connector tightness, and insulation inspection	Yes/No
Array ground/racking debris removal and vegetation inspection	
Verify fence condition and grounding	Ye
Inspect system and site drainage	Ye
Module Visual Inspection	Ye
Inspect 100% of glass side for cleanliness and obvious defects	Yes/No
Inspect 100% of back-sheet a J-Boxes	Ye.
Inspect 100% of module clamps for looseness	Ye:
String Inverters (Central Inverters vary by Size/Band)	Yes
Inspect for corrosion, labelling and basic condition of housing	Yes/No
Verify functionality of display and operation of PV system	Yes
Inspect base of inverter and conduit entry points	Yes
Clean inverter interior and inspect for moisture intrusion	Yes
Check string fuse functionality	Yes
Check ground straps and ensure all grounds are intact and tight to the enclosure	Yes
Clean heat sink and filters (replace filters if necessary)	Yes
Torque AC and DC conductors connections to manufacturers specs	Yes
IR scan all string terminations	Yes
AC/DC Disconnections & Panel Boards	Yes
Cycle all movable parts in AC/DC disconnect & Panel Boards	Yes/No
Forque all conductor connections to manufacturers specs	Yes
R scan all string terminations	Yes
DAS & MET Stations	Yes
nspect cabinet for labelling, corrosion, moisture intrusion and basic onditions of housing	Yes/No
insure all conductors and wires are routed in a neat and clean manner	Yes
orque data terminations to manufacturers specs	Yes
lean reference cell and/or pyranometer (Replace desiccant)	Yes
erify functionality of all DAS Components	Yes
Other Services (Please list below)	Yes
and delivers (Liease list below)	Yes/No

Corrective Maintenance Requirements and Costs

Corrective Maintenance (CM) Services are generally triggered by a monitoring alert reporting an issue at the site. Certain alerts can be corrected remotely, while more severe alerts can require an emergency response due to safety concerns, or (far more typically) permit the on-site service call to be scheduled.

Please indicate which services your company provides and the respective costs associated with typical corrective maintenance service visit in the O&M bid below. The preferred cost structure can be in terms of Hourly, Half Day, or Full Day Rate.

Standard

Corrective Maintenance Work Scope	, <u></u>
Common Corrective Maintenance Task	Yes/No
Inverter troubleshooting and warranty management	Y
String and Connector repairs	Ye
Panel Replacements	Ye
Panel manufacturer defect identification and tracking	
Monitoring troubleshooting and repair	Ye
Fuse replacements	Ye
Breaker tightening and replacement	Ye
Transformer Oil Sampling	Ye
Ground fault identification	Ye
System wide IV Curve testing	Ye:
Aerial or customized IR thermal imaging	Yes
Power Quality Analysis	Yes
Additional Services May Include	Yes
Auditing/correcting sites installed by others	Yes/No
Commissioning of sites installed by others	Yes
Commissioning of sites installed by others	Yes
Medium Voltage and Fiber Optic Services	Yes
Other Services (Please list below)	Yes/No
	7.00/110

Cost Structure for Above	e Indicated Services (Fill in all that apply)
riodity Nate	\$75/hr
Half Day Rate Full Day Rate	\$250
ruii Day Nate	\$500



O&M Proposal

Service	Service Levels and Rates	
	Description Flectrical faults	Rate
Medium Voltage Electrician	location, site management	
Master Electrician Level 3 Datacom	engineering, transferred and modifications, field	\$100/hr \$75/hr
Electrician	2 capable Inverter and Datacom second level troubleshooting, panel testing, fuse and cable replace.	\$50/hr
Level 2 Technician	Images and Power Quality measurements. OEM repairs Inverter and Datacom resets. Primary to a label of the primary to a lab	\$36/hr
Level 1 Technician	panels, and completes basic electrical and mechanical	\$25/hr
Professional Services	Performance engineering, integration services, system designs, commissioning review, project management and services oversight	
Travel Charges	For teams of 2: Labor + Mileage	\$47/hr
Per Diem	For teams of 2: Overnight Accommodations	
Overtime	Workdays exceeding 8 hours	\$250
Emergency Response	Deploy within 4 hours of notification	
	Specialized Site Services	
Service	Description	
Transformer Service	Sample of transformer fluid for DGA, refill nitrogen, includes all labor, laboratory and material cost	Rate
echnical Services	Diagnostics (IR Imaging), Module and String level I-V Characterization (IV Curves), DC/AC Power Quality Analysis (PQA)	
Service	Other Services (Please list below)	
Service	Description	Rate

Onsite training for Amesbury Line Solar

Power Factor is happy to offer Amesbury Line Solar training services.

Training	Training Services and Rates	
1-Day Training	Training to be held for Points of Contacts at a least	Rate
Customize in-class training	Half Day training(s) on specific topics of need for AMESBURY	\$25/hr
Field Shadowing	LINE SOLAR	\$50/hr
Not Applicable	On-site, hands-on training Our company does not provide specific training	\$25/hr

Credibility

References:

- Maryland Management Christopher Dimario
 Rental Property Owner/Manager
 Cdimario@Marylandmgmt.com
- URI (Unlimited Restoration Inc) Rodney O'Neal Co-Owner
 ROneal@urinow.com
- Onyx renewable Partners Greg Cousoulas Sr VP of Construction On file
- Uhaul
 Jim Dickerson
 Owner Representative
 <u>jim_dickerson@uhaul.com</u>

Temporary construction access easement agreement

This temporary construction access easement agreement is entered into this 24 day of march 2021 by Albert Duchemin and Jual Realty Trust whose legal address is 235 Amesbury Line Rd Haverhill, Mass.

Collectively the Grantor, And Michael Harrington of Harrington Excavating of 358 Grafton st.

Shrewsbury, Mass .as grantee

In consideration of the easement grantee agree's to repair and grade Mr Duchemin driveway and remove the tree,s he requested.

also agreed because of the temporary construction easement when site is running albert Duchemin would get a ___%credit on his power bill for the next years.

The Temporary Construction easement is granted to grantee' and is for vehicle's and pedestrian and ingress and egress to do all things reasonably necessary to construct and install the project including transporting, stockpiling, storage materials, equipment and vehicles.

The grantee, at its sole cost and expence, shall restore temporary easement to its original condition.

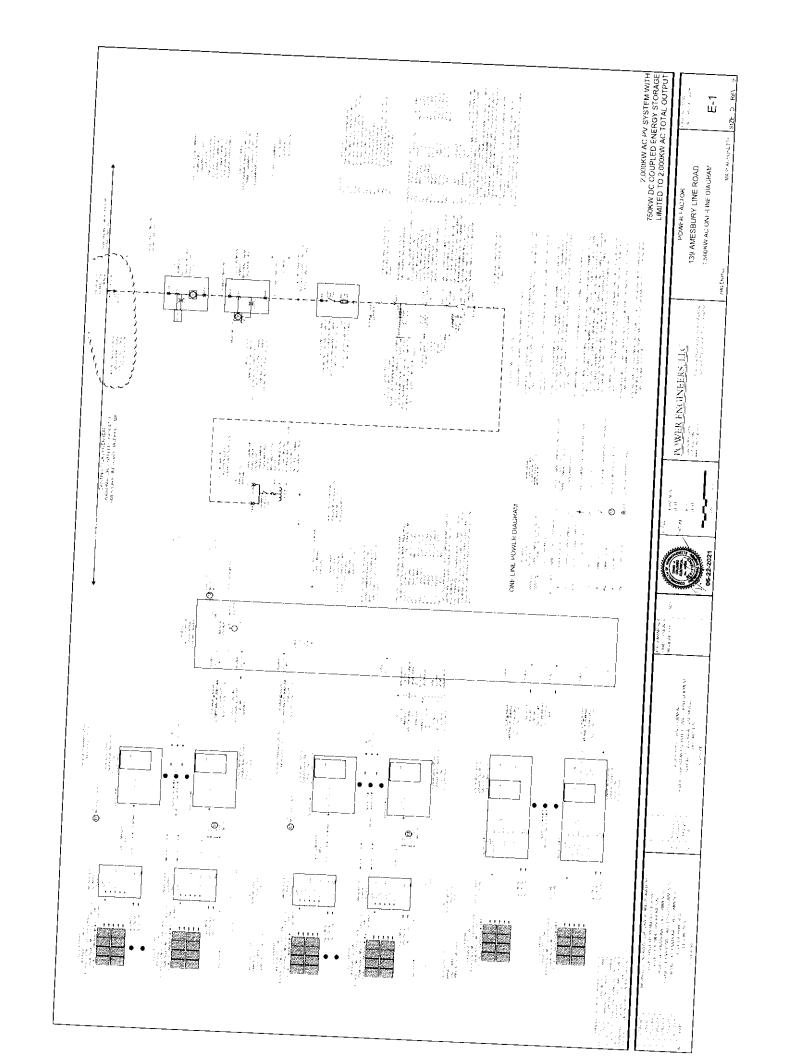
The easement also allows the town inspectors and consultants access till the completion of project.

Albert Duchemin and Jual Realty trust

allet Hackemin

Michael Harrington Harrington Excavating

Michael Harringh





ILLUSTRATIVE VIEW FROM WEST EDUCATION PLATFORM

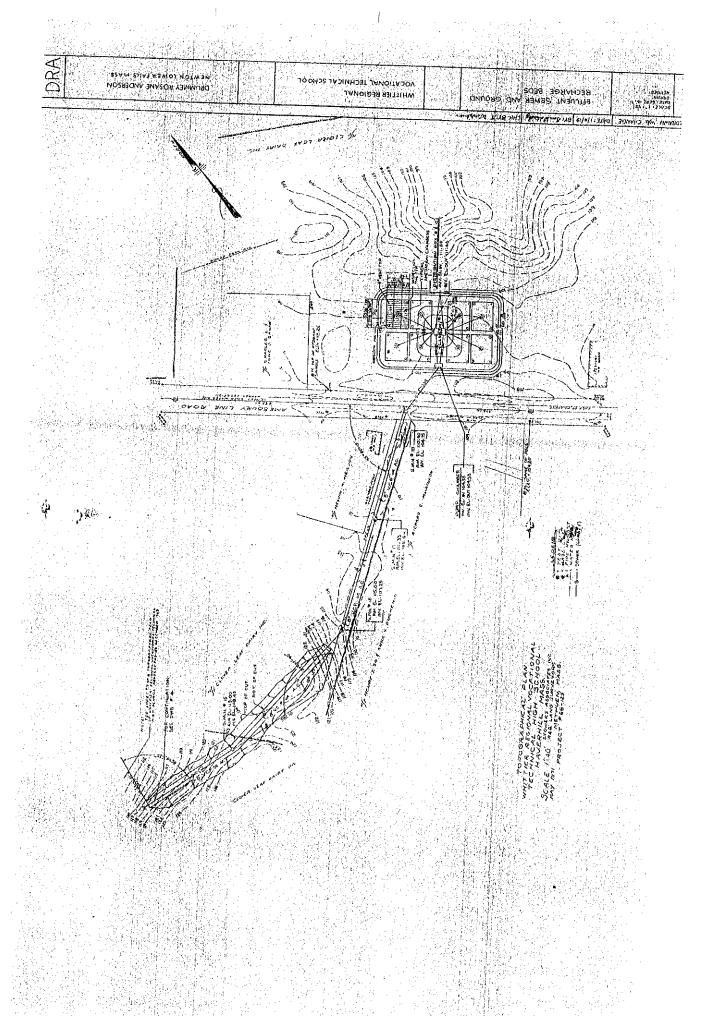


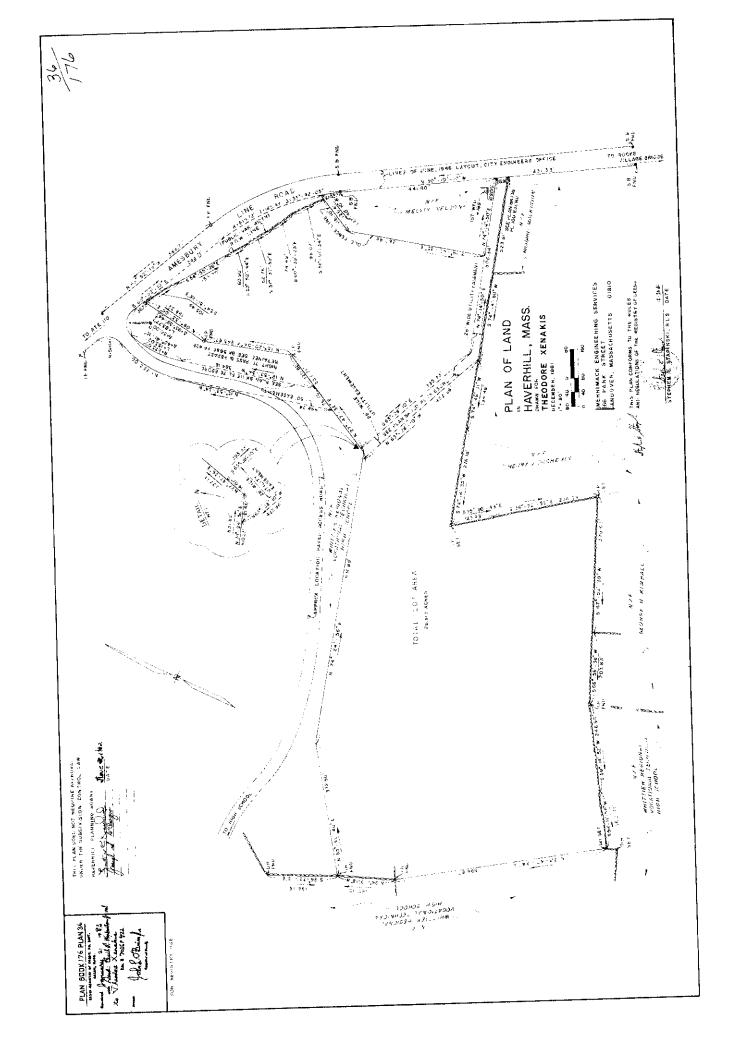
ILLUSTRATIVE VIEW FROM EAST EDUCATION PLATFORM



ILLUSTRATIVE VIEW ENTERING MAIN GATE

CONTROLL
 CONTROLL





HAVERHILL SOLAR FARM 139 AMESBURY LINE ROAD

SOLAR SYSTEM COMPONENTS (AMENDED 8/16/2021)

- -CANADIAN SOLAR MODULES
- -DCE SOLAR RACKING
- -SAMSUNG LITHIUM ION BATTERIES
- -SUNGROW BATTERY HOUSING
- -ANSUL FM200 CLEAN FIRE SUPPRESSION
- -ENVIROTEMP DIELECTRIC COOLANT
- -FIRE LANE CART PATH TREATMENT



Andrew to Update



BiHiKu6 Mono

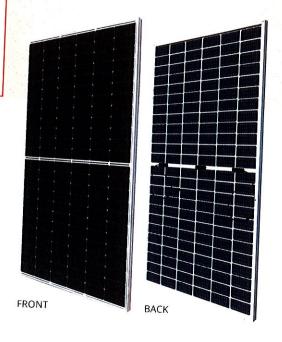
BIFACIAL MONO PERC
520 W ~ 540 W

UP TO 30% MORE POWER FROM THE BACK SIDE CS6W-520 | 525 | 530 | 535 | 540MB-AG

Dimensions: 2266 × 1135 × 35 mm (89.2 × 44.7 × 1.38 in)

Weight: 32.4 kg (71.4 lbs)

Max. System Voltage: 1500 V (IEC/UL) or 1000 V (IEC/UL)



MORE POWER



Module power up to 540 W Module efficiency up to 21.0 %



Up to 12.3 % lower LCOE Up to 5.2 % lower system cost



Comprehensive LID / LeTID mitigation technology, up to 50% lower degradation



Compatible with mainstream trackers, cost effective product for utility power plant



Better shading tolerance

MORE RELIABLE



Minimizes micro-crack impacts



Heavy snow load up to 5400 Pa, wind load up to 2400 Pa*

12 Years

Enhanced Product Warranty on Materials and Workmanship*



Linear Power Performance Warranty*

1st year power degradation no more than 2% Subsequent annual power degradation no more than 0.45%

*According to the applicable Canadian Solar Limited Warranty Statement.

MANAGEMENT SYSTEM CERTIFICATES*

ISO 9001:2015 / Quality management system ISO 14001:2015 / Standards for environmental management system OHSAS 18001:2007 / International standards for occupational health & safety

PRODUCT CERTIFICATES*

* As there are different certification requirements in different markets, please contact your local Canadian Solar sales representative for the specific certificates applicable to the products in the region in which the products are to be used.

CANADIAN SOLAR INC. is committed to providing high quality solar products, solar system solutions and services to customers around the world. No. 1 module supplier for quality and performance/price ratio in IHS Module Customer Insight Survey. As a leading PV project developer and manufacturer of solar modules with over 43 GW deployed around the world since 2001.

^{*} For detailed information, please refer to the Installation Manual.





Contour™ DB-II

ASSEMBLY MANUAL



INSPECTION OPERATION AND MAINTENANCE PROCEDURE INSPECTIONS DURING THE SYSTEM WARRANTY PERIOD

SNOW REMOVAL

Substantial snow accumulation that completely fills the gap between front of the panels and ground must be removed immediately to prevent excessive snow drift and ice dam formation. DCE Solar should be notified immediately of any structural issues and the issues should be documented with photos.

The following inspections should be performed at a minimum of every year of the warranty period.

CHECK CONNECTIONS

- Visually inspect all bolted connections and verify that connections have not visually loosened (torque marks should be inline). Also look for any instance of slippage or part movement.
- Check the torque on 10% of the bolted connections to 80% of the torque value given in the installation manual. If 10% of the of the inspected hardware does not meet the 80% torque value, perform a site-wide inspection and retorque all similar connections.
- If any of the connections require re-torqueing, reinspect in 6 and notify DCE Solar. DCE solar should be notified on any instances where such corrective action is required.

INSPECT FOUNDATIONS

- Check for ground erosion and settlement around the foundation of the system and correct any site issues where excessive erosion, standing water, or other factors that could inhibit foundation performance.
- Ground screw system; check the height of the inside tube connected to the N/S beam to ensure no vertical CORROSION

Perform a visual inspection for evidence of corrosion on all structural components. Excessive corrosion is defined

- Any instance where red rust covers more than 5% of the total surface area
- Any localized or pitting corrosion where the structural performance of a component may be impeded.

Note: It is common to observe white rust on galvanized components, this does not present any structural concern and requires no corrective action. It is common on pre-galvanized materials to observe red rust on cut edges or holes. This is typical and does not present any structural concern and requires no corrective action.

Any component where the structural integrity has been compromised must be replaced immediately. Where the integrity of structural components has not been impacted, the galvanized coating should be repaired in accordance

CONTACT

If any corrective action is required on a site, or if there are any questions or causes for concern from the site inspection, contact DCE Solar at 704 659-7477 or info@dcesolar.com.



SAMSUNG SDI

Energy Storage System Battery Business

Global Network

No./88, Mingchuan Rd. Boyan Science & Technology Park.Hefei State Hi-tech Zone P.R.China. (108-00/5) Shinagawa Grand Central Tower 9F, 2-16-4, Konan, Minato-ku, Tokyo, Japan 150-20 Gongse-ro, Giheung-gu, Yongin-si, Gyeonggi-do 17084, Korea 7F-1, No.599, Rurguang Rd., Neihu Dist., Taiper City 114, Taiwan TEL +886-2-81/8-5974 E-mail alten01.chen@samsung.com TEL +82-31-210-8209 E-mail energy.storage@samsung.com TEL +49-89-9292-7799(19) E-mail sintaek.yim@samsung.com TEL +86-551-6532-7500 E-mail hgteo.ryu@samsung.com TEL +81-3-6369-6414 E-mail m.goto@samsung.com TEL +1-408-544-4491 E-mail hk1.kim@samsung.com Reichenbachstrasse 2, 85737 Ismaning, Germany 5655 North 1st Street, San Jose, CA 95134, USA KOREA(HQ) GERMANY TAIWAN CHINA JAPAN USA

www.samsungsdi.com

Feb. 2019

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SAMSUNG SDI

& Materials Solution Leader **Creative Energy**

Samsung SDI is leading the change of a new era with lithium-ion batteries. we led with the technological superiority of our innovative IT devices In addition, we are contributing to the expansion of an eco-friendly and expanded into electric cars which have now become reality. Through our constant innovation towards excellence,

environment by the deployment of batteries for energy storage.

Samsung SDI Battery Solution for Energy Storage

Powering Tomorrow,

Samsung SDI's technology supplies eco-friendly energy solutions for the present and the future.

We provide safe, reliable and long-lasting performance with our Energy Storage solutions.

ESS projects are deployed using Samsung SDI's battery solutions optimized for a range from residential to

We are all dreaming of a better future with BoT (Battery of Things) in which Samsung SDI will provide solutions for the world.

Expanded Business into Automotives Began Lithium-ion Battery Business Samsung SDI Established 1970 -





Utility & Commercial Battery Platform

Optimized Battery Platforms Based on High-Density Design Technology



S

UPS Lithium ion Solution

Proven High-Voltage LIB Solutions Compatible with Premium UPS



Residential & Telecom Belley Box

Scalable Standard Battery Pack for Customized ESS





Why Samsung SDI

Samsung SDI optimizes battery systems with advanced cell technology.

Safety First





Safety first is Samsung SDI priority. Prismatic cell has multi-layered protection at the cell level resulting in best in class safety. In addition, the aluminum exterior has excellent thermal conductivity and cooling performance, and it releases high temperature safety and efficiently from the inside to the outside.

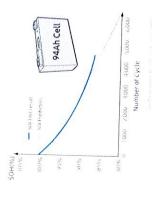
Long Cycle Life

Mustry'i eading Cycle i in Performsin

6,000 CYCleS

© continuous IC/IE, SOH KR19

Samsung SDI ESS leverages our manufacturing experience in II and automotive battery cells resulting in superior and adaptive technology. Samsung SDI ESS is recognized as the industry leader in the market, providing our customers with the safest and long lasting batteries.



Sustainable Design

Easy to Upgrade Capacity without Design Change



We are continuously innovating to increase the energy density while maintaining the same form factor and cell dimensions, thus facilitating future upgrades to higher capacity, higher energy density, ESS with no change to pack design.

Accurate Lifetime Simulation



Samsung SDI offers optimal battery solution with its superior lifetime prediction technology. We design and propose a battery system with analyzing the various parameter such as purpose, operation period and installation environment.

Utility & Commercial ESS

Commercial ESS Utility &

Standard Platform

Optimized Battery Platforms Based on High-Density Design Technology



















































footprint and installation cost savings

Higher density enables better

than 16% with upgrades to Samsung

SDI's new advanced module

Energy density has increased more

Energy Platform Com



















Operating Voltage

Dimension (W x D x H)

Cell Capacity Energy







The Highest Lifetime Performance in

a Continuous Charge/Discharge

Optimized Solution for around One

hour of Grid Service

Unique Platform in the ESS Industry

+hour up to 45 minutes Medium Platform

with Mid-range Capabilities

			00 mm (H	
	KWh	_	E	0
100	20	5.19-5.07	\$70 × 650 × 150	4
COL	*	654-822	458×711×1,791 458×711×7,123	32
(00)	680	1/4 : ,004	458 x 711 x 2,125	

M5 R075

M5 M087

458×733×7289



		Module		Rack	
Model		P5 M065	P5 R05/	P5 R070	P5 R0/6
Cell Capacity	Ah	χ,	X.	8//	8/
Energy	kWh	5.5	2/5	07	u/
Operating Voltage	>	7.06-7.89	614 812	666-057	838-3,08,
Dimension $(W \times D \times H)$	mm	570 x 650 x 160	458 x / H x 1,791	455	5.5
Weight	5	5.6		***	***

Power Platform

30 minutes up to 20 minutes

- High Power Platform Optimized for Less than 30 minutes of Use
- Applications such as F/R, Railway, Optimized Solution for Power

Utility & Commercial ESS Battery Platform for

Utility & Commercial ESS

Optimized Battery Platforms Based on High-Density Design Technology

Special Platform

1,500 High Voltage

Platform New



High Efficiency Battery Solution for 1,500V PCS

by Reducing Footprint of PCS and Battery System **Total Footprint**

by Enabling High PowerOutput Power Loss Minimize

Minimize

Maximize Economics & Efficiency

Product Lineup

78 101 1,091-1,443 458 x 711 x 5,082 965 100 130 176-1,461 1785-1,461 1001 8/6×/71×2,/50 1929 114-1444 Dimension (W x D x H) Backup Time Operating Voltage Cell Capacity Energy Weight

Global Track Record

Since 2010, Samsung SDI's ESS products have been successfully operating in over 30 countries.

ESS market, based on best in class battery technology and strong partnerships. Today, Samsung SDI continues to make history by leading the growing global

California 150MWh Deployed 2017-

Canada

Sault Sainte Marie, Ontario 8MW / 8MW!

Europe

Asia & Oceania

KEPCO F/R 38MMh Deployed 2015-

Schwerin 15MWh Deployed 2014/17~

Germany

Korea

KEPCO(5 Sites) 128MW / 38MWh KOEN(3 Sites) 22MW / 63MWh PyeongChang 6MW / 18MWh Ulsan 24MW / STMWh

S

China

Leighton Buzzard 10MWh Deployed 2014~

Tibet 28MWh(2 Sites) Deployed 2016



Barrow in Furness 49MW / 25MWh Leighton Buzzard 6MW / 10MWh Broxburn 20MW / 22MWh

Tibet Shuanghu 2MW / 14MWh Tibet Gaize 4MW / 14MWh

Italy

Potenza 2MW / 2MWth

Netherlands

Zeeland 10MW / 10MWh

Japan



Hokkaido Shinhidaka 17MW 9MWh Hokkaido Chitose 17MW / 14MWh

Australia

Alice Spring AMW / 2MWn Western Australia 4MW / 2MWh Adelaide 30MW/ISMWh

Americas



El Cajon/Escondido, CA 37.5MW / 150MWh Indianapolis, IN 20MW / 20MWh El Centro, CA 30MW / 20MWh Punta Gorda, FL 10MW / 40MWh. Pomona, CA 20MW / 80MWh Austin, TX 36MW / 14MWh Tucson, AZ 10MW / 5MWh

Chemnitz 10MW / 10MWh Hassfurth 10MW / 10MWh

Schwerin 15MW / 15MWh

Port of Tyne 3cMW / 28MWh Tynemouth 75MW / 17MWh

Petham SOMW / SOMWh

Spain

Carboneras 20MW / 12MWh

8

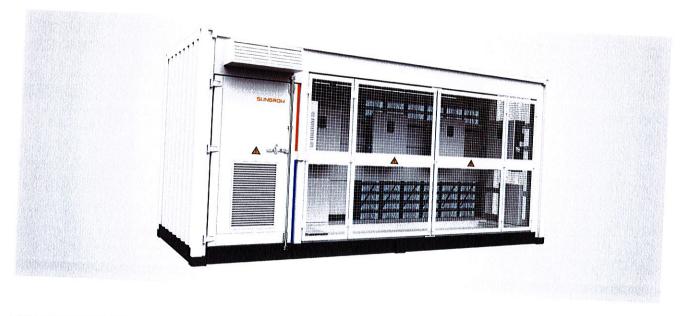
William .





ST548KWH-D250HV +4xSG125HV

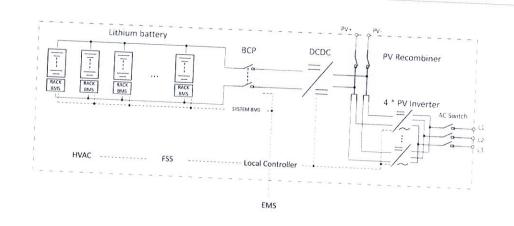
Storage System



SYSTEM FEATURES

- ESS system integrated with PV inverter 180
- 1500V DC coupled PV+ESS system
- Compact mechanical design, minimized footprint
- High efficient system with safe and long lifecycle lithiun-ion battery
- Integrated local controller, HVAC and FSS to enable unified communication and ensure system safety

CIRCUIT DIAGRAM



PV Data	ST548KWH-D250HV+4xSG125HV
Max PV Input voltage	
MPPT voltage range at nominal power	1.500 V
Number of DC inputs	860 ~ 1,250 V
Max. PV input current	5
DCDC Data	1.250 A
Working voltage range	
Nominal power	500 ~ 1,500 V
Max.current	250 KW
Battery Data	344 A
Cell type	
Configuration of system	Samsung SDI Mega E2, 3,68 V 94 An
Battery capacity (BOL)	26456Þ
Battery voltage range	548 kWh
AC Data	844 NO95 V
AC output power	
Max. AC output current	500KVA @ 50 °C
Nominal AC voltage	480 A
AC voltage range	3 / PE. 600 V
Nominal grid frequer cy / Orid frequency range	480 ~ 690 v
Power factor at nominal power. Adjustable power factor	60 Hz / 55 ~ 65 Hz
Feed-in phases / connection phases	> 0.99 / 0.8 leading + 0.8 lagging
General Data	3/3
Dimensions (W · H · D)	
Weight (with / without battery)	6,058 * 2,896 * 2,438 mm / 238,5 * 114,0 * 96,0
Degree of protection	12.5 T / 8.6 T 27.558 lbs /18.960 lbs
Operating temperature range	IP 54 / NEMA 3R
Relative numidity	-30 to 50 °C / -22 to 122 °F
Max, working artitude	0 - 95 % (non-condensing)
Cooling concept of pattery chamber	2,000 m = 5,562 ft
Fire suppression system of pattery unit	Heating, ventilation and Air Conditioning
Communication interfaces	FM-200 extinguishment system
iommunication protocols	95483 Ethernat
ompliance	Modbus RTU Medibus ficip







Power Generation

CHALLENGE:

Protecting sub-stations, electrical switch rooms, control rooms, data communications and other critical areas

SOLUTION:

ANSUL_® FM-200[™] Clean Agent Fire Suppression System

APPLICATION:

Protecting critical operational infrastructure in cramped conditions

Power stations and power generation facilities incorporate a wide range of critical and ancillary services and buildings to ensure continued operations and plant uptime. Away from the primary power circuit, boiler and turbine system; vital facilities such as sub-stations, cable voids, control rooms, data communications and backup systems must be effectively protected against fire risk. Selecting the right solution to protect this critical plant infrastructure is key.

The ANSUL FM-200 Clean Agent Fire Suppression System has zero ozone depletion potential (ODP). The system uses FM-200 (HFC-227ea) fire extinguishant which vaporizes upon discharge and absorbs heat to rapidly suppress fire. This results in less damage to critical equipment, facilitating a much shorter recovery time and reducing downtime. Safe for use in occupied areas at the design concentration, the system helps protect critical infrastructure and delivers effective asset protection for power generation facilities.

The ANSUL FM-200 system is most effective when used with the automatic AUTOPULSE Detection and Control System to introduce the clean agent rapidly. This detection system is used to actuate a single, fixed fire suppression or alarm system based on inputs received from fire detection devices. The detection circuits can be configured using cross, counting, independent or priority-zone concepts.

Both automatic and manual actuators are available for release of the agent into the hazard area through fixed piping and nozzles. Seven nozzle sizes are available to provide the correct flow of agent in either 180 or 360 horizontal discharge patterns. For large hazards, cylinders can be connected to a common manifold.

The ANSUL FM-200 system carries UL, FM and ULC, as well as marine approvals. The system can be designed to meet the requirements of EN 15004, ISO 14520 and NFPA 2001 with components approved to provide the highest quality fire suppression system.





R227EA

A-Gas (U.S. Headquarters)

Chemwatch: 54078 Version No: 6.1.10.9

Safety Data Sheet according to OSHA HazCom Standard (2012) requirements

Chemwatch Hazard Alert Code: 1

Issue Date: 09/09/2018 Print Date: 16/08/2021

L.GHS.USA.EN

SECTION 1 Identification

Product Identifier

Product name R227EA **Chemical Name**

1,1,1,2,3,3,3-heptafluoropropane

Synonyms

F7-C3-H; HFC-227ea; Halon 37; halogenated alkane fire extinguishing agent; FM-200

Proper shipping name Heptafluoropropane or Refrigerant gas R 227

Chemical formula

C3HF7 Not Available

Other means of identification CAS number

431-89-0

Recommended use of the chemical and restrictions on use

Fire extinguishing agent for use in total flooding application.

Relevant identified uses

Hydrofluorocarbons (HFCs) are organic compounds that contain fluorine and hydrogen atoms, and are the most common type of organofluorine compounds. They are frequently used in air conditioning and as refrigerants in place of the older chlorofluorocarbons. Fluorocarbons with few C–F bonds behave similarly to the parent hydrocarbons, but their reactivity can be altered significantly. Packed as liquid under pressure and remains liquid only under pressure.

Name, address, and telephone number of the chemical manufacturer, importer, or other responsible party Registered company name

A-Gas (U.S. Headquarters) 1100 Haskins Rd. Bowling Green, OH 43402 United States Address Telephone 14198678990 Fax 1-419-867-3279 Website www.agasamericas.com Email tammy.myers@agas.com

Emergency phone number

Association / Organisation PERS **Emergency telephone numbers** 1-800-633-8253 Other emergency telephone numbers

International 1-801-629-0667

SECTION 2 Hazard(s) identification

Classification of the substance or mixture

NFPA 704 diamond



Note: The hazard category numbers found in GHS classification in section 2 of this SDSs are NOT to be used to fill in the NFPA 704 diamond. Blue =Health Red = Fire Yellow = Reactivity White = Special (Oxidizer or water reactive substances)

Classification Gases Under Pressure (Liquefied Gas)



Signal word

Warning

Hazard statement(s)

Contains gas under pressure; may explode if heated.

Hazard(s) not otherwise classified

Not Applicable

Precautionary statement(s) General

If medical advice is needed, have product container or label at hand. P101 P102

Keep out of reach of children. Read label before use. P103

Precautionary statement(s) Prevention

Not Applicable

Precautionary statement(s) Response

Not Applicable

Precautionary statement(s) Storage

P410+P403 Protect from sunlight. Store in a well-ventilated place.

Precautionary statement(s) Disposal

Not Applicable

SECTION 3 Composition / information on ingredients

Substances

CAS No	%[weight]	
431-89-0	100	Name
		R227ea

Mixtures

See section above for composition of Substances

SECTION 4 First-aid measures

Description of first aid measures

- If product comes in contact with eyes remove the patient from gas source or contaminated area.
- Take the patient to the nearest eye wash, shower or other source of clean water.
- Open the eyelid(s) wide to allow the material to evaporate.
- Gently rinse the affected eye(s) with clean, cool water for at least 15 minutes. Have the patient lie or sit down and tilt the head back. Hold the eyelid(s) open and pour water slowly over the eyeball(s) at the inner corners, letting the water run out of the outer corners.
- ► The patient may be in great pain and wish to keep the eyes closed. It is important that the material is rinsed from the eyes to prevent

Eye Contact

- Ensure that the patient looks up, and side to side as the eye is rinsed in order to better reach all parts of the eye(s)
- Even when no pain persists and vision is good, a doctor should examine the eye as delayed damage may occur.
- If the patient cannot tolerate light, protect the eyes with a clean, loosely tied bandage.
- Ensure verbal communication and physical contact with the patient.

DO NOT allow the patient to rub the eyes

DO NOT allow the patient to tightly shut the eyes

DO NOT introduce oil or ointment into the eye(s) without medical advice

DO NOT use hot or tepid water.

If skin contact occurs:

- Immediately remove all contaminated clothing, including footwear.
- Flush skin and hair with running water (and soap if available).
- Seek medical attention in event of irritation

Skin Contact

- In case of cold burns (frost-bite): Move casualty into warmth before thawing the affected part; if feet are affected carry if possible
- ▶ Bathe the affected area immediately in luke-warm water (not more than 35 deg C) for 10 to 15 minutes, immersing if possible and

without rubbing

- DO NOT apply hot water or radiant heat.
- Apply a clean, dry, light dressing of "fluffed-up" dry gauze bandage
- If a limb is involved, raise and support this to reduce swelling
- If an adult is involved and where intense pain occurs provide pain killers such as paracetomol
- Transport to hospital, or doctor
- Subsequent blackening of the exposed tissue indicates potential of necrosis, which may require amputation.
- Following exposure to gas, remove the patient from the gas source or contaminated area.
- NOTE: Personal Protective Equipment (PPE), including positive pressure self-contained breathing apparatus may be required to assure
- ▶ Prostheses such as false teeth, which may block the airway, should be removed, where possible, prior to initiating first aid procedures. If the patient is not breathing spontaneously, administer rescue breathing.
- If the patient does not have a pulse, administer CPR.
- If medical oxygen and appropriately trained personnel are available, administer 100% oxygen. Summon an emergency ambulance. If an ambulance is not available, contact a physician, hospital, or Poison Control Centre for further
- Keep the patient warm, comfortable and at rest while awaiting medical care.
- MONITOR THE BREATHING AND PULSE, CONTINUOUSLY.
- Administer rescue breathing (preferably with a demand-valve resuscitator, bag-valve mask-device, or pocket mask as trained) or CPR if Not considered a normal route of entry.
- For advice, contact a Poisons Information Centre or a doctor.
- Avoid giving milk or oils.
- Avoid giving alcohol.

Most important symptoms and effects, both acute and delayed

See Section 11

Indication of any immediate medical attention and special treatment needed

for intoxication due to Freons/ Halons;

A: Emergency and Supportive Measures

Maintain an open airway and assist ventilation if necessary

Inhalation

Ingestion

- ▶ Treat coma and arrhythmias if they occur. Avoid (adrenaline) epinephrine or other sympathomimetic amines that may precipitate ventricular arrhythmias. Tachyarrhythmias caused by increased myocardial sensitisation may be treated with propranolol, 1-2 mg IV or esmolol 25-100 microgm/kg/min IV.
- B: Specific drugs and antidotes:
- Triere is no specific antidote

C: Decontamination

- Inhalation; remove victim from exposure, and give supplemental oxygen if available.
- Ingestion; (a) Prehospital: Administer activated charcoal, if available. DO NOT induce vomiting because of rapid absorption and the risk of abrupt onset CNS depression. (b) Hospital: Administer activated charcoal, although the efficacy of charcoal is unknown. Perform gastric lavage only if the ingestion was very large and recent (less than 30 D: Enhanced elimination:
- There is no documented efficacy for diuresis, haemodialysis, haemoperfusion, or repeat-dose charcoal.

POISONING and DRUG OVERDOSE, Californian Poison Control System Ed. Kent R Olson; 3rd Edition

- Do not administer sympathomimetic drugs unless absolutely necessary as material may increase myocardial irritability.
- Because rapid absorption may occur through lungs if aspirated and cause systematic effects, the decision of whether to induce vomiting or not should be made by an If lavage is performed, suggest endotracheal and/or esophageal control.
- Danger from lung aspiration must be weighed against toxicity when considering emptying the stomach.
- Treatment based on judgment of the physician in response to reactions of the patient

For frost-bite caused by liquefied petroleum gas:

- If part has not thawed, place in warm water bath (41-46 C) for 15-20 minutes, until the skin turns pink or red.
- If there has been a massive exposure, the general body temperature must be depressed, and the patient must be immediately rewarmed by whole-body immersion, in a Shock may occur during rewarming.
- Administer tetanus toxoid booster after hospitalization.
- Prophylactic antibiotics may be useful.
- The patient may require anticoagulants and oxygen

[Shell Australia 22/12/87]

For gas exposures:

BASIC TREATMENT

- Establish a patent airway with suction where necessary.
- Watch for signs of respiratory insufficiency and assist ventilation as necessary.
- Administer oxygen by non-rebreather mask at 10 to 15 l/min.
- Monitor and treat, where necessary, for pulmonary oedema.
- ► Monitor and treat, where necessary, for shock.
- Anticipate seizures.

ADVANCED TREATMENT

- Consider orotracheal or nasotracheal intubation for airway control in unconscious patient or where respiratory arrest has occurred.
- Positive-pressure ventilation using a bag-valve mask might be of use.
- Monitor and treat, where necessary, for arrhythmias.
- Start an IV D5W TKO. If signs of hypovolaemia are present use lactated Ringers solution. Fluid overload might create complications.
- Drug therapy should be considered for pulmonary oedema.
- Hypotension with signs of hypovolaemia requires the cautious administration of fluids. Fluid overload might create complications.
- Proparacaine hydrochloride should be used to assist eye irrigation.

BRONSTEIN, A.C. and CURRANCE, P.L.

EMERGENCY CARE FOR HAZARDOUS MATERIALS EXPOSURE: 2nd Ed. 1994

SECTION 5 Fire-fighting measures

Extinguishing media

SMALL FIRE: Use extinguishing agent suitable for type of surrounding fire.

LARGE FIRE: Cool cylinder.

DO NOT direct water at source of leak or venting safety devices as icing may occur.

Special hazards arising from the substrate or mixture

Fire Incompatibility

* Avoid contamination with oxidising agents i.e. nitrates, oxidising acids, chlorine bleaches, pool chlorine etc. as ignition may result

Special protective equipment and precautions for fire-fighters

GENERAL

Fire Fighting

- Alert Fire Brigade and tell them location and nature of hazard.
- Wear breathing apparatus and protective gloves
- Fight fire from a safe distance, with adequate cover.
- Use water delivered as a fine spray to control fire and cool adjacent area.
- ▶ Containers may explode when heated Ruptured cylinders may rocket
- Fire exposed containers may vent contents through pressure relief devices.
- ► High concentrations of gas may cause asphyxiation without warning.
- May decompose explosively when heated or involved in fire.
- Contact with gas may cause burns, severe injury and/ or frostbite.

Fire/Explosion Hazard

Decomposition may produce toxic fumes of:

carbon monoxide (CO)

carbon dioxide (CO2)

hydrogen fluoride

other pyrolysis products typical of burning organic material.

Contains low boiling substance: Closed containers may rupture due to pressure buildup under fire conditions.

SECTION 6 Accidental release measures

Personal precautions, protective equipment and emergency procedures

See section 8

Environmental precautions

See section 12

Methods and material for containment and cleaning up

Minor Spills

- Avoid breathing vapour and any contact with liquid or gas. Protective equipment including respirator should be used.
- DO NOT enter confined spaces where gas may have accumulated.
- Increase ventilation.
- Clear area of all unprotected personnel and move upwind.
- Alert Emergency Authority and advise them of the location and nature of hazard.
- Wear breathing apparatus and protective gloves.

Major Spills

- Prevent by any means available, spillage from entering drains and water-courses.
- Remove leaking cylinders to a safe place.
- Fit vent pipes. Release pressure under safe, controlled conditions
- Burn issuing gas at vent pipes.
- DO NOT exert excessive pressure on valve; DO NOT attempt to operate damaged valve.

Personal Protective Equipment advice is contained in Section 8 of the SDS.

Precautions for safe handling

Safe handling

-Consider use in closed pressurised systems, fitted with temperature, pressure and safety relief valves which are vented for safe dispersal. Use only properly specified equipment which is suitable for this product, its supply pressure and temperature The tubing network design connecting gas cylinders to the delivery system should include appropriate pressure indicators and

Fully-welded types of pressure gauges, where the bourdon tube sensing element is welded to the gauge body, are recommended. Before connecting gas cylinders, ensure manifold is mechanically secure and does not containing another gas.

DO NOT transfer gas from one cylinder to another.

Do NOT store halogenated aliphatics in areas containing alkali or alkaline earth metals such as powdered aluminum, zinc, or

Other information

- Store below 38 deg. C.
- Cylinders should be stored in a purpose-built compound with good ventilation, preferably in the open.
- Such compounds should be sited and built in accordance with statutory requirements.
- The storage compound should be kept clear and access restricted to authorised personnel only.
- Cylinders stored in the open should be protected against rust and extremes of weather.

Conditions for safe storage, including any incompatibilities

Suitable container

- DO NOT use aluminium or galvanised containers Cylinder
- Ensure the use of equipment rated for cylinder pressure.
- Ensure the use of compatible materials of construction. Valve protection cap to be in place until cylinder is secured, connected.
- Cylinder must be properly secured either in use or in storage.

Haloalkanes:

- are highly reactive:some of the more lightly substituted lower members are highly flammable; the more highly substituted may be used as fire suppressants, not always with the anticipated results.
- may react with the lighter divalent metals to produce more reactive compounds analogous to Grignard reagents.
- may produce explosive compounds following prolonged contact with metallic or other azides
- * may react on contact with potassium or its alloys although apparently stable on contact with a wide rage of halocarbons, reaction products may be shock-sensitive and may explode with great violence on light impact; severity generally increases with the degree of halocarbon substitution and potassium-sodium alloys give extremely sensitive mixtures

Storage incompatibility

BRETHERICK L.: Handbook of Reactive Chemical Hazards

- react with metal halides and active metals, eg. sodium (Na), potassium (K), lithium (Li), calcium (Ca), zinc (Zn), powdered aluminium (Al) and aluminium alloys, magnesium (Mg) and magnesium alloys.
- As a general rule, hydrofluorocarbons tend to be flammable unless they contain more fluorine atoms than hydrogen atoms.
- Compressed gases may contain a large amount of kinetic energy over and above that potentially available from the energy of reaction produced by the gas in chemical reaction with other substances

SECTION 8 Exposure controls / personal protection

Control parameters

Occupational Exposure Limits (OEL)

INGREDIENT DATA

Not Available

Emergency Limits

Ingredient	TEEL-1	TEEL-2	TEEL-3
R227EA	Not Available	Not Available	Not Available
Ingredient	Original IDLH	Revised IDLH	

Revised IDLH R227ea Not Available Not Available

MATERIAL DATA

Sensory irritants are chemicals that produce temporary and undesirable side-effects on the eyes, nose or throat. Historically occupational exposure standards for these irritants have been based on observation of workers' responses to various airborne concentrations. Present day expectations require that nearly every individual should be protected against even minor sensory irritation and exposure standards are established using uncertainty factors or safety factors of 5 to 10 or more. On occasion animal no-observableeffect-levels (NOEL) are used to determine these limits where human results are unavailable

Exposure controls

Appropriate engineering

Engineering controls are used to remove a hazard or place a barrier between the worker and the hazard. Well-designed engineering controls can be highly effective in protecting workers and will typically be independent of worker interactions to provide this high level of protection.

Process controls which involve changing the way a job activity or process is done to reduce the risk.

Enclosure and/or isolation of emission source which keeps a selected hazard "physically" away from the worker and ventilation that strategically "adds" and "removes" air in the work environment.

Personal protection

Eye and face protection









- Chemical goggles.
- Full face shield may be required for supplementary but never for primary protection of eyes.
- Contact lenses may pose a special hazard; soft contact lenses may absorb and concentrate irritants. A written policy document, describing the wearing of lenses or restrictions on use, should be created for each workplace or task. See Hand protection below

Skin protection

- Butyl rubber gloves
 - Butyl rubber gloves should be used when handling halogenated aliphatics Nitrile, PVC-coated nitrile, and PVC protective equipment are not recommended
- Neoprene gloves
- Polyethylene gloves
 - When handling sealed and suitably insulated cylinders wear cloth or leather gloves.
 - ► Insulated gloves:

NOTE: Insulated gloves should be loose fitting so that may be removed quickly if liquid is spilled upon them. Insulated gloves are not made to permit hands to be placed in the liquid; they provide only short-term protection from accidental contact with the liquid. See Other protection below

Body protection

Hands/feet protection

Halogen-selective detectors use a specialized sensor that allows the monitor to detect compounds containing fluorine, chlorine, bromine, and iodine with-out interference from other species. These detectors are typically easy to use, feature higher sensitivity than the nonselective detectors (detection limits are typically <5 ppm when used as an area monitor and <1.4 gm/yr [<0.05 oz/yr]

Other protection

- Compound-Specific Detectors are typically capable of detecting the presence of a single compound without interference from other compounds.
- Protective overalls, closely fitted at neck and wrist.
- Eye-wash unit.
- Ensure availability of lifeline in confined spaces.
- Staff should be trained in all aspects of rescue work.

Respiratory protection

Type AX Filter of sufficient capacity. (AS/NZS 1716 & 1715, EN 143:2000 & 149:2001, ANSI Z88 or national equivalent)

Selection of the Class and Type of respirator will depend upon the level of breathing zone contaminant and the chemical nature of the contaminant. Protection Factors (defined

	, was be important.	65.400	rection ractors (defined
Required minimum protection factor	Maximum gas/vapour concentration		
up to 10	Maximum gas/vapour concentration present in air p.p.m. (by volume)	Half-face Respirator	Full-Face Respirator
up to 50	1000	AX-AUS / Class1	•
up to 50	5000	•	AX-AUS / Class 1
up to 100	5000	Airline *	Tal.
up to 100	10000		AX-2
100+		•	AX-3
- Continuous Flow ** - Continuous-flow or n			Airline * *

^{* -} Continuous Flow ** - Continuous-flow or positive pressure demand

A(All classes) = Organic vapours, B AUS or B1 = Acid gasses, B2 = Acid gas or hydrogen cyanide(HCN), B3 = Acid gas or hydrogen cyanide(HCN), E = Sulfur dioxide(SO2), G = Agricultural chemicals, K = Ammonia(NH3), Hg = Mercury, NO = Oxides of nitrogen, MB = Methyl bromide, AX = Low boiling point organic compounds(below 65 degC)

- Cartridge respirators should never be used for emergency ingress or in areas of unknown vapour concentrations or oxygen content.
- ▶ The wearer must be warned to leave the contaminated area immediately on detecting any odours through the respirator. The odour may indicate that the mask is not functioning properly, that the vapour concentration is too high, or that the mask is not properly fitted. Because of these limitations, only restricted use of cartridge respirators is considered appropriate.
- Cartridge performance is affected by humidity. Cartridges should be changed after 2 hr of continuous use unless it is determined that the humidity is less than 75%, in which case, cartridges can be used for 4 hr. Used cartridges should be discarded daily, regardless of the length of time used
- Positive pressure, full face, air-supplied breathing apparatus should be used for work in enclosed spaces if a leak is suspected or the primary containment is to be opened
- Air-supplied breathing apparatus is required where release of gas from primary containment is either suspected or demonstrated.

SECTION 9 Physical and chemical properties

Information on basic physical and chemical properties

Appearance			
Appearance	Colourless, odourless comp	ressed gas; does not mix with water.	
Physical state	Liquified Gas		
		Relative density (Water = 1)	1.46
Odour	Not Available	Partition coefficient n-octanol	
Odour threshold	Not Available	/ water	Not Available
pH (as supplied)	Not Applicable	Auto-ignition temperature (°C)	Not Applicable
· · · · · · · · · · · · · · · · · · ·	Not Applicable	Decomposition temperature	Not Available

Melting point / freezing point (°C)	-131	E	
nitial boiling point and boiling		Viscosity (cSt)	Not Availabl
range (°C)	-16.4	MALESTAN SERVICE	
Flash point (°C)	Not Applicable	Molecular weight (g/mol)	170.03
Evaporation rate	Not Available	Taste	Not Available
Flammability	Not Applicable	Explosive properties	Not Available
Unner Fred		Oxidising properties	Not Available
Upper Explosive Limit (%)	Not Applicable	Surface Tension (dyn/cm or	
Lower Explosive Limit (%)	Not Applicable	mN/m)	Not Available
Vapour pressure (kPa)	404.32 @ 21 C	Volatile Component (%vol)	100
Solubility in water	Immiscible	Gas group	Not Available
Vapour density (Air = 1)	Not Available	pH as a solution (%)	Not Applicable
		VOC g/L	Not Available

SECTION 10 Stability and reactivity

Reactivity	See section 7
Chemical stability	 Unstable in the presence of incompatible materials. Product is considered stable. Hazardous polymerisation will not occur.
Possibility of hazardous reactions	See section 7
Conditions to avoid	See section 7
Incompatible materials	See section 7
Hazardous decomposition products	See section 5

SECTION 11 Toxicological information

Information on toxicological effects

Inhaled

Inhalation of vapours may cause drows ness and dizzness. This may be accompanied by narcosis, reduced alertness, loss of reflexes, lack of

Inhalation of vapours or aerosols (mists, fumes), generated by the material during the course of normal handling, may be damaging to the

Limited evidence or practical experience suggests that the material may produce irritation of the respiratory system, in a significant number of individuals, following inhalation. In contrast to most organs, the lung is able to respond to a chemical insult by first removing or neutralising the irritant and then repairing the damage. The repair process, which initially evolved to protect mammalian lungs from foreign matter and antigens, may however, produce further lung damage resulting in the impairment of gas exchange, the primary function of the lungs. Respiratory tract irritation often results in an inflammatory response involving the recruitment and activation of many cell types,

Exposure to high concentrations of fluorocarbons may produce cardiac arrhythmias or cardiac arrest due sensitisation of the heart to adrenalin or noradrenalin. Deaths associated with exposures to fluorocarbons (specifically halogenated aliphatics) have occurred in occupational settings and in inhalation of bronchodilator drugs.

Bronchospasm consistently occurs in human subjects inhaling fluorocarbons. At a measured concentration of 1700 ppm of one of the commercially available aerosols there is a biphasic change in ventilatory capacity, the first reduction occurring within a few minutes and the

Common, generalised symptoms associated with non-toxic gas inhalation include

- central nervous system effects such as headache, confusion, dizziness, progressive stupor, coma and seizures:
- respiratory system complications may include tachypnoea and dyspnoea;
- cardiovascular effects may include circulatory collapse and arrhythmias;
- gastrointestinal effects may also be present and may include mucous membrane irritation and nausea and vomiting.

Acute intoxication by halogenated aliphatic hydrocarbons appears to take place over two stages. Signs of a reversible narcosis are evident in the first stage and in the second stage signs of injury to organs may become evident, a single organ alone is (almost) never involved. Depression of the central nervous system is the most outstanding effect of most halogenated aliphatic hydrocarbons. Inebriation and excitation, passing into narcosis, is a typical reaction. In severe acute exposures there is always a danger of death from respiratory failure or cardiac arrest due to a tendency to make the heart more susceptible to catecholamines (adrenalin)

Material is highly volatile and may quickly form a concentrated atmosphere in confined or unventilated areas. The vapour may displace and replace air in breathing zone, acting as a simple asphyxiant. This may happen with little warning of overexposure.

The use of a quantity of material in an unventilated or confined space may result in increased exposure and an irritating atmosphere developing. Before starting consider control of exposure by mechanical ventilation.

Overexposure is unlikely in this form. Ingestion

Not normally a hazard due to physical form of product.

Considered an unlikely route of entry in commercial/industrial environments

Prolonged or widespread skin contact with the liquid may result in the absorption of harmful amounts of material. Repeated exposure may cause skin cracking, flaking or drying following normal handling and use. Skin contact with the material may damage the health of the individual; systemic effects may result following absorption.

Skin Contact

Limited evidence exists, or practical experience predicts, that the material either produces inflammation of the skin in a substantial number

of individuals following direct contact, and/or produces significant inflammation when applied to the healthy intact skin of animals, for up to four hours, such inflammation being present twenty-four hours or more after the end of the exposure period. Skin irritation may also be present after prolonged or repeated exposure; this may result in a form of contact dermatitis (nonallergic). The dermatitis is often characterised by skin redness (erythema) and swelling (oedema) which may progress to blistering (vesiculation), scaling and thickening of the epidermis. At the microscopic level there may be intercellular oedema of the spongy layer of the skin (spongiosis) and intracellular oedema

In common with other halogenated aliphatics, fluorocarbons may cause dermal problems due to a tendency to remove natural oils from the skin causing irritation and the development of dry, sensitive skin. They do not appear to be appreciably absorbed. Open cuts, abraded or irritated skin should not be exposed to this material

Material on the skin evaporates rapidly and may cause tingling, chilling and even temporary numbness

Entry into the blood-stream through, for example, cuts, abrasions, puncture wounds or lesions, may produce systemic injury with harmful effects. Examine the skin prior to the use of the material and ensure that any external damage is suitably protected.

Vapourising liquid causes rapid cooling and contact may cause cold burns, frostbite, even through normal gloves. Frozen skin tissues are painless and appear waxy and yellow. Signs and symptoms of frost-bite may include "pins and needles", paleness followed by numbness, a hardening an stiffening of the skin, a progression of colour changes in the affected area, (first white, then mottled and blue and eventually

Eye

Although the material is not thought to be an irritant (as classified by EC Directives), direct contact with the eye may produce transient discomfort characterised by tearing or conjunctival redness (as with windburn).

Direct contact with the eye may not cause irritation because of the extreme volatility of the gas; however concentrated atmospheres may

Limited evidence suggests that repeated or long-term occupational exposure may produce cumulative health effects involving organs or

Chronic

It is generally accepted that the fluorocarbons are less toxic than the corresponding halogenated aliphatic based on chlorine. Repeated inhalation exposure to the fluorocarbon FC-11 does not produce pathologic lesions of the liver and other visceral organs in experimental animals. There has been conjecture in non-scientific publications that fluorocarbons may cause leukemia, cancer, sterility and birth defects; these have not been verified by current research. The high incidence of cancer, spontaneous abortion and congenital anomalies amongst hospital personnel, repeatedly exposed to fluorine-containing general anaesthetics, has caused some scientists to call for a lowering of the Principal route of occupational exposure to the gas is by inhalation.

0222	TOXICITY	
R227ea	Inhalation(Rat) LC50; >788696 ppm4h[1]	IRRITATION
	7/88696 ppm4h[1]	Not Available

Legend:

1. Value obtained from Europe ECHA Registered Substances - Acute toxicity 2. * Value obtained from manufacturer's SDS. Unless otherwise specified data extracted from RTECS - Register of Toxic Effect of chemical Substances

R227EA

Disinfection by products (DBPs) re formed when disinfectants such as chlorine, chloramine, and ozone react with organic and inorganic matter in water. The observations that some DBPs such as trihalomethanes (THMs), di-/trichloroacetic acids, and 3-chloro-4-(dichloromethyl)-5-hydroxy-2(5H)-furanone (MX) are carcinogenic in animal studies have raised public concern over the possible adverse

Numerous haloalkanes and haloalkenes have been tested for carcinogenic and mutagenic activities. In general, the genotoxic potential is dependent on the nature, number, and position of halogen(s) and the molecular size of the compound.

×	Acute Toxicity
×	Skin Irritation/Corrosion
×	Serious Eye Damage/Irritation
v	Respiratory or Skin
	sensitisation
×	Mutagenicity

 $oldsymbol{\mathsf{X}}$ – Data either not available or does not fill the criteria for classification Data available to make classification

SECTION 12 Ecological information

Toxicity

	Endpoint	_astron			
	Litapoint	Test Duration (hr)	Species		
	NOEC(ECx)	96h	Species	Value	C
R227ea	Fore		Fish		Source
rzz/ea	EC50	72h		10mg/I	2
	LC50	96h	Algae or other aquatic plants	>114mg/	2
	5650		Fish	0.	2
	EC50	48h		>81.8mg/l	2
			Crustacea	>97.9mg/l	9
Legend:	Extracted from	1. IUCLID Toxicity Data 2 Europe 5			2
	V3.12 (QSAR) -	Aquatic Toxicity Data (5-1	CHA Registered Substances - Ecotoxicological Information		
	Data 6. NITE (Ja	pan) - Bioconcentration 2	CHA Registered Substances - Ecotoxicological Information - L. US EPA, Ecotox database - Aquatic Toxicity Data 5 - ECETO.	Aquatic loxicity 3. EPI	WIN Suite

V3.12 (QSAR) - Aquatic Toxicity Data (Estimated) 4. US EPA, Ecotox database - Aquatic Toxicity Data 5. ECETOC Aquatic Hazard Assessment Data 6. NITE (Japan) - Bioconcentration Data 7. METI (Japan) - Bioconcentration Data 8. Vendor Data

HFCs (hydrofluorocarbons) have been widely used as replacements for Ozone Depletion Substances (ODSs.) Because they do not contain chlorine or bromine, they have an ozone Depletion Potential (ODP) of 0. However, certain HFCs have high Global warming Potential (GWPs). Perfluorinated fluorocarbons (PFCs) have extremely high GWPs and long atmospheric lifetimes. They do not deplete stratospheric ozone, but the U.S. Environmental Protection Agency (EPA) is concerned about their impact on global warming. 90halkane

In addition to carbon dioxide (CO2), methane (CH4) and nitrous oxide (N2O), the greenhouse gases mentioned in the Kyoto Protocol include synthetic substances that share the common feature of being highly persistent in the atmosphere and exhibiting very high specific radiative forcing (radiative forcing is the change in the balance between radiation coming into the atmosphere and radiation out; a positive radiative forcing tends on average to warm the surface of the earth). These synthetic substances include hydrocarbons that are partially fluorinated (HCFs) or totally fluorinated (PFCs) as well as sulfur hexafluoride (SF6).

The greenhouse potential of these substances, expressed as multiples of that of CO2, are within the range of 140 to 11,700 for HFCs, from 6500 to 9,200 for PFCs and 23,900 for SF6. Once emitted into the atmosphere, these substances have an impact on the environment for decades, centuries, or in certain instances, for thousands of years.

DO NOT discharge into sewer or waterways.

Persistence and degradability

Ingredient	Persistence: Water/Soil	Persistence: Air
R227ea	HIGH	HIGH

Bioaccumulative potential

Ingredient	Bioaccumulation	
R227ea	LOW (LogKOW = 2.5133)	

Mobility in soil

Ingredient	Mobility	
R227ea	LOW (KOC = 680.2)	

SECTION 13 Disposal considerations

Waste treatment methods

Product / Packaging disposal

- Evaporate residue at an approved site.
- Return empty containers to supplier. If containers are marked non-returnable establish means of disposal with manufacturer prior to
- Ensure damaged or non-returnable cylinders are gas-free before disposal.

SECTION 14 Transport information

Labels Required



Marine Pollutant

Land transport (DOT)

UN number UN proper shipping name	3296 Heptafluoropropane or Refrigerant gas R 227		
Transport hazard class(es)	Class 2.2 Subrisk Not Applicable		
Packing group Environmental hazard	Not Applicable Not Applicable		
Special precautions for user	Hazard Label 2.2 Special provisions T50		

Air transport (ICAO-IATA / DGR)

UN number	3296		
UN proper shipping name	Refrigerant gas R 227; Heptafluoropropar		
	ICAO/IATA Class	2.2	
Transport hazard class(es)	ICAO / IATA Subrisk	Not Applicable	
	ERG Code	2L	
	eno code	21	

Packing group Not Applicable **Environmental hazard** Not Applicable Special provisions Not Applicable Cargo Only Packing Instructions 200 Cargo Only Maximum Qty / Pack Special precautions for user 150 kg Passenger and Cargo Packing Instructions 200 Passenger and Cargo Maximum Qty / Pack 75 kg Passenger and Cargo Limited Quantity Packing Instructions Forbidden Passenger and Cargo Limited Maximum Qty / Pack

Sea transport (IMDG-Code / GGVSee)

	1.50	
UN number UN proper shipping name	3296 HEPTAFLUOROPRO	PANE (REFRIGERANT GAS R 227)
Transport hazard class(es)	IMDG Class	2.2 Not Applicable
Packing group Environmental hazard	Not Applicable Not Applicable	
Special precautions for user	EMS Number Special provisions Limited Quantities	F-C , S-V Not Applicable 120 mL

Transport in bulk according to Annex II of MARPOL and the IBC code Not Applicable

Transport in bulk in accordance with MARPOL Annex V and the IMSBC Code

Product name

Group

R227ea

Not Available

Transport in bulk in accordance with the ICG Code

Product name

Ship Type

R227ea

Not Available

SECTION 15 Regulatory information

Safety, health and environmental regulations / legislation specific for the substance or mixture

R227ea is found on the following regulatory lists

US Toxic Substances Control Act (TSCA) - Chemical Substance Inventory

US TSCA Chemical Substance Inventory - Interim List of Active Substances

Forbidden

Federal Regulations

Superfund Amendments and Reauthorization Act of 1986 (SARA)

Section 311/312 hazard categories

317 312 Hazard categories	
Flammable (Gases, Aerosols, Liquids, or Solids)	
Gas under pressure	
Explosive	No
Self-heating	Yes
Pyrophoric (Liquid or Solid)	No
Pyrophoric Gas	No
Corrosive to metal	No
Oxidizer (Liquid, Solid or Gas)	No
Organic Peroxide	No
Self-reactive	No
In contact with water emits flammable gas	No
Combustible Dust	No
Carcinogenicity	No
	No
	No

Acute toxicity (any route of exposure)	
Reproductive toxicity	No
Skin Corrosion or Irritation	No
Respiratory or Skin Sensitization	No
Serious eye damage or eye irritation	No
Specific target organ toxicity (single or repeated exposure)	No
Aspiration Hazard	No
Germ cell mutagenicity	No
Simple Asphyxiant	No
Hazards Not Otherwise Clarified	No
	No
US. EPA CERCLA Hazardous Substances and Reportable Quantity of the substances and Reportable Quantity	140

US. EPA CERCLA Hazardous Substances and Reportable Quantities (40 CFR 302.4)

None Reported

State Regulations

US. California Proposition 65

None Reported

National Inventory Status

status inventory Status	
National Inventory	Status
Australia - AIIC / Australia Non-Industrial Use	Yes
Canada - DSL	Yes
Canada - NDSL	No (R227ea)
China - IECSC	Yes
Europe - EINEC / ELINCS / NLP	Yes
Japan - ENCS	Yes
Korea - KECI	Yes
New Zealand NZIOC	Yes
Philippines - PICCS	Yes
USA - TSCA	Yes
Taiwan - TCSI	Yes
Mexico - INSQ	Yes
Vietnam - NCI	Yes
Russia - FBEPH	Yes
Legend:	Yes = All CAS declared ingredients are on the inventory No = One or more of the CAS listed ingredients are not on the inventory. These ingredients may be exempt or will require registration.
SECTION 16 Other information	oc exempt or will require registration.

SECTION 16 Other information

Revision Date	09/09/2018
Initial Date	04/10/2003

SDS Version Summary

Version	Date of Update	Sections Updated
5.1.2.1	15/04/2009	Acute Health (eye), Acute Health (skin), Advice to Doctor, Disposal, Fire Fighter (fire/explosion hazard), Fire Fighter (fire incompatibility), First Aid (eye), First Aid (skin), Personal Protection (Respirator), Personal Protection (eye), Personal Protection (eye
6.1.2.1	09/09/2018	Acute Health (eye), Acute Health (inhaled), Acute Health (skin), Advice to Doctor, Classification, Environmental, Exposure Standard, Fire Fighter (fire/explosion hazard), Personal Protection (other), Personal Protection (Respirator), Personal Information, Synonyms, Toxicity and Irritation (Other), Use
6.1.3.1	10/05/2021	Regulation Change
6.1.4.1	24/05/2021	Regulation Change
6.1.4.2	30/05/2021	Template Change
6.1.4.3	04/06/2021	Template Change
6.1.4.4	05/06/2021	Template Change
6.1.4.5	09/06/2021	Template Change

Version	Date of Update	Sections Updated
6.1.4.6	11/06/2021	Template Change
6.1.4,7	15/06/2021	Template Change
6.1.4.8	05/07/2021	Template Change
6.1.5.8	14/07/2021	Regulation Change
6.1.6.8	15/07/2021	Regulation Change
6.1.6.9	01/08/2021	Template Change
6.1.7.9	02/08/2021	Regulation Change
6.1.8,9	05/08/2021	Regulation Change
6.1.9.9	09/08/2021	Regulation Change
6.1.10.9	16/08/2021	Regulation Change

Other information

Classification of the preparation and its individual components has drawn on official and authoritative sources as well as independent review by the Chemwatch Classification

The SDS is a Hazard Communication tool and should be used to assist in the Risk Assessment. Many factors determine whether the reported Hazards are Risks in the workplace or other settings. Risks may be determined by reference to Exposures Scenarios. Scale of use, frequency of use and current or available engineering controls must be considered.

Definitions and abbreviations

PC — TWA: Permissible Concentration-Time Weighted Average

PC — STEL: Permissible Concentration-Short Term Exposure Limit

IARC: International Agency for Research on Cancer

ACGIH: American Conference of Governmental Industrial Hygienists

STEL: Short Term Exposure Limit

TEEL: Temporary Emergency Exposure Limit。

IDLH: Immediately Dangerous to Life or Health Concentrations

ES: Exposure Standard

OSF: Odour Safety Factor

MOAEL :No Observed Adverse Effect Level

LOAEL: Lowest Observed Adverse Effect Fixel

TLV: Threshold Lim t Value

LOD: Limit Of Detection

OTV: Odour Threshold Value

BCF: BioConcentration Factors

BEI: Biological Exposure Index

AllC: Australian Inventory of Industrial Chemicals

DSL: Domestic Substances List

NDSL: Non-Domestic Substances List

IECSC: Inventory of Existing Chemical Substance in China

EINECS: European Inventory of Existing Commercial chemical Substances

ELINCS: European List of Notified Chemical Substances

NLP: No-Longer Polymers

ENCS: Existing and New Chemical Substances Inventory

KECI: Korea Existing Chemicals Inventory

NZIoC: New Zealand Inventory of Chemicals

PICCS: Philippine Inventory of Chemicals and Chemical Substances

TSCA: Toxic Substances Control Act

TCSI: Taiwan Chemical Substance Inventory

INSQ: Inventario Nacional de Sustancias Químicas

NCI: National Chemical Inventory

FBEPH: Russian Register of Potentially Hazardous Chemical and Biological Substances

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Envirotemp 360 fluid

Synthetic Ester Fluid

Product Description

Envirotemp 360 fluid is a less flammable dielectric liquid ideally suited for use in free-breathing transformers (both new and retrofill) and is also proven in traction transformers. Envirotemp 360 fluid has been thoroughly evaluated and conforms to IEC 61099 "Specifications for Unused Synthetic Organic Esters for Electrical Purposes."

Advantages

- The high fire point (315°C vs 160°C for mineral oil) allows its classification as a K-Class, less flammable liquid.
- It is a high thermal class dielectric liquid, suitable for use in free-breathing applications.
- It continues to flow even in extremely cold climates.
- Envirotemp 360 fluid is optimized for oxidative stability. It surpasses the required performance of the oxidative stability test of synthetic ester liquids^a even when tested for a period almost 5x longer.
- It is readily biodegradable according to OECD 301B and not classified as hazardous according to GHS.

Envirotemp[™]360 fluid values and specification units

PHYSICAL	TEST METHOD	IEC 61099 PERMISSIBLE VALUES	-
Color	ISO 2211		TYPICAL
	ISO 2049	≤ 200 Hazen	≤ 100 Hazen 0.1
Appearance	Vigually at -		0.1
Density at 20°C (kg/dm³)	visually clear, free from water,	suspended matter and sediment	
Kinematic viscosity (mm²/s)	ISO 3675,ISO 12185 ISO 3104	≤ 1000	
100°C	130 3 104	2 1000	960
40°C			
-20°C		≤ 35	6
		≤ 3000	34
Flash-point (°C)	ISO 2719	0000	1700
Fire-point (°C)	ISO 2592	≥ 250	000
Pour-point (°C)	ISO 3016	≥ 300	>283
HEMICAL	100 00 10	≤ -45	>315
Vater content (mg/kg)			< -48
Acidity (mg KOH/g)	IEC 60814	2004	
(ing KOn/g)	IEC 62021 -1, IEC 62021 -2	≤ 200 ^b	≤ 50
		≤ 0.03	0.01 - 0.02
XIDATION STABILITY 64 h @ 120°C			0.07 - 0.02
Total acidity (mg KOH/g)	IEC 61125, Method C		
Otal sludge (% mass)		≤ 0.3	
00 h @ 120°C	IEC 61125, Method C	≤ 0.01	0.13
Total acidity (mg KOH/g)	120 01125, Wethod C		< 0.01
Total sludge (% mass)			0.04
			0.21
ECTRICAL			< 0.01
eak down voltage (kV)			
	IEC 60156		
electric dissipation factor(tanδ)	ASTM D1816	≥ 45°	68
90°C and 50 Hz	IEC 60247, IEC 61620		59
resistivity at 90°C(GΩ·m)	THE STATE OF THE S	≤ 0.03 ^b	
, (0.1.11)	IEC 60247	≥ 2	0.01
		< 2	60

^a IEC 61099 requires testing synthetic ester liquids according to IEC 61125 method C for 164h. Envirotemp 360 was tested for 800h.

Material Compatibility

Envirotemp* 360 fluid is compatible with most materials used in conventional mineral oil filled transformers. Some restrictions may exist with materials such as PVC's, certain silicone rubber formulations, and polyurethanes. It is recommended to verify the chemical compatibility for each application.

Storage Location

Indoor tank storage is preferable. Since the fluid viscosity increases at low temperatures, indoor controlled temperatures reduce the need for heating the fluid to proper pumping and filtering temperatures.

For outdoor installations, a thermal insulating backfill should be considered for economic advantages. Despite having a low pour point temperature, increased fluid viscosity at low temperatures may make it difficult to handle.

Storage Temperature

Envirotemp 360 fluid can be pumped directly from storage tanks. If suction line lengths or suction lift heights are excessive, warming of the Envirotemp 360 fluid may be desired to reduce the viscosity. If heating of Envirotemp 360 fluid is required, the following systems are recommended:

A circulating pump and piping with a low watt density electric heater (in line) can be attached to the storage tank to maintain temperatures of 38°C (100°F) or higher (i.e., a 76 liter/min (20 GPM) pump with a 10 kW heater will maintain a temperature of 43°C (110°F) in a 19 m³ (5,000 gal) storage tank if heat losses to the environment are not excessive). The tank and piping should be insulated if ambient temperatures are low, to help minimize heating costs.

Tanks

Standard steel storage tanks conventionally used for transformer oil are satisfactory. Tanks should conform to local codes and standards. New tanks are preferred, should have at least one manhole, and should be protected from moisture by nitrogen blanketing. Before use, the inside of tanks should be sandblasted and primed with a coating compatible with synthetic ester fluid. Primers used for transformers' interiors are recommended. Existing storage tanks that have been used for conventional transformer oil can be used for Envirotemp 360 fluid if the following conditions are met:

- The tank is of proper capacity and the lines for filling and suction areadequate.
- The tank is thoroughly cleaned and inspected closely for any rusting condition or leakage.

Drum Handling Storage

- The Envirotemp 360 fluid-filled drums are sealed at the factory to protect against foreign material and moisture contamination during shipping. Seals over the bung plugs assure that the drum has not been opened.
- When drums of Envirotemp 360 fluid are to be stored, it is good practice to store them in a dry, temperature-controlled building. It is recommended the drum be stored horizontally with the bungs of the drum below the level of the fluid inside.
- A drip pan or basin is always recommended for drum storage.

CONTACT

Contact your sales representative for pricing and availability of the product

Europe (The Netherlands)

Cargill Bioindustrial
Evert van de Beekstraat 378
1118 CZ Schiphol
The Netherlands
+31 20 500 6695
EMEAenvirotemp@cargill.com

Europe (Turkey)

Cargill Bioindustrial Dilovası 5. Kimya Organize San.Bölgesi Çerkeşli Köyü Yolu, Dilovası, Kocaeli, Turkey Tel: +90 (262) 754 03 03 Faks: +90 (262) 754 03 10 -CIS-SalesTR@Cargill.com

www.envirotempfluids.com

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MATERIAL SAFETY DATA SHEET



1. Product and Company Identification

Material name

ENVIROTEMP FR3 FLUID

Version #

01

Issue date

06-13-2012

Revision date

-

Supersedes date

-

CAS#

Mixture

MSDS Number

12.55.1

Product use

Dielectric Coolant

Manufacturer/Supplier

Industrial Oils & Lubricants 9320 Excelsior Blvd. Hopkins, Minnesota 55343

US

IOLCustomerService@cargill.com

General Information:

1-800-842-3631

Emergency

Emergency Telephone: 1-800-424-9300

2. Hazards Identification

Physical state

Liquid.

Appearance

Green Liquid.

Emergency overview

CAUTION!

Prolonged or repeated skin contact may cause drying, cracking, or irritation.

OSHA regulatory status

This product is not hazardous according to OSHA 29CFR 1910.1200.

Potential health effects

Routes of exposure

Skin contact.

Eyes

Direct contact with eyes may cause temporary irritation.

Skin

Prolonged or repeated contact may cause itching, redness, and rash in some individuals.

Inhalation

Under normal conditions of intended use, this material is not expected to be an inhalation hazard.

Ingestion

No harmful effects expected in amounts likely to be ingested by accident.

3. Composition / Information on Ingredients

Components	CAS#	Percent	
Vegetable Oil	8001-22-7	> 98.5	

Composition comments

All concentrations are in percent by weight unless ingredient is a gas. Gas concentrations are in percent by volume.

4. First Aid Measures

First aid procedures

Eye contact

Any material that contacts the eye should be washed out immediately with water. If easy to do, remove contact lenses. Get medical attention promptly if symptoms occur after washing.

Skin contact

Wash skin with soap and water. Get medical attention promptly if symptoms occur after washing.

Inhalation

If symptomatic, move to fresh air. Get medical attention if symptoms persist.

Ingestion

First aid is normally not required. However, if greater than 1/2 liter (pint) ingested, seek medical

attention.

5. Fire Fighting Measures

Flammable properties

No unusual fire or explosion hazards noted.

 ENVIROTEMP FR3 FLUID
 CPH MSDS NA

 908795
 Version #: 01
 Revision date: - Issue date: 06-13-2012
 1 / 4

Extinguishing media

Suitable extinguishing

media

Water, Water fog. Foam. Dry chemical powder, Carbon dioxide (CO2).

Fire fighting

equipment/instructions

Self-contained breathing apparatus and full protective clothing must be worn in case of fire.

Hazardous combustion

products

Carbon oxides.

6. Accidental Release Measures

Personal precautions

Wear appropriate personal protective equipment (See Section 8).

Environmental precautions

Environmental manager must be informed of all major releases.

Methods for cleaning up

Absorb spill with vermiculite or other inert material, then place in a container for chemical waste.

Large Spills: Flush area with water. Prevent runoff from entering drains, sewers, or streams. Dike for later disposal.

7. Handling and Storage

Handling

Observe good industrial hygiene practices.

Storage

Keep container closed.

8. Exposure Controls / Personal Protection

Occupational exposure limits

No exposure limits noted for ingredient(s).

Engineering controls

Ensure adequate ventilation, especially in confined areas.

Personal protective equipment

Eye / face protection

Wear safety glasses with side shields (or goggles).

Skin protection

Wear chemical-resistant gloves, footwear and protective clothing appropriate for risk of exposure.

Contact glove manufacturer for specific information.

Respiratory protection

If engineering controls do not maintain airborne concentrations below recommended exposure limits (where applicable) or to an acceptable level (in countries where exposure limits have not been established), an approved respirator must be worn. Respirator type: Air-purifying respirator with an appropriate, government approved (where applicable), air-purifying filter, cartridge or

canister.

General hygiene considerations

Always observe good personal hygiene measures, such as washing after handling the material and before eating, drinking, and/or smoking. Routinely wash work clothing and protective

equipment to remove contaminants.

9. Physical & Chemical Properties

Appearance

Green Liquid.

Physical state

Liquid. Liquid.

Form Color

Green.

Odor

Mild.

Odor threshold

Not available.

pΗ

Neutral

Vapor pressure

< 0.01 mm Hg @ 20 °C

Vapor density

Not available.

Not Available

Boiling point

> 680 °F (> 360 °C)

Melting point/Freezing point Solubility (water)

Insoluble

Specific gravity

0.92

Flash point

590 - 608 °F (310 - 320 °C) Closed Cup

Flammability limits in air, upper, % by volume

Not Available.

Flammability limits in air,

Auto-ignition temperature

Not Available.

lower, % by volume

753.8 - 759.2 °F (401 - 404 °C)

ENVIROTEMP FR3 FLUID CPH MSDS NA

2/4

908795 Version #: 01 Revision date: - Issue date: 06-13-2012

VOC

< 0.001 g/I

Viscosity

33 - 35 mm²/s @ 40 °C

Other data

Decomposition temperature

Not Available.

10. Chemical Stability & Reactivity Information

Chemical stability

Material is stable under normal conditions.

Conditions to avoid

Excessive heat.

Incompatible materials

Strong oxidizing agents.

Hazardous decomposition

products

No hazardous decomposition products are known.

Possibility of hazardous

Hazardous polymerization does not occur.

reactions

11. Toxicological Information

Sensitization

No sensitizing effects known.

Acute effects

Prolonged or repeated skin contact may cause drying, cracking, or irritation.

Local effects

High mist concentrations may cause irritation of respiratory tract.

Carcinogenicity

This product is not considered to be a carcinogen by IARC, ACGIH, NTP, or OSHA.

Symptoms and target organs

Prolonged or repeated skin contact may cause drying, cracking, or irritation.

12. Ecological Information

Ecotoxicity

Not expected to be harmful to aquatic organisms.

Persistence and degradability

No data available. No data available.

Bioaccumulation / Accumulation

Mobility in environmental

media

No data available.

13. Disposal Considerations

Disposal instructions

Dispose of contents/container in accordance with local/regional/national/international regulations.

Waste from residues / unused

products

Dispose of in accordance with local regulations.

Contaminated packaging

Since emptied containers may retain product residue, follow label warnings even after container is emptied.

14. Transport Information

DOT

Not regulated as a hazardous material by DOT.

IATA

Not regulated as dangerous goods.

IMDG

Not regulated as dangerous goods.

TDG

Not regulated as dangerous goods.

15. Regulatory Information

US federal regulations

This product is not hazardous according to OSHA 29CFR 1910.1200.

All components are on the U.S. EPA TSCA Inventory List.

TSCA Section 12(b) Export Notification (40 CFR 707, Subpt. D)

Not regulated.

CERCLA (Superfund) reportable quantity (lbs) (40 CFR 302.4)

None

ENVIROTEMP FR3 FLUID CPH MSDS NA Superfund Amendments and Reauthorization Act of 1986 (SARA)

Hazard categories Immediate Hazard - No

Delayed Hazard - No Fire Hazard - No. Pressure Hazard - No. Reactivity Hazard - No

Section 302 extremely hazardous substance (40 CFR 355, Appendix A)

No

Section 311/312 (40 CFR

No

370)

Drug Enforcement

Not controlled

Administration (DEA) (21 CFR

1308.11-15) WHMIS status

Non-controlled

Inventory status

Country(s) or region

Inventory name

On inventory (yes/no)*

Canada

Domestic Substances List (DSL)

Yes

Canada

Non-Domestic Substances List (NDSL)

No

United States & Puerto Rico

Toxic Substances Control Act (TSCA) Inventory

Yes

4/4

*A "Yes" indicates this product complies with the inventory requirements administered by the governing country(s)

State regulations

This product does not contain a chemical known to the State of California to cause cancer, birth defects or other reproductive harm.

US - California Proposition 65 - Carcinogens & Reproductive Toxicity (CRT): Listed substance

US. Massachusetts RTK - Substance List

Vegetable Oil (CAS 8001-22-7)

Listed.

US. New Jersey Worker and Community Right-to-Know Act

Not regulated.

US. Pennsylvania RTK - Hazardous Substances

Vegetable Oil (CAS 8001-22-7)

Listed.

16. Other Information

Further information

HMIS® is a registered trade and service mark of the NPCA.

HMIS® ratings

Health: 1 Flammability: 1

Physical hazard: 0

NFPA ratings

Health: 1 Flammability: 1 Instability: 0

Disclaimer

To the best of our knowledge, the information contained herein is accurate. However, neither the

above named supplier nor any of its subsidiaries assumes any liability whatsoever for

completeness of the information contained herein. Final determination of suitability of any material is the sole responsibility of the user. All materials may present unknown hazards and should be used with caution. Although certain hazards are described herein, we cannot guarantee that these are the only hazards that exist.

CPH MSDS NA 908795 Version #: 01 Revision date: -Issue date: 06-13-2012



Engineering Solutions for Land & Structures

July 16, 2021

City of Haverhill Office of the Fire Chief City Hall, Room 113 4 Summer Street Haverhill, MA 01830

Attention: Lieutenant Michael Picard & Deputy Chief Eric Tarpy

Subject: 139 Amesbury Line Road Solar Project

Fire Lane Treatments

Dear Haverhill Fire Department:

On behalf of the project proponent, Solar Smart, LLC, and the property owner, Ted & Bernadette Xenakis, and in consultation with the abutting property owners Gerry Boucher (189 Amesbury Line Road) and Bill Pepe (199 Amesbury Line Road), GPR is requesting that the City of Haverhill Fire Department review the attached materials to then accept the following proposed fire lane treatments in accordance with Haverhill Zoning Ordinance Section 7.8.7.4.

The first of the proposed driveway from Amesbury Line Road is proposed according to the Solar Driveway Exhibit Plan cross section details prepared by GPR in the attachment to this letter.

After the first 235± feet, the proposed driveway will transition back to a standard gravel driveway.

The intention of the first 235± feet is to provide a stable, compacted driving surface for heavy vehicles that is closer to the appearance of an old country cart road.

The plastic cellular confinement grid product is manufactured by various companies, and the information contained within is from one such manufacturer, Invisible Structures, for a proprietary product named GrassPave2. This product has been chosen because of the research and documentation available demonstrating its strength and durability in a variety of applications. Other products, if determined to

Goldsmith, Prest & Ringwall, Inc.

be equivalent in strength, function and durability, may be substituted due to pricing or

The technical data provided demonstrates that the cellular confinement structure is suitable for heavy vehicular loads, and is also durable throughout yearly seasonal changes, and can be maintained year-round both by mowing and snow removal.

The addition of raised compacted gravel wheel path, with grass strips in between makes this sturdy driveway look more like an old cart path. This appearance is more pleasing to the abutters and is less likely to encourage errant cars from trying to use the driveway for recreational purposes. There are no recreational facilities down this driveway, so maintaining the appearance of a lazy cart path addresses a very specific security concern not to encourage unsolicited access on the driveway.

The first 235± feet of the driveway also happens to be perfectly straight, and with a longitudinal slope of less than 1%, approximately at 0.006 FT/FT slope. If any emergency or maintenance vehicle were to swerve off of the slight raised gravel wheel paths, the underlying structure provides a stable recovery and alternate driving area capable of supporting heavy vehicles.

We hope that this proposal for fire lane treatment meets with the acceptance and approval of the City of Haverhill Fire Department for life safety and emergency vehicle passage in accordance with the requirements of Haverhill Zoning Ordinance

If you have any questions or concerns about this proposal, please contact me at (978) 772-1590 and/or email kburchard@gpr-inc.com.

Sincerely,

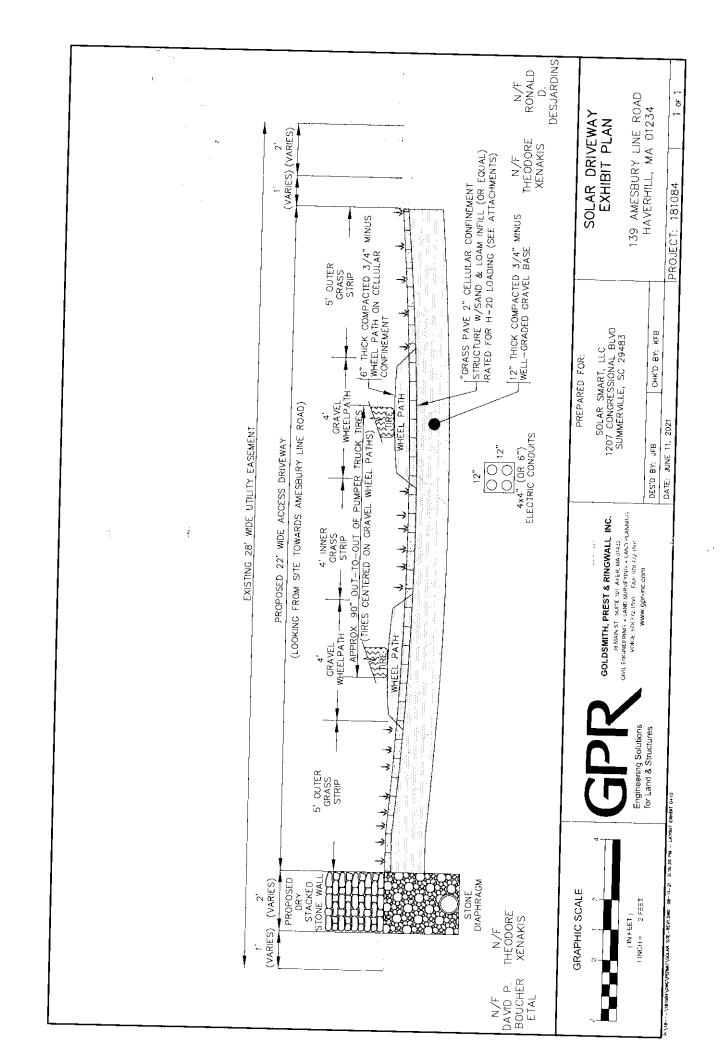
Goldsmith, Prest & Ringwall, Inc.

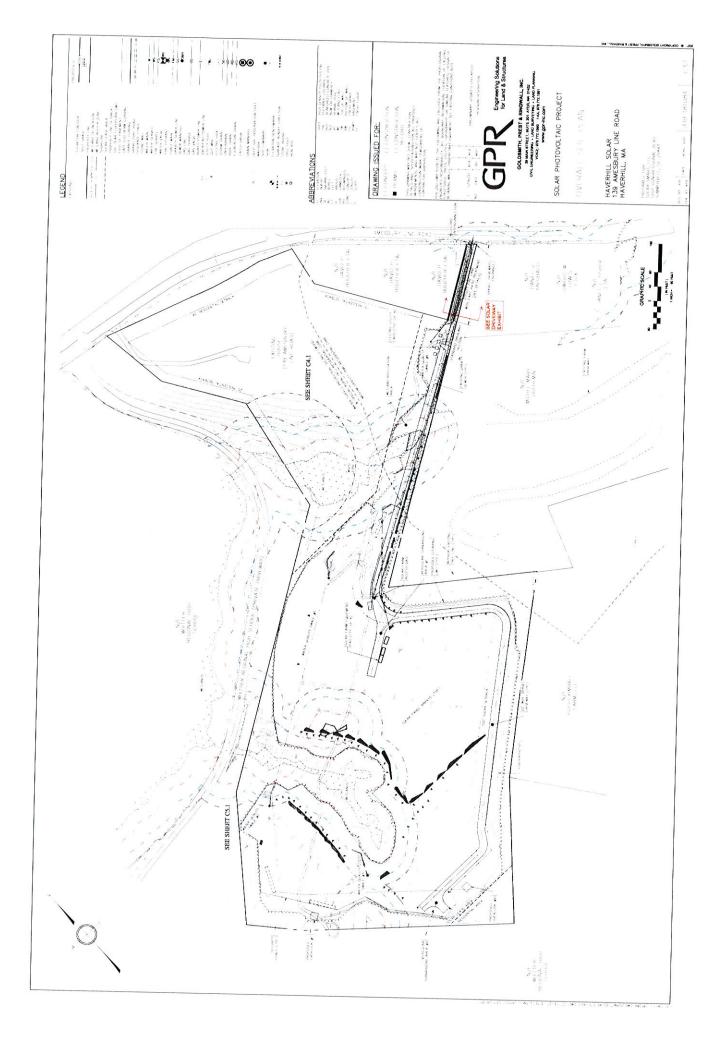
Kyle Burchard, P.E.

Project Manager

Copy to:

Owner, Client, GPR #181084 file







100% Grass Covered Porous Pavement

Grasspave2 Flexible Plastice Porous Pavement

Grasspave2 protects and enhances the environment in three ways: First, made from 100% recycled plastic, Grasspave2 keeps common consumer and industrial products from going into landfills. Second, grass paving directly improves the environment by recharging water tables on site (reducing flooding hazards downstream), reducing sources of oils and solvents from asphalt, absorbing carbon dioxide, and creating oxygen. Third, it enhances the beauty and quality of the built environment - replacing hot asphalt paved areas with cool, sparking green lawn-like Product Description

Grasspave2 has thin-walled independent plastic rings connected by an interlocking geogrid structure, which, because it is installed below the surface, is invisible in the completed project. While the rings are rigid, the grid itself is flexible, which makes it easy to install on uneven grades, and reduces usual cut and fill

The rings transfer loads from the surface to the grid structure and engineered base course material below, thus preventing compaction of the upper root zone of the grass. A single ring supports small loads, such as shoes; several rings support tires and large

The rings also act to contain the root zone medium (sand) and prevent lateral migration away from tires, feet, or other loads. This protects the grass root system, enabling roots to grow deep into the porous base course. The result is healthy, green turf at

One person can easily install the Grasspave2 rolls at a rate of 70m2 (750 ft2) per hour, plus time for base course preparation and grass installation (seeding, sod or sprigging). Step-by-step instructions are included in our Installation Instructions, which accompany each order.

Features and Benefits

- Allows 100% grass coverage instead of asphalt
- Made from 100% post consumer plastic
- High strength to weight load-bearing capacity
- Supports vehicular and pedestrian traffic

- Maximum porosity
- · Low to zero runoff
- Free air/water movement
- · Permits more trees
- Cooler site
- Greater oxygen
- Removes air pollutants
- Can preserve existing trees
- Helps to meet "Green Coverage Codes"
- Fast, low cost installation
- Competes in cost with asphalt paving
- No gutter and rain system needed
- No added land required for detention facilities
 - Lower life cycle costs

Applications

- Church/employee parking
- Overflow and event parking
- Golf cart paths
- · Residential driveways
- Firelanes

Specifications

Unit Size – 20"x 20"x 1" (50 x 50 x 2.5cm)

Unit Weight - 18oz (510 grams)

25 CM (9.8")

CM (6.6")

Sand fill

Hydrogrow

Grass, hydroseeded or sodded (thin)

Grasspave2 - 1 in, 2.5 cm

Sand and gravel base course - 6 in to 12 in

Compacted sub-grade

Strength - 15,940 psi (109,906 kPa)

Connector Pull Apart Strength (Tensile) - 458 lbf/in

Color - Black

Resin - 100% recycled HDPE with 3% carbon black

Shipped in Rolls (431 sq ft standard, other roll sizes available) 92% Void Space (8% plastic by volume)





Base Course Depth Recommendations GRASSPAVE2 and GRAVELPAVE2

10-12 in **CBR** >4 Infrequent Passes **CBR 2-4** 12 in Occassional Passes 12 in **CBR 2-4** 12-14 in 12-14 in CBR >4 Normal Traffic **CBR 2-4** 14 in Heavy Fire Truck & H-20 Loading

2-4 in 8 in 6 in 8-10 in 6-8 in 4-6 in 8-10 in 6-8 in 4-6 in 0-2 in 8-10 in 10 in 2-4 in e in 10-12 in 4-6 in 8 in 6 in 8-10 in 12 in 6-8 in 6 in Utility & Delivery Truck & H-10 Loading Light Fire Truck & H-15 Loading Cars & Pick-Up Truck Access Trail Use and Cart Paths Typical 85 psi 60,000 lb Typical 60 psi 40,000 lb Max 110 psi Typical 45 psi 80000 lb <1,000 lb 8,000 lb

* THESE DEPTH RECOMMENDATIONS SHOULD BE VERIFIED BY THE PROJECT ENGINEER AND LOCAL AUTHORITIES

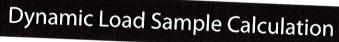
None

None





H-20 and HS-20 loading



Wheel load = W_L = 8000 lbs (32,000 lb axle / 4) Dynamic Force = F_d = 1.2 (20% greater than static force) Spread Area = A = 256 si (12" cover w/45 degree angle) Weight of base = d_y = 0.97 psi (12" road base @ 140 lbs/cf)

 $\sigma va = (W_L \times F_d / A) + d_V$

 $\sigma_{Va} = (8000 \text{ lbs x } 1.2 / 256 \text{ sqin}) + 0.97 \text{ lbs}$

 σva = 38.5 psi load results at top of RS3 Chamber

38.5 psi (256 kPa) on Rainstore3 Chamber with H-20/HS-20 Loads [47.8 psi (330 kPa with HS-25 Loads]

Rainstore3 has been independently field and laboratory tested to meet H-20 Bridge Loading.

Lab tests determine average Rainstore3 load capacity to be 93 psi at 2x safety factor.

Grasspave2, Gravelpave2, and Slopetame2 can withstand 15,940 psi with fill material (109,906 kPa) or 2.3 mil lbs/sq ft.

Surface Pressure

32,000 lb load for single rear axle

32,000 lbs / 4 tires per rear axle = 8000 lbs per tire

100 sqin = contact area (10" x 10")

 $8000 \, \text{lbs} / 100 \, \text{sq inches} = 80 \, \text{psi}$

80 psi (552 kPa) Static at Top of Cover



www.invisiblestructures.com 303-233-8383



Snow Removal from Grasspave²

Since 1982, most of our product sales have been to projects with secondary firelanes that cities required be kept free from depths of snow (usually 2 to 3" max) for emergency access. Over 1000 firelanes have been installed with our grass paver products - with at least half in regions subject to snowfall.

We have given all of the clients, contractors, and city agencies the same guidelines for removal of snow from our surfaces - <u>use skids</u> on the corners of snowplow blades.

Westfarms Mall in Farmington, Connecticut installed 6 acres of our Grasspave2 system for parking purposes, primarily used during the Christmas season. The grass looks beautiful after the first 3 years of use. They use skid rollers on dump truck mounted plows and have sustained no substantial damage due to plowing.

The idea to use skid plates was given to us by our very first client - the Snowmass Club, in Snowmass Colorado after they plowed snow 95 days during their first winter of 1982-83. Installed in October, days before snow fell, the 6,000 sf of 6 foot wide grass paved shoulders of the asphalt firelane/cart and pedestrian path had both horizontal and vertical curves in abundance.

Only 4% of the grass pavement was lost the first winter - and the plow did not have skids! They told us how to avoid damage in the future and suggest the skids to all future clients - which we have done. We never had additional requests for replacement product from the Snowmass Club again. Most of the pavement remains in place today except for areas lost to new tennis courts and pathways.

Another means to remove snow is the snowblower - most of which have a height adjustment capability to avoid direct blade contact with the surface. Tractor mounted brooms could be used with extreme care, but are not recommended as the potential for severe damage to the grass plant's crown is too high.

Please call us with any specific questions or concerns. Thank you.







BASE COURSE MATERIAL RECOMMENDATION

Sandy Gravel material from local sources commonly used for road base construction, passing sieve analysis:

Sieve % Passing

1"	100
3/4"	80 - 100
3/8"	60 - 80
#4	40 - 60
#10	25 - 40
#40	5 - 25
#200	0 - 5

Acceptable alternate base: AASHTO #57 stone mixed with clean, sharp sand (ASTM C-33) at a rate of 70% stone to 30% sand for full depth of base.

Make sure to avoid using materials such as recycled asphalt, limestone and decomposed granite, as they will cause problems with the porosity and/or pH levels.



Pioneering Stormwater Solutions

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Cold Weather Performance of Grasspave2 and Gravelpave2

Grasspave2 and Gravelpave2 have many advantages for use in cold climates over hard surface impermeable pavements, such as asphalt and concrete.

Porous Paving is more resistant to freezing. Damp underlying soils hold heat beneath the paved surface (Backstrom 2000). Porous pavement exhibits increased speed in thawing compared to conventional pavements, due to the ability of melted water to flow directly through the pavement, increasing the temperature in the cross-section (2003,

Grasspave2 and Gravelpave2 are made from flexible, High Density Polyethylene (HDPE) plastic with UV inhibitors, which withstands repeated freeze-thaw cycles and continuous subzero temperatures without cracking. HDPE resists aggressive chemicals such as road salts, motor oils and fuels. HDPE is highly abrasion-resistant and is unaffected by extremes in pH (Eastpoint Oltean Co & Plastic Pipe Institute).

The expansion and contraction of the HDPE in Grasspave2 and Gravelpave2 caused by temperature variations will not affect the performance of the systems. Flexibility in the snap fitting connectors and in the connecting grid, absorb the thermal expansion/contraction due to temperature fluctuations. Since, Grasspave2 and Gravelpave2 are only 6% plastic per volume (of the top 1.25" section), with a coefficient of expansion of 0.00007 [HDPE] (Eastpoint Oltean Co.), these products will not experience any noticeable expansion.

A proper base course material, 3/4 inch minus sandy gravel (25 to 35% void space), will also absorb much of the expansion due do temperature fluctuations, relieving most upward forces. Unlike concrete and asphalt, Grasspave2 and Gravelpave2 can flex and move with the remaining vertical forces imposed by expanding base course and subsoils. The flexible ring and grid structures were engineered to conform to natural undulations and variation in the site contours. This property also applies to shifting in the subsoils and base course due to freeze-thaw cycles.

Quicker thaw times and resistance to freezing, via porous paving, result in less de-icing chemicals and less plowing compared to impermeable hard surfaces. All season maintenance is also reduced with Grasspave2 and Gravelpave2.

In cold climates, Grasspave2 and Gravelpave2 have lifespans of 60 and 25 years, respectively, whereas impermeable asphalt and concrete have projected lifespans of 8 to

Backstrom M. 2000. "Ground Temperature in Porous Pavement during Freezing and Thawing." Journal of Transportation Engineering – ASCE 126(5) (September – October): 375-381.

Backstrom M, and Viklander M. 2000. "Integrated Stormwater Management in Cold Climates." Journal of Hazardous Substances & Environmental Engineering 35(8): 1237-1249.

Moser, Emily 2002, "Porous Pavements A Review of Literature," published by Penn State University "Thermal Expansion and Contraction in Plastics Piping Systems, PPI TR-21/2001" Plastic Pipe Institute. http://www.plasticsusa.com/hdpe.html, plasticsusa.com is published by Eastpoint Oltean Co http:// nemo.uconn.edu/reducing_runoff/questions.htm is published by the University of Connecticut



www.invisiblestructures.com

How to Incorporate Grasspave2 and Gravelpave2 into Your Runoff Calculations

Performing stormwater drainage design is one of the requirements of a site designer. Recent regulations created and enforced by the EPA require new developments to limit the amount of stormwater that flows off of a newly developed site, to be equivalent to or less, than the flow rate prior to development. The site designer must determine how much water is running off the original site, and compare this to the amount of water expected to flow off the newly developed site. Each site must have a drainage plan designed and certified by a Professional Engineer before construction can move forward.

The permeable nature of Porous Pavement is an attractive feature for the site designer because the Porous Pavement reduces the amount of stormwater runoff, and thus, reduces the amount of water that must be managed on-site. Designers often ask how to take the porous pavers Grasspave2 and/or Gravelpave2 into account when determining their runoff values.

Effective Percent Imperviousness

Porous Pavement, like Grasspave2 and Gravelpave2, is designed to allow stormwater to infiltrate back into the ground as opposed to impervious surfaces with the same function. Grasspave2 and Gravelpave2 reduce the Effective Imperviousness (I_A) of the developed site, thereby reducing the runoff and pollutant load off the site. Effective Imperviousness is defined as the combined effect of the proportion of constructed impervious surfaces to the catchment, and the connectivity of these impervious surfaces to receiving water bodies. Minimizing the Effective Imperviousness of the site helps to retain the post-development hydrology as close as possible to the pre-developed hydrology.

The Urban Drainage and Flood Control District has published a Drainage Criteria Manual (Vol.3) that discusses many Best Management Practices (BMPs) used industry wide to address handling stormwater on-site. Among the Structural BMPs detailed in this manual are Porous Pavements (PPs). This manual has an Effective Percent Imperviousness chart (see page 3) which details Porous Pavements and their use in different circumstances. The x-axis of this chart refers to the tributary area feeding the Porous Pavement area. The ratio of impervious tributary area to the area of Porous Pavement allows the designer to account for a site design where an impervious surface is designed to sheet flow onto a Porous Pavement. On the Chart, the bottom red line applies to all Porous Pavements, besides Porous Concrete Pavement – including Grasspave2 and Gravelpave2 – when site soils allow for infiltration. The green line refers to Grasspave2 (RGP = Reinforced Grass Pavement) used with underdrains or Porous Concrete Pavement with infiltration. The top blue line refers to all Porous Pavement types, besides Grasspave2 or Porous Concrete Pavement, when installed with underdrains. Use of underdrains would be necessary onsite if there are poor draining soils, or other drainage concerns. The on-site geotechnical engineer determines this.

Effective Imperviousness and the Rational Method

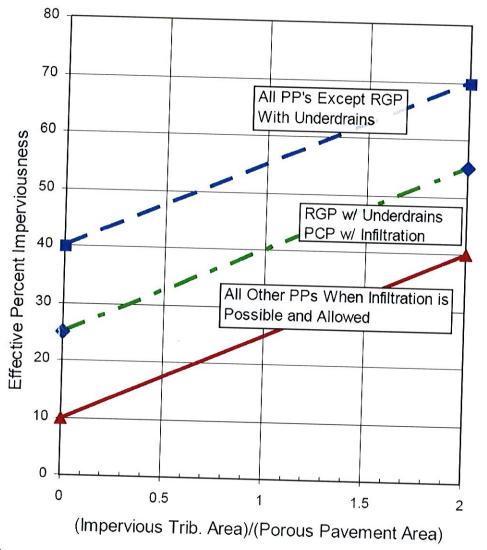
This chart provides critical information to the designer about how to incorporate the Porous Pavements Grasspave2 and Gravelpave2 into their runoff calculations. Effective Imperviousness directly correlates to the Runoff Coefficient used in the Rational Method. Both values measure the amount of expected runoff using a percentage approach. A Runoff Coefficient of 0.2 means 20% of the stormwater will runoff, while 80% will infiltrate into the ground. An Effective Imperviousness Percent of 20% translates identically. As such, the Urban Drainage chart tells that if there is no tributary area from adjacent impervious surfaces, and the site soils allow for infiltration. Gravelpave2 and Grasspave2 have an Effective Imperviousness of 10%. This equates to a Runoff Coefficient of 0.10. This value (depending on the source of the Runoff Chart) is representative of a lawn area.

Effective Imperviousness and TR-55

Effective Imperviousness also translates into the Curve Numbers used in National Resource Conservation Society's TR-55 hydrology calculation method. As demonstrated above, if there is no tributary stormwater load from adjacent impervious areas, and site soils allow water to infiltrate back into the ground, both Grasspave2 and Gravelpave2 can be considered to have a pervious nature similar to lawns, or open space in good condition. The designer can then select the appropriate Curve Number according to the site's Hydrologic Soil Group from TR-55's Table 2-2a - Open Space in Good Condition. An alternative method for determining the appropriate Curve Number would be to create a composite Curve Number. The composite Curve Number should be computed using TR-55's Figures 2-3 or 2-4 based on the Effective Impervious Area percentage (with CN = 98) given in the Urban Drainage chart and the pervious area Curve Number assuming Open Space in Good Condition.

Conclusion

The use of the Effective Percent Imperviousness Chart developed by Urban Drainage and Flood Control District allows the designer to appropriately incorporate Grasspave2 and/or Gravelpave2 into their drainage plan. Both products have been shown to have a similar runoff profiles as open spaced areas in good hydrological condition. This allows the designer to select the appropriate Runoff Coefficient or Curve Number for their hydrologic soil group, slope, and design storm. Each site has its own special needs and circumstances. As always, the designer should be aware of the assumptions and limitation of both methods, and as such, should use his or her good judgment regarding the applicability of the above values. The chart and tables included in this paper are not intended to replace reasonable and prudent engineering judgment that should permeate each step in the design process.



Notes:

- Chart applies only to porous pavements described in Volume 3 of the USDCM, Structural MBPs chapter. Not to be used for other types of porous pavements.
- Apply the "Effective Percent Imperviousness" to the total area that included the area of porous pavement and the tributary impervious area that can be made to flows uniformly onto PP.
- Use no more than two units of impervious area for each unit of PP. All impervious areas exceeding this ratio shall be treated as 100% impervious in hydrologic calculations, including runoff volumes.
- Whenever impervious areas cannot be made to run onto the pervious areas in a uniform sheet-flow fashion, identify individual areas and what ratios apply to each and then composite them reating each as a separate area.

Figure PP-1—Interim Recommended Effective Percent Imperviousness for Porous Pavements (Based on the Ratio of the Impervious Area Tributary to Porous Pavement)

References:

Rational Method:

Runoff Coefficients for Rational Formula:

United States Department of Transportation

Federal Highway Administration

"Urban Drainage Design Manual - HEC 22" - November 1996

"Table 3-1. Runoff Coefficients for Rational Formula"

http://www.fhwa.dot.gov/engineering/hydraulics/pubs/hec/hec22.pdf

Runoff Coefficients for the Rational Formula versus Hydrologic Soil Group (A, B, C, D) and Slope Range:

McCuen, R. Hydrologic Analysis and Design – 3rd Edition http://www.bossintl.com/download/RunoffCoefficients.html

TR-55:

Table 2-2a from TR-55, Runoff Curve Numbers for Urban Areas

United States Department of Agriculture

Natural Resources Conservation Service

Conservation Engineering Division

"Urban Hydrology for Small Watersheds: Technical Release 55" – June 1996

http://www.cpesc.org/reference_tr55.pdf

Effective Imperviousness Chart:

Urban Drainage and Flood Control District

"Urban Storm Drainage Criteria Manual Volume III" - 2008 latest revision Section 04 – Structural BMP

http://www.udfcd.org/downloads/down_critmanual_volIII.htm



Invisible Structures, Inc. 303-233-8383 www.invisiblestructures.com

Grasspave2 Product Specification (CSI Format)

Notes: This product guide specification is written according to the Construction Specifications Institute (CSI) Format, including MasterFormat (1995 Edition). SectionFormat, and PageFormat, contained in the CSI Manual of Practice.

The section must be carefully reviewed and edited by the Engineer to meet the requirements of the project and local building code. Coordinate with other specification sections and the drawings.

Delete all "Specifier Notes" when editing this section.

SECTION 32 12 43 POROUS FLEXIBLE PAVING (Formerly 02795 Porous Paving)

Notes: This section covers Grasspave2 Porous Pavement System from Invisible Structures. The system provides vehicular and heavy load support over grass areas while protecting grass roots from harmful effects of traffic.

The major components of the complete system are the Grasspave2 units, an engineered base course, Hydrogrow soil amendment/fertilizer, sand, and grass from seed, hydromulch, or sod.

Consult Invisible Structures, Inc. for assistance in editing this section for the specific application.

PART 1 **GENERAL**

1.1 SECTION INCLUDES

A. Porous pavement system.

1.2 **RELATED SECTIONS**

В.	Section [31 20 00 – Earth Moving] []. Section [33 46 00 – Subdrainage] []. Section [32 10 00 – Bases, Ballasts, and Paving] [].
Notes: pavem	Edit the following list as required for the project. List other sections with work directly related to the porous lent system.
D.	Section [32 30 00 - Site Improvements] [
E.	Section [32 90 00 Planting] [].
F.	Section [32 92 00 – Manufacturers of Turfs and Grasses] [
G.	Section [32 80 00 – Irrigation or Section 32 84 13 – Drip Irrigation] [

1.3 REFERENCES

- A. ASTM F 1951-08 Standard Specification for Determination of Accessibility of Surface Systems Under and
- B. ASTM D 638-10 Standard Test Method for Tensile Properties of Plastics
- C. ASTM C 33 Standard Specification for Concrete Aggregates
- D. AASHTO M6 Standard Specification for Fine Aggregate for Hydraulic Cement Concrete

1.4 SYSTEM DESCRIPTION

- A. The Grasspave2 porous pavement system provides vehicular and pedestrian load support for grass areas, while protecting grass roots from harmful effects of traffic.
- B. Major Components of the Complete System
 - 1. Grasspave2 units, assembled in rolls.
 - 2. Engineered sand and gravel base course.
 - 3. Hydrogrow soil amendment and fertilizer, supplied with Grasspave2.
 - 4. Sand fill or USGA greens mix.
 - 5. Selected grass from seed, hydroseeding/hydro-mulching, or sod.
 - 6. Selected topsoil (only for seeded installation).
 - Mulch (needed only for seeded or hydroseeded installations).
- C. The Grasspave2 grass paving units, sand, and base course work together to support imposed loading.
- D. The Grasspave2 grass paving units, Hydrogrow, and sand fill contribute to vegetation support.

1.5 SUBMITTALS

- A. Submit under provisions of Section 01 30 00.
- B. Shop Drawings: Submit design detail showing proper cross-section.
- C. Samples: Submit manufacturer's sample of Grasspave2 10" x 10" section of Grasspave2 material.
- D. Installation Instructions: Manufacturer's printed installation instructions. Include methods for maintaining
- E. Certificates:
 - 1. Manufacturer signed certificate stating the product is made in the USA.
 - 2. Submit Material Certificates for base course and sand (or USGA mix) fill materials
 - 3. Product certificates signed by the manufacturer certifying material compliance of polyethylene used to make Grasspave2 units.
 - 4. ISO Certificate certifying manufacturer's quality management system is currently registered to ISO 9001:2008 quality standards.
- F. LEED Submittals: Provide documentation of how the requirements of Credit will be met:
 - 1. List of proposed materials with recycled content. Indicate post-consumer recycled content and preconsumer recycled content for each product having recycled content.
 - 2. Product data and certification letter indicating percentages by weight of post-consumer and preconsumer recycled content for products having recycled content.
 - 3. Description of Grasspave2 in stormwater design to limit the disruption of natural hydrology by reducing impervious cover, increasing on-site infiltration, reducing or eliminating pollution from stormwater runoff and eliminating contaminants.
 - 4. Designing elements for Grasspave2 to limit the disruption and pollution of natural water flows by managing stormwater runoff.
 - 5. Documenting the use of Grasspave2 to reduce heat islands to minimize the impact on

microclimates and human and wildlife habitats.

- G. Substitutions: No material will be considered as an equivalent to the Grasspave2 unit specified herein unless it meets all areas of this specification without exception. Manufacturers seeking to supply what they represent as equivalent material must submit records, data, independent test results, samples, certifications, and documentation deemed necessary by the Specifier to prove equivalency.
- H. Manufacturer's Material Certification: Product manufacturers shall provide certification of compliance with all applicable testing procedures and related specifications upon written request. Request for certification shall be submitted by the purchasing agency no later than the date of order placement.
- I. Product manufacturers shall also have a minimum of 30 years' experience producing products for porous
- J. Manufacturer Quality Certification: ISO Certification certifying manufacturer's quality management system for its Grasspave2 system is currently registered to ISO 9001:2008 quality standards. Any alternate materials submitted shall provide a certification that their porous pavement system manufacturing process is part of an ISO program and a certification will be required specifically stating that their testing facility is certified and in accordance with ISO.

DELIVERY, STORAGE, AND HANDLING 1.6

- A. Store products in manufacturer's unopened packaging until ready for installation.
- B. Protect Grasspave2 units/rolls from damage during delivery and store rolls upright, under tarp, to protect from sunlight, when time for delivery to installation exceeds one week.
- C. Store Hydrogrow in a dark and dry location
- D. Handling: Protect materials during handling and installation to prevent damage

1.7 MAINTENANCE SERVICE

Notes: Once healthy turf has been established, the cell wall structure maintenance practices are followed.	cture will have minimal visibility when proper turf
A Installer regnerable (

A.	Installer responsible for maintenance of
	Installer responsible for maintenance of grass plants – water/irrigation, fertilizing, mowing – for one growing season. DO NOT AFRATE, See Grasspace 3 Maintenance of grasspace 3 Maintenance 3 Maint
В.	growing season. DO NOT AERATE. See <i>Grasspave2 Maintenance Guide</i> from Invisible Structures

В.	System to be maintained by	The state of the s
		, after one growing season

1.8 **Project Conditions**

- A. Maintain environmental conditions within limits recommended by manufacturer for optimum results. Do not install products under environmental conditions outside manufacturer's absolute limits.
- B. Do not begin installation of porous pavements until all hard surface paving adjacent to porous pavement areas, including concrete walks and asphalt paving, is completed.
- C. Install turf when ambient air temperatures is at least 55 degrees F (13 degrees C).
- D. In cold weather, do not use frozen materials or materials mixed or coated with ice or frost, and do not build on frozen base or wet, saturated or muddy subgrade.
- E. Protect partially completed paving against damage from other construction traffic when work is in
- F. Adequately water sod or grass seed to assure germination of seed and growth of root system.
- G. Grass coverage on the sand-filled Grasspave2 rings must be completed within one week: See Part 3
- H. DO NOT DRIVE, PARK ON, or use Grasspave2 system for two or three mowing cycles until grass root system has matured (about 3 to 4 weeks for sod or 6 to 8 weeks for seeded areas). Any barricades constructed must still be accessible by emergency and fire equipment during and after installation.

1.9 LIMITED WARRANTY

- A. Invisible Structures, Inc. (ISI) warrants to its purchasers that all products furnished by ISI will be free from
- B. This warranty shall be extended for a period of five (5) years following the date of shipment by ISI.
- C. Providing a written claim is presented to ISI within the warranty period and after inspection by ISI showing the materials have failed under this warranty, all defective materials shall be refurnished under this warranty, at no charge, excluding re-installation costs. This in lieu of all other warranties expressed or implied and is the sole warranty extended by ISI.
- D. Our liability under this warranty is limited to the refurnishing of materials and does not include any responsibility for incidental, consequential, or other damages of any nature.

PART 2 **PRODUCTS**

2.1 **MANUFACTURERS**

- A. Acceptable Manufacturer: Invisible Structures, Inc., which is located at: 3510 Himalaya Rd. Suite 200; Aurora, CO 80011; Tel: 303-233-8383; Web: www.invisiblestructures.com.
- B. Substitutions: Not permitted.

2.2 **GRASSPAVE2**

- A. Composition:
 - 1. Manufactured in the USA.
 - High density polyethylene (HDPE): 100 percent recycled materials. 2.
 - 3. Color: black
 - Color Uniformity: Uniform color throughout all units rolls. 4.
 - Carbon Black for ultraviolet light stabilization. 5.
 - Hydrogrow soil amendment and fertilizer, provided by manufacturer with Grasspave2. 6.
- B. Performance Properties:
 - Maximum Loading Capability: 15,940 psi (2.29 million psf, 109,906 kPa) when filled with sand.
 - Wheelchair Access testing for ADA Compliance: Passing ASTM F 1951-08. 3.
 - Wheelchair Access testing for ADA Compliance: Passing Rotational Penetrometer testing.
 - Tensile strength, pull-apart testing: 458 lbf/in from ASTM D638 Modified. 4. 5.
 - System Permeability (Grasspave2, sand, base course): 2.63 to 38.55 inches of water per hour. Effective Imperviousness (E.I.): 10%.
- C. Dimensions (individual units are assembled and distributed into rolls):
 - Roll area: From 108 sq ft (10 sq m) to 538 sq ft (50 sq m), in 108 sq ft (10 sq m) increments 2.
 - Roll Widths: From 3.3 ft (1 m) to 8.2 ft (2.5 m), in 1.6 ft (0.5 m) increments. 3.
 - Roll Lengths: From 32.8 ft (10m) to 65.6 ft (20 m), in 3.3 ft (1 m) increments. 4.
 - Roll Weights: From 41 lbs (19kg) to 205 lbs (93kg), in 41 lbs (19 kg) increments.
 - Unit Nominal Width by Length: 20 inches by 20 inches (0.5 m by 0.5 m) or 40 inches by 40 inches
 - Nominal Depth: 1 inch (2.5 cm) for rolls and individual units. 6.
 - Unit Weight: 18 oz (510 g) or 5 lbs. (2.27 kg). 7.
 - Volume Solid: 8 percent.

2.3 SYSTEM MATERIALS

Notes: All measurements are subject to manufacturing tolerances, unless otherwise specified. A. Base Course: Sandy gravel material from local sources commonly used for road base construction (recycled materials such as crushed concrete or crushed asphalt are NOT acceptable). Conforming to the following sieve analysis and requirements: 100 percent passing sieve size 1 inch (25 mm). 80-100 percent passing sieve size 3/4 inch (19 mm). b. 60-80 percent passing sieve size 3/8 inch (9 mm). C. 40-60 percent passing sieve size #4. đ. 25-40 percent passing sieve size #10. e. f. 5-25 percent passing sieve size #40. 0-5 percent passing sieve size #200. g. Provide a base course material nearly neutral in pH (range from 6.5 to 7.2) to provide adequate root zone development for turf. Material may be either "pit run" or "crusher run." Avoid using clay based crusher run/pit run. Crusher run material will generally require coarse, well-draining sand conforming to AASHTO M6 or ASTM C 33 to be added to mixture (20 to 30 percent by volume) to ensure long-term porosity. Alternative materials such as crushed shell, limerock, or crushed lava may be used for base course use, provided they are mixed with sharp sand (20 to 30 percent) to ensure long-term porosity, and are brought to proper compaction. Without added sand, crushed shell and limerock set up like concrete and become impervious. Alternative size and/or composition of base course materials should be submitted to Invisible Structures, Inc. (Manufacturer) for approval. B. Sand Fill for Rings and Spaces Between Rings: Clean sharp sand (washed concrete sand). Choose one Coarse, well-draining sand, such as washed concrete sand conforming to AASHTO M6 or ASTM United States Golf Association (USGA) greens, section - sand mix "The Root Zone Mixture." C. Turf Conditioner: Hydrogrow a proprietary soil amendment manufactured by Invisible Structures, Inc. and provided with Grasspave2. 2. NO SUBSTITUTIONS. Notes: Use grass species resistant to wear by traffic generally a Blue/Rye/Fescue mix used for athletic fields in northern climates, and Zoysia, Fescue, or Bermuda types in southern climates. Check with local sod and seed suppliers for preferred mixtures. Dedicated fire lanes can use same grass species used on surrounding turf. Parking applications require greatest wear-resistant species possible, generally available only by seed or hydroseeding/hydro-mulching. D. Grass - Choose either sod or seed: __]. Use 13 mm (0.5") thick (soil thickness) rolled sod from a reputable local grower. Species should be wear resistant, free from disease, and in excellent condition. Sod shall be

- grown in sand or sandy loam soils only. Sod grown in soils of clay, silt, or high organic materials such as 2. Seed: [_]. Use seed materials, of the preferred species for local environmental and projected traffic conditions, from certified sources. Seed shall be provided in containers clearly labeled to show seed name, lot number, net weight, % weed seed content, and guaranteed % of purity and germination. Pure Live Seed types and amount shall be as shown on
 - Mulch needed only for hydroseeding: Wood or paper cellulose commercial mulch materials compatible with hydroseeding operations. Mulch depth according to mulch

- manufacturers' recommendation. DO NOT use mulch of straw, pine needles, etc., because of their low moisture holding capacity.
- b. Topsoil needed only for seeding, recommended for hydroseeding: Obtain specified topsoil for a light "dusting" (no more than ½" or 13mm) above rings filled with sand for seeding germination.

PART 3 EXECUTION

3.1 INSPECTION

- A. Examine subgrade and base course installed conditions. Do not start porous paving installation until unsatisfactory conditions are corrected. Check for improperly compacted trenches, debris, and improper gradients.
- B. For fire lane installations: prior to installing base course for turf paving, obtain approval of local fire authorities of sub-base.
- C. Start of installation constitutes acceptance of existing conditions and responsibility for satisfactory performance. If existing conditions are found unsatisfactory, contact Architect for resolution.

3.2 PREPARATION

Notes: Ensure that subbase materials are structurally adequate to receive designed base course, wearing course, and designed loads. Generally, excavation into undisturbed normal strength soils will require no additional modification. Fill soils and otherwise structurally weak soils may require modifications, such as geotextiles, geogrids, and/or compaction (not to exceed 90%). Ensure that grading and soil porosity of the subbase will provide adequate subsurface drainage

A. Subgrade Preparation:

- Prepare subgrade as specified in Section 32 10 00. Verify subgrade in accordance with porous paving system manufacturer's instructions.
- 2. Proper subgrade preparation will enable the Grasspave2 rolls/units to connect properly and remain

Notes: For Fire lanes and emergency access. It is recommended that Fire Department inspectors be scheduled to inspect installation of Grasspave2 during preparation of the subbase, installation of the base course, and installation of Grasspave2 units. Most small projects can accommodate these inspections all on the same day. Verify with Fire Department if certificates of inspection are required.

level and stationary after installation.

- 3. Excavate area allowing for unit thickness, the engineered base depth (where required), and 0.5 inch (1.25 cm) for depth of sod root zone or topsoil germination area (when applicable).
- 4. Provide adequate drainage from excavated area if area has potential to collect water, when working with in-place soils that have poor permeability.
- 5. Ensure in-place soil is relatively dry and free from standing water.
- 6. Uniformly grade base.
- Level and clear base of large objects, such as rocks and pieces of wood.

B. Base Preparation:

- Install Base as specified in Section 32 10 00. Verify engineered base (if required) is installed in accordance with porous paving system manufacturer's instructions.
- Coordinate base installation and preparation with subdrains specified in Section 33 46 00.
- 3. If required, place a geotextile separation layer between the natural ground and the 'engineered base'.
- 4. If required, install the specified sub-drain and outlet according to construction drawings.
- 5. Coordinate base installation and preparation with irrigation and drip irrigation lines specified in Section 32 80 00 and 32 84 13, respectively.
- 6. Place engineered base in lifts not to exceed 6 inches (150 mm), compacting each lift separately to

- 95 percent Modified Proctor.
- 7. Leave 1 inch (2.5 cm) of depth below final grade for porous paver unit and sand fill and 0.5 inch (1.25 cm) for depth of sod root zone or topsoil germination area (when applicable).

Notes: Delete requirement for on-site manufacturer's field representative if not required

3.3 ON-SITE MANUFACTURER'S FIELD REPRESENTATIVE

- A. A qualified Manufacturer's field representative shall be available for a pre-construction meeting via phone or in person and will provide installation videos, design details, installation instructions, and the technical specifications.
- B. The time for on-site observation shall be indicated in the Contract Documents and included in the base bid price.

3.4 HYDROGROW INSTALLATION

- A. Spread all Hydrogrow mix provided (spreader rate = 4.53 kg per 100 m2 (10 lbs per 1076 ft2) evenly over the surface of the base course with a hand-held, or wheeled, rotary spreader.
- B. The Hydrogrow mix should be placed immediately before installing the Grasspave2.

3.5 GRASSPAVE2 INSTALLATION

- A. Install the Grasspave2 units by placing units with rings facing up, and using snap-fit connectors, pegs and holes, provided to maintain proper spacing and interlock the units. Units can be easily shaped with pruning shears or knife. Units placed on curves, slopes, and high traffic areas shall be anchored to the base course, using 40d common nails with fender washer, as required to secure units in place. Tops of rings shall be between 6 mm to 13 mm (0.25" to 0.5") below the surface of adjacent hard-surface
- B. Install sand in rings as they are laid in sections by "back-dumping" directly from a dump truck, or from buckets mounted on tractors, which then exit the site by driving over rings already filled with sand. The sand is then spread laterally from the pile using flat bottomed shovels and/or wide "asphalt rakes" to fill the rings. A stiff bristled broom should be used for final "finishing" of the sand. The sand must be "compacted" by using water from hose, irrigation heads, or rainfall, with the finish grade no less than the top of rings and no more than 6 mm (0.25") above top of rings.

3.6 INSTALLATION OF GRASS

A. Grass coverage on the sand-filled rings must be completed within one week. Sand must be re-installed and leveled and Grasspave2 checked for integrity if rings become exposed due to wind, rain, traffic, or other factors. (Choose one paragraph below to meet grass installation method desired.)

Notes: Choose one paragraph below to match grass installation method

- 1. Preferred method: Hydroseeding/hydro-mulching A combination of water, seed and fertilizer are homogeneously mixed in a purpose-built, truck-mounted tank. The seed mixture is sprayed onto the site at rates shown on plans and per hydroseeding manufacturer's recommendations. Coverage must be uniform and complete. Following germination of the seed, areas lacking germination larger than 20 cm x 20 cm (8" x 8") must be reseeded immediately. Seeded areas must be fertilized and kept moist during development of the turf plants.). DO NOT DRIVE ON SYSTEM: Hydroseeded/hydro-mulch areas must be protected from any traffic, other than emergency vehicles, for a period of 6 to 8 weeks, or until the root system has penetrated and established well below the Grasspave2 units.
- 2. Install thin sod directly over sand filled rings, filled no higher than the top of the rings. Sod strips should be placed with very tight joints. Sodded areas must be fertilized and kept moist during root

- establishment (minimum of 3 weeks). DO NOT DRIVE ON SYSTEM: Sodded areas must be protected from any traffic, other than emergency vehicles, for a period of 3 to 4 weeks, or until the root system has penetrated and established well below the Grasspave2 units.
- Install grass seed at rates per grass type. A light "dusting" of commercial topsoil mix, not to exceed 1/2" (25 mm) will be placed above the rings and seed mix to aid germination rates. Seeded areas must be fertilized and kept moist during development of the turf plants.). DO NOT DRIVE ON SYSTEM: Seeded areas must be protected from any traffic, other than emergency vehicles, for a period of 6 to 8 weeks, or until the root system has penetrated and established well below the
- B. Adequately water sod or grass seed to assure germination of seed and growth of root system.

3.7 **PROTECTION**

Notes: Choose one paragraph below to match grass installation method.

- A. Seeded areas must be protected from any traffic, other than emergency vehicles, for a period of 4 to 8 weeks, or until the grass is mature to handle traffic.
- B. Sodded areas must be protected from any traffic, other than emergency vehicles, for a period of 3 to 4 weeks, or until the root system has penetrated below the Grasspave2 units.

3.8 FIELD QUALITY CONTROL

- A. Remove and replace segments of Grasspave2 units where three or more adjacent rings are broken or damaged, reinstalling as specified, so no evidence of replacement is apparent.
- B. Perform cleaning during the installation of work and upon completion of the work. Remove all excess materials, debris, and equipment from site. Repair any damage to adjacent materials and surfaces resulting from installation of this work.

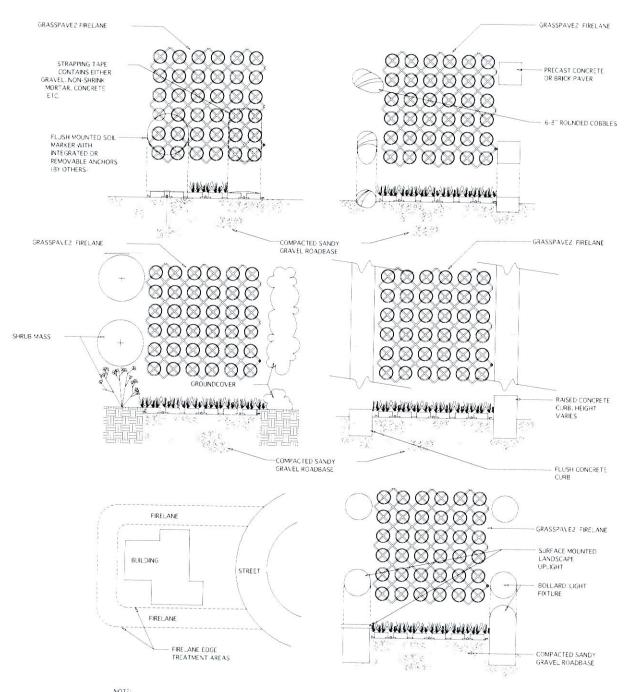
3.9 MAINTENANCE

- A. Maintain grass in accordance with manufacturer's instructions and as specified in Section 32 92 00 Manufacturers of Turfs and Grasses.
- B. Lawn Care: Normal turf care procedures should be followed, including de-thatching.
- C. DO NOT AERATE. Aerator will damage the Grasspave2 units. Aeration in not necessary in a sand root
- D. When snow removal is required, keep a metal edged plow blade a minimum of ¾ inch (17 mm) above the surface during plowing operations to avoid causing damage to the Grasspave2 units, or
 - Use a plow blade with a flexible rubber edge, or
 - Use a plow blade with skids on the lower outside corners set so the plow blade does not come in 2.

END OF SECTION

GRASSPAVE2 Firelane Detail

Use this detail for delineating a Grasspave2 firelane

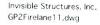


NOTE:: THIS DETAIL IS SCHEMATIC IN NATURE: DESIGNER SHALL SPECIFY SPACING AND DESIGN OF EDGE TREATMENTS. SPACING WILL VARY WITH TURE TYPE, SLOPE, FIRE DEPARTMENT REQUIREMENTS. ETC.

NOT TO SCALE











INSTALLATION GUIDE - Grasspave2 Porous Grass Pavement

Introduction

A. This document describes step-by-step information on how to properly install the Grasspave2 Porous Pavement System. Grasspave2 provides vehicular and pedestrian load support for grass areas, while protecting grass roots from harmful effects of traffic. The major components of the complete system are the Grasspave2 units, an engineered base course, Hydrogrow soil amendment/fertilizer, sand, and grass from seed, hydromulch, or sod.

- B. **Contractors**: Only licensed contractors should install the Grasspave2 system. The contractor should have a good performance record with similar construction projects. *Homeowners should only attempt installation after they have read and understood fully this installation guide and/or our Technical Specifications.*
- C. **Landscaping:** Plant a grass species in Grasspave2 that 1) is climate appropriate, 2) will receive the necessary maintenance for the species (irrigation and fertilizer support), 3) is wear resistant to hold up to vehicular traffic, 4) can be grown in a sand-based root zone, 5) is shade tolerant (if applicable).
- F. Warning: Unless there is an emergency, DO NOT DRIVE, PARK ON, or use Grasspave2 system for two or three mowing cycles until grass root system has matured (about 3 to 4 weeks for sod or 6 to 8 weeks for seeded areas). Any barricades constructed to prevent traffic flow must still be accessible by emergency and fire equipment during and after installation.
- G. Warranty: Invisible Structures, Inc. (ISI) warrants to its purchasers that all products furnished by ISI will be free from defects in material and/or workmanship. This warranty shall be extended for a period of five (5) years following the date of shipment by ISI. Providing a written claim is presented to ISI within the warranty period and after inspection by ISI showing the materials have failed under this warranty, all defective materials shall be refurnished under this warranty, at no charge, excluding re-installation costs. This in lieu of all other warranties expressed or implied and is the sole warranty extended by ISI. Our liability under this warranty is limited to the refurnishing of materials and does not include any responsibility for incidental, consequential, or other damages of any nature.

Delivery, Storage, and Handling

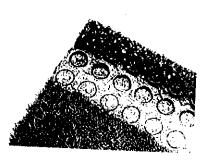
- A. Store products in manufacturer's unopened packaging until ready for installation.
- B. Protect Grasspave2 units/rolls from damage during delivery and store rolls upright (like a soda can), and under a tarp to protect from sunlight when time for delivery to installation exceeds one week. Do not store rolls on their sides.
- C. Store Hydrogrow in a dark and dry location.
- D. Handling: Protect materials during handling and installation to prevent damage.

Installation Considerations

- A. Review installation procedures and coordinate Grasspave2 work with other work affected. Generally, Grasspave2 is installed at the same time as project grass installation, nearly the last site construction activity.
- B. Do not begin installation of porous pavements until all hard surface paving adjacent to porous pavement areas, including concrete walks and asphalt paving, is completed.
- C. Install turf when ambient air temperatures is at least 55 degrees F (13 degrees C).
- D. In cold weather, do not use frozen materials or materials mixed or coated with ice or frost, and do not build on frozen base or wet, saturated or muddy subgrade.
- E. Protect partially completed paving against damage from other construction traffic when
- F. Adequately water sod or grass seed to assure germination of seed and growth of root
- G. Grass coverage on the sand-filled Grasspave2 rings must be completed within one week.
- H. DO NOT DRIVE, PARK ON, or use Grasspave2 system for two or three mowing cycles until grass root system has matured (about 3 to 4 weeks for sod or 6 to 8 weeks for seeded areas). Any barricades constructed must still be accessible by emergency and fire equipment

Materials

- A. Grasspave2 Porous Paving Rolls
- B. Base Course: Sandy gravel material from local sources commonly used for road base construction (recycled materials such as crushed concrete or crushed aggregate are NOT acceptable).
 - 1. Conforming to the following sieve analysis and requirements:
 - 100 percent passing sieve size 1 inch (25 mm).
 - 80-100 percent passing sieve size 3/4 inch (19 mm). 60-80 percent passing sieve size 3/8 inch (9 mm).
 - 40-60 percent passing sieve size #4.
 - 25-40 percent passing sieve size #10.
 - 5-25 percent passing sieve size #40.
 - 0-5 percent passing sieve size #200.
 - 2. Provide a base course material nearly neutral in pH (range from 6.5 to 7.2) to provide adequate root zone development for turf.
 - 3. Material may be either "pit run" or "crusher run." Avoid using clay based crusher run/pit run. Crusher run material will generally require coarse, well-draining sand conforming to AASHTO M6 or ASTM C 33 to be added to mixture (20 to 30 percent by volume) to ensure long-term porosity.
- 4. Alternative materials such as crushed shell, limerock, or crushed lava may be used for base course use, provided they are mixed with sharp sand (20 to 30 percent by volume) to ensure long-term porosity, and are brought to proper compaction. Without added sand, crushed shell and limerock set up like concrete and become impervious.
- 5. Alternative size and/or composition of base course materials should be submitted to Invisible Structures, Inc. (Manufacturer) for approval.



- C. Sand Fill for Rings and Spaces Between Rings: Clean sharp sand (washed concrete sand). Choose one of the following:
 - 1. Coarse, well-draining sand, such as washed concrete sand conforming to AASHTO M6 or ASTM C-33.
 - 2. United States Golf Association (USGA) greens, section sand mix "The Root Zone Mixture."

D. Turf Conditioner:

- 1. Hydrogrow a proprietary soil amendment manufactured by Invisible Structures, Inc. and provided with Grasspave2.
- 2. NO SUBSTITUTIONS.
- E. Grass Choose either sod or seed. Use grass species resistant to wear by traffic generally a Blue/Rye/Fescue mix used for athletic fields in northern climates, and Zoysia, Fescue, or Bermuda types in southern climates. Check with local sod and seed suppliers for preferred mixtures. Dedicated fire lanes can use same grass species used on surrounding turf. Parking applications require greatest wear-resistant species possible, generally available only by seed or hydroseeding/hydro-mulching.
 - 1. Sod: Use 13 mm (0.5") thick (soil thickness) rolled sod from a reputable local grower. Species should be wear resistant, free from disease, and in excellent condition. Sod shall be grown in sand or sandy loam soils only. Sod grown in soils of clay, silt. or high organic materials such as peat, will not be accepted.
 - 2. Seed: Use seed materials, of the preferred species for local environmental and projected traffic conditions, from certified sources. Seed shall be provided in containers clearly labeled to show seed name, lot number, net weight, % weed seed content, and guaranteed % of purity and germination. Pure Live Seed types and amount shall be as shown on plans.
 - a. Mulch needed only for hydroseeding: Wood or paper cellulose commercial mulch materials compatible with hydrosceding operations. Mulch depth according to mulch manufacturers' recommendation. DO NOT use mulch of straw, pine needles, etc., because of their low moisture holding capacity.
 - b. Topsoil needed only for seeding, recommended for hydroseeding: Obtain specified topsoil for a light "dusting" (NO MORE than 1/2" or 13mm) above rings filled with sand for seeding germination.
- F. Fertilizer: A commercial "starter" fertilizer, with Guaranteed Analysis of 17-23-6, or as recommended by local grass supplier, for rapid germination and root development.
- G. Grasspave2 Sign: A sign to identify the presence of Grasspave2 paving, stating that special maintenance is required, with the Manufacturer's phone number, and made of durable materials for outdoor exposure shall be provided and installed.
- H. Fire lane Signage & Delineation: Fire lanes must be identified regarding their entrance and physical location with the placement of signs, gates, curbs, bollards, etc. Specific signage wording and other details must be coordinated with and approved by local fire authorities.

INSTALLATION

Inspection

(For Fire lanes and emergency access, It is recommended that Fire Department inspectors be scheduled to inspect installation of Grasspave2 during preparation of the subbase, installation of the base course, and installation of Grasspave2 units. Most small projects can accommodate these inspections all on the same day. Verify with Fire Department if certificates of inspection are required.)

- A. Examine subgrade and base course installed conditions. Do not start porous paving installation until unsatisfactory conditions are corrected. Check for improperly compacted trenches, debris, and improper gradients.
- B. For fire lane installations: prior to installing base course for turf paving, obtain approval of local fire authorities of sub-base.
- C. Start of installation constitutes acceptance of existing conditions and responsibility for satisfactory performance. If existing conditions are found unsatisfactory, contact Architect

Preparation

(Ensure that subbase materials are structurally adequate to receive designed base course, wearing course, and designed loads. Generally, excavation into undisturbed normal strength soils will require no additional modification. Fill soils and otherwise structurally weak soils may require modifications, such as geotextiles, geogrids, and/or compaction (not to exceed 90%). Ensure that grading and soil porosity of the subbase will provide adequate subsurface drainage)

A. Subgrade Preparation:

1. Prepare subgrade as specified for project.

2. Proper subgrade preparation will enable the Grasspave2 rolls/units to connect properly and remain level and stationary after installation.

3. Excavate area allowing for unit thickness (1 in), the engineered base depth (where required), and 0.5 inch (1.25 cm) for depth of sod root zone or topsoil germination area (when applicable).

4. Provide adequate drainage from excavated area if area has potential to collect water, when working with in-place soils that have poor permeability.

5. Ensure in-place soil is relatively dry and free from standing water.

6. Uniformly grade base.

7. Level and clear base of large objects, such as rocks and pieces of wood.

B. Base Preparation:

1. Install Base as specified.

2. Coordinate base installation and preparation with subdrains (if necessary).

3. If required, place a geotextile separation layer between the natural ground and the 'engineered base'.

4. If required, install the specified sub-drain and outlet according to construction drawings.

5. Coordinate base installation and preparation with irrigation and drip irrigation lines.

6. Place engineered base in lifts not to exceed 6 inches (150 mm), compacting each lift separately to 95 percent Modified Proctor.

7. Leave 1 inch (2.5 cm) of depth below final grade for porous paver unit and sand fill and 0.5 inch (1.25 cm) for depth of sod root zone or topsoil germination area (when applicable).

Hydrogrow Installation

A. Spread all Hydrogrow mix provided (spreader rate = 4.53kg per 100 m2 (10 lbs per 1076 ft2) evenly over the surface of the base course with a hand-held, or wheeled, rotary spreader.





B. The Hydrogrow mix should be placed immediately before installing the Grasspave2.

Grasspave2 Unit Installation

A. Install the Grasspave2 units by placing units with rings facing up, and using snap-fit connectors, pegs and holes, provided to maintain proper spacing and interlock the units. Units can be easily shaped with pruning shears or knife. Units placed on curves, slopes, and high traffic areas shall be anchored to the base course, using 40d common nails with fender washer, as required to secure units in place. Tops of rings shall be between 6 mm to 13 mm (0.25" to 0.5") below the surface of adjacent hard-surface pavements.



B. Install sand in rings as they are laid in sections by "backdumping" directly from a dump truck, or from buckets mounted on tractors, which then exit the site by driving over rings already filled with sand. The sand is then spread laterally from the pile using flat bottomed shovels and/or wide "asphalt rakes" to fill the rings. A stiff bristled broom should be used for final "finishing" of the sand. The sand must be "compacted" by using water from hose, irrigation heads, or rainfall, with the finish grade no less than the top of rings and no more than 6 mm (0.25") above top of rings.

Installation of Grass

A. Grass coverage on the sand-filled rings must be completed within one week. Sand must be re-installed and leveled and Grasspave2 checked for integrity if rings become exposed due to wind, rain, traffic, or other factors.

Notes: Choose one paragraph below to match grass installation method

1. Preferred method: Hydroseeding/hydro-mulching - A combination of water, seed and fertilizer are homogeneously mixed in a purpose-built, truck-mounted tank. The seed mixture is sprayed onto the site at rates shown on plans and per hydroseeding manufacturer's recommendations. Coverage must be uniform and complete. Following germination of the seed, areas lacking germination larger than 20 cm x 20 cm (8" x 8") must be reseeded immediately. Seeded areas must be fertilized and kept moist during development of the turf plants.). DO NOT DRIVE ON SYSTEM: Hydrosceded/hydromulch areas must be protected from any traffic, other than emergency vehicles, for a period of 6 to 8 weeks, or until the root system has penetrated and established well below the Grasspave2 units.

OR

2. Install thin sod directly over sand filled rings, filled no higher than the top of the rings. Sod strips should be placed with very tight joints. Sodded areas must be fertilized and kept moist during root establishment (minimum of 3 weeks). DO NOT DRIVE ON SYSTEM: Sodded areas must be protected from any traffic, other than emergency vehicles, for a period of 3 to 4 weeks, or until the root system has penetrated and established well below the Grasspave2 units.

3. Install grass seed at rates per grass type. A light "dusting" of commercial topsoil mix, not to exceed 1/2" (25 mm) will be placed above the rings and seed mix to aid germination rates. Seeded areas must be fertilized and kept moist during development of the turf plants). DO NOT DRIVE ON SYSTEM: Seeded areas must be protected from any traffic, other than emergency vehicles, for a period of 6 to 8 weeks, or until the root system has penetrated and established well below the Grasspave2 units.

B. Adequately water sod or grass seed to assure germination of seed and growth of root system.

Protection

Choose one paragraph below to match grass installation method.

- A. Seeded areas must be protected from any traffic, other than emergency vehicles, for a period of 4 to 8 weeks, or until the grass is mature to handle traffic.
- B. Sodded areas must be protected from any traffic, other than emergency vehicles, for a period of 3 to 4 weeks, or until the root system has penetrated below the Grasspave2 units.



Field Quality Control

- A. Remove and replace segments of Grasspave2 units where three or more adjacent rings are broken or damaged, reinstalling as specified, so no evidence of replacement is apparent.
- B. Perform cleaning during the installation of work and upon completion of the work. Remove all excess materials, debris, and equipment from site. Repair any damage to adjacent materials and surfaces resulting from installation of this work.



Invisible Structures, Inc. 303.233.8383 www.invisibelstructures.com

Porosity, Permeability and Infiltration

Permeability – the rate at which a fluid flows through a porous substance under given conditions.

Porosity (void space) – the portion of a volume of material that is not solid

Infiltration – movement of a fluid into the surface of a porous substance.

Infiltration and Permeability are used interchangeably in reference materials

The Permeability (infiltration) of Grasspave2

Sand permeability = 8.27 inches/hour

Grass in Sand root zone= 9 to 25 inches per hour (various USGA mixes)

Base course poor draining = 2.63 inches/hour* (sandstone with 10% fines) Base course common = 7.37 inches /hour* (limestone with 3% fines)

Base course mixed = 38.55 inches /hour***** (66% GP and 33% GW) Subsoils need to infiltrate at least 0.5 in/hr to be considered permeable**

Our system would deliver 2.63 to 38.55 inches of water per hour to the subsoils.

The Permeability (infiltration) of Gravelpave2

Open graded aggregate, 1/4" = 2500 inches/hour***

0.1" to .2" inside open-celled grids = 40+ inches per hour****

Base course poor draining = 2.63 inches/hour* (sandstone with 10% fines)

Base course common = 7.37 inches /hour* (limestone with 3% fines)

Base course mixed = 38.55 inches /hour***** (66% GP and 33% GW)

Subsoils need to infiltrate at least 0.5 in/hr to be considered permeable** and recommended soils would be loam, sandy loam, or loamy sand.

Our system would 2.63 to 38.55 inches of water per hour to the subsoils

The Porosity (void space) and Water Storage of Grasspave2

13 inch cross-section

One inch Grasspave2 with Sand = 20% void

12 inches base course = 20% void (16%-and-up depending on composition)

13 inches x approx. 20% void space =

2.6 cubic inches of Water Storage

The Porosity (void space) and Water Storage of Gravelpave2

13 inch cross-section

One inch of Gravelpave2 with Open Graded Aggregate at $3/16^{\circ} - 3/8^{\circ} = 35\%$

12 inches base course = 20% void (16-35% depending on composition)

(One inch x 35%) + (12 inches at 20%) =

2.75 cubic inches of Water Storage

GW = Well graded, clean gravels, gravel/sand mixtures GP = Poorly graded, clean gravels, gravel sand mixtures

All rates are approximate and actual installed rates will vary depending on local materials and other conditions.

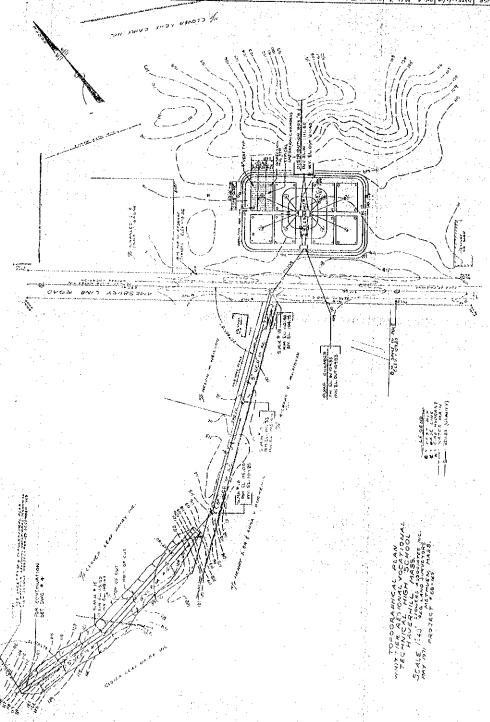
If existing site soils infiltration rates are below .5 in hr (silt loam, sandy clay loam, clay loam, silty clay loam, sandy clay, silty clay, or clay), additional drainage is recommended below Grasspave2 and Gravelpave2.

- *Permeability of Pavement Base Course, SAM I. THORNTON & CHIN LEONG TOH, Civil Engineering Department, University of Arkansas, May 1995
- **Guidelines set by the EPA
- ***AASHTO, 1993, p I-19, extracted from page 144. Porous Pavement, Bruce Ferguson, Taylor and Francis, 2005.
- **** Pratt et al 1995 extracted from page 144, Porous Pavement, Bruce Ferguson, Taylor and Francis, 2005.
- ***** Data from "Civil Engineering Design Manual", 1995

Soil Permeability Rates Data from "Civil Engineering Design Manual", 1995.

Description	Well graded, clean gravels, gravel/sand mixtures	Poorly graded, clean gravels, gravel/sand mixtures	Well graded, clean sands, gravely sands	poorly graded, clean sands, sand/gravel mix
Rate in/hr	226.77	56.69	2.27	2.27
Rate cm/sec Rate in/min Rate in/hr Description	3.78	0.94	0.04	0.04
Rate cm/sec	0.16	0.04	0.0016	0.0016
Coeff cm/sec	2.5 EE -2	5 EE -2	5 EE -4	5 EE -4
Soil Type Coeff	CW	GP	SW	SP

Best base course for GP2 and GV2 would be mix of 2/3GP and 1/3GW
Rate cm/sec Rate in/min Rate in/hr
0.0272 0.64 38.55







ILLUSTRATIVE VIEW FROM EAST EDUCATION PLATFORM



ILLUSTRATIVE VIEW ENTERING MAIN GATE

SOLAR PHOTOVOLTAIC PROJECT

HAVERHILL SOLAR 139 AMESBURY LINE ROAD HAVERHILL, MA

SITE PLAN

HAVERHILL SOLAR PROJECT

HAVERHILL, MA

REGULATORY NOTES

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SITE DATA

LOT AREA. OPEN SPACE. SOLAR LEASE AREA.

268±AC (1,167,844 S.F.) 93%± 18.6±AC (810,801 S.F.)

GENERAL NOTES

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430-11-12

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SITE

VICINITY MAP SCALE: 1" = 600"

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BY WHITEN SOUGH.

DRAMING ISSUED FOR:
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SPECIAL PENALT TO CITY COUNCIL FOR CONSTRUCTION OF LANCE-SCALE CROUND-WOUNTED SOUNT DICKEY SYSTEM

ASSESSORS REFERENCE ASSESSORS MAP 430, BLOCK 11, LOI

SUBMITTALS

S DRAWNG MAY NOT SHOW CONSTRUCTION
ALE AND SPECIFICATIONS FOR ALL PROPOSED
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ELEVATION DATUM

SHEET INDEX
C1.1 TITLE SHEET
C1.1 TITLE SHEET
C2.1 STATING CONDITIONS
C3.1 OVERALL SITE PLAN
C3.2 RESOLNGE IMPACT MAP
C3.2 RESOLNGE IMPACT MAP
C3.2 RESOLNGE IMPACT MAP
C3.4 RESOLNGE IMPACT MAP
C3.4 RESOLNGE IMPACT MAP
C3.4 RESOLNGE PLAN
C4.1 SITE PLAN
C4.1 SITE PLAN
C4.1 SITE PLAN
C5.2 DRIVEWAY PLAN & PROFILE (14-00 TO 74-00)
C5.2 DRIVEWAY PLAN & RROFILE (14-00 TO 24-83)
C6.3 CONSTRUCTION DETAILS
C6.2 CONSTRUCTION DETAILS
C6.3 CONSTRUCTION DETAILS
C6.4 WETLAND REPLICATION PLAN
C6.4 WETLAND REPLICATION PLAN



CASCAGNI

ZONING

	-	2	SCHOOL PLANT (169-00-764) & medium density (re
fay Demot	212 & Zonny Map	CodSM	WSPD (Water Supply Protection Dates) 9.2.7
cosed Use	7.8.3	Allowed by SPGA RS / RM	Large-Scale Ground-Mounted Solar Energy Sys
Arms	Appendix 6-Table 2	87,120	1.6784.5
tage	Appendix B-Table 2		7555
Depth	Appendix B-Table 2		1800 FT
	Appendix B-Table 2	95	Use Sour Demensions
	Appendix B-Table 2	40 FT / 25 FT / 100 FT	100 FT (7 8 6-1 a.)
	Appendix B-Table 2	74 677 15 FT/ 100 FT	100 FT (7 & 6-1 b.)
	Appendix 8-Table 2	73671786717867	100 87 (7 8 6-1 c.)
ang Height	Appendix 8-Table 2	387738	N.A
mum Stories	Appendix B-Table 2	25/25	NA
ang Coerage	Appendix B-Table 2	16%/25%	N.Y
r Area Ratio	Appendix B-Table 2	None	NA
Spece (MIN.)	Appendix B-Table 2	70 11 145 14	45 85 K
2	93.15	500 (800	
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SYE/

MEGETATED WETLAND (TYP.)

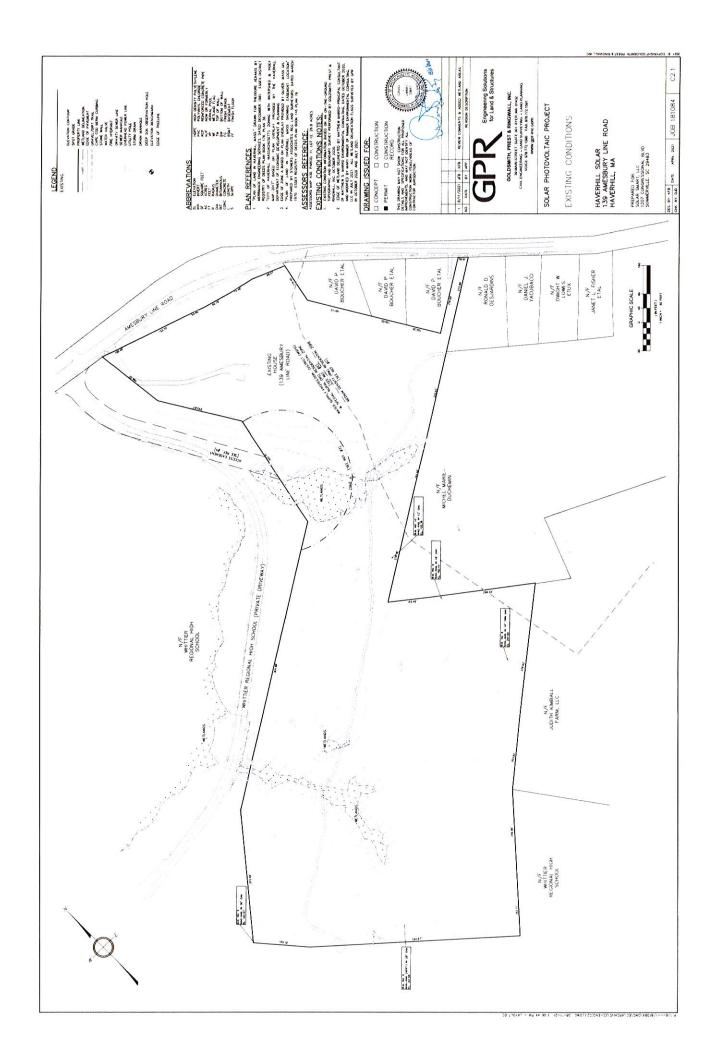
Engineering Solutions for Land & Structures

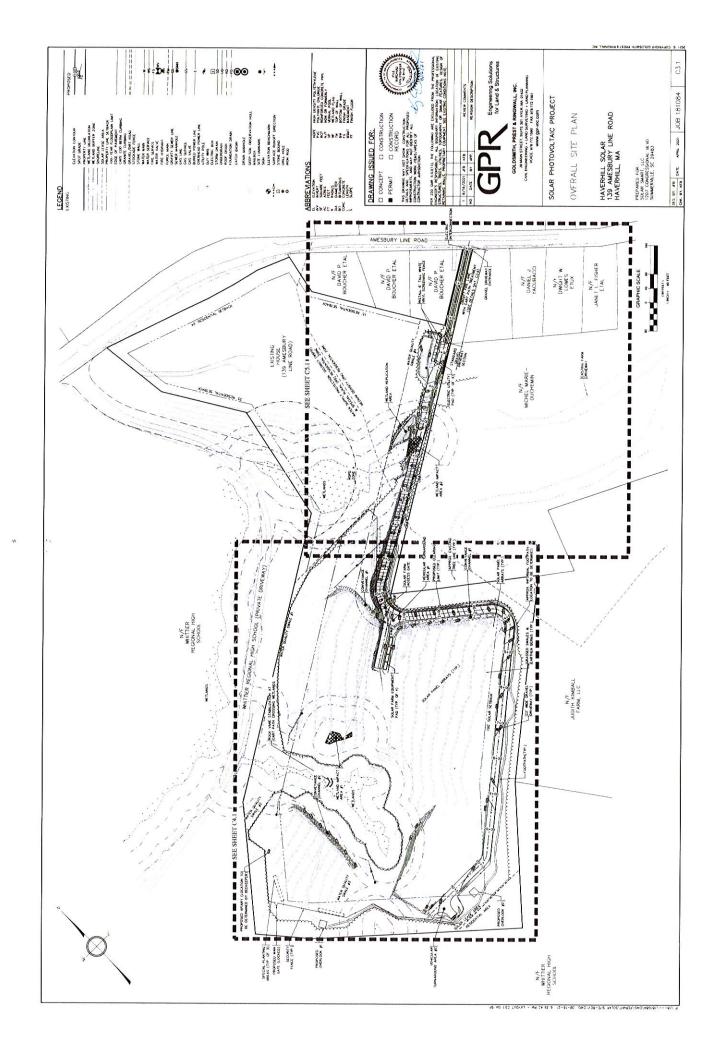
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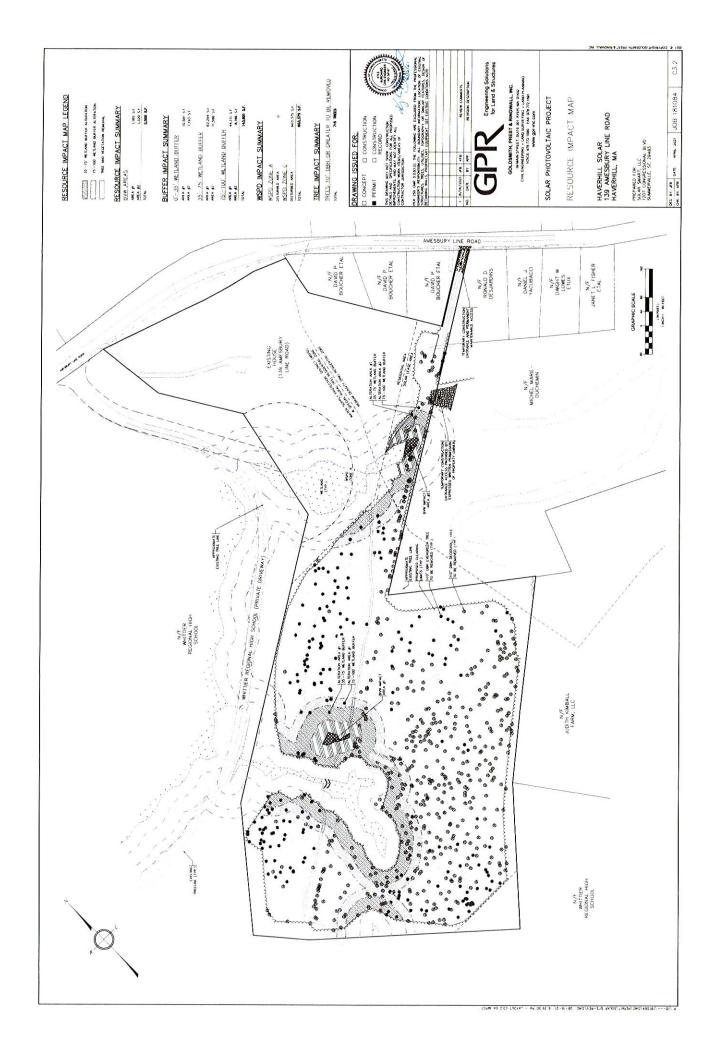


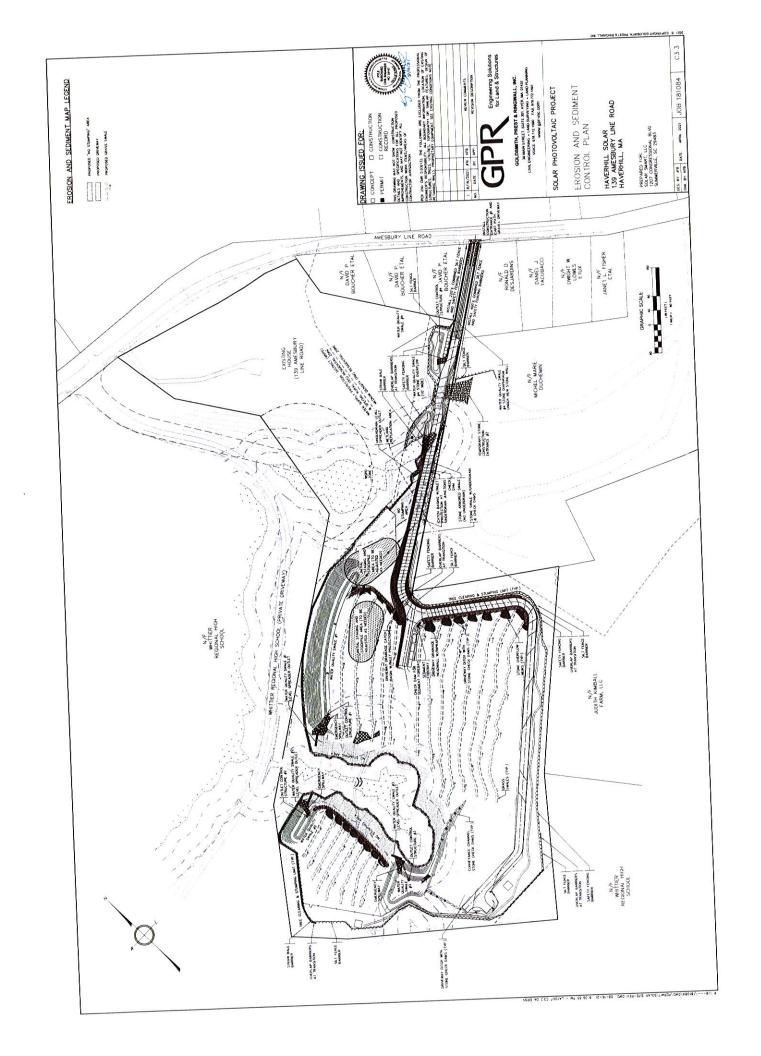
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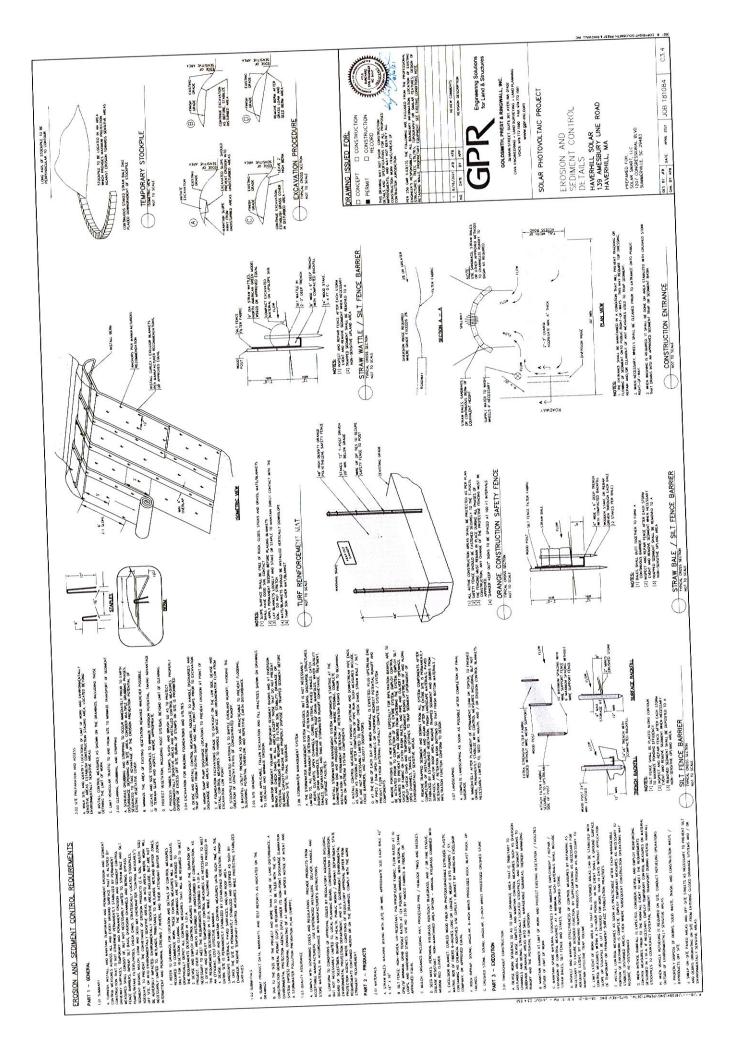
OVERALL MAP & ZONING SCALE: 1" = 250"

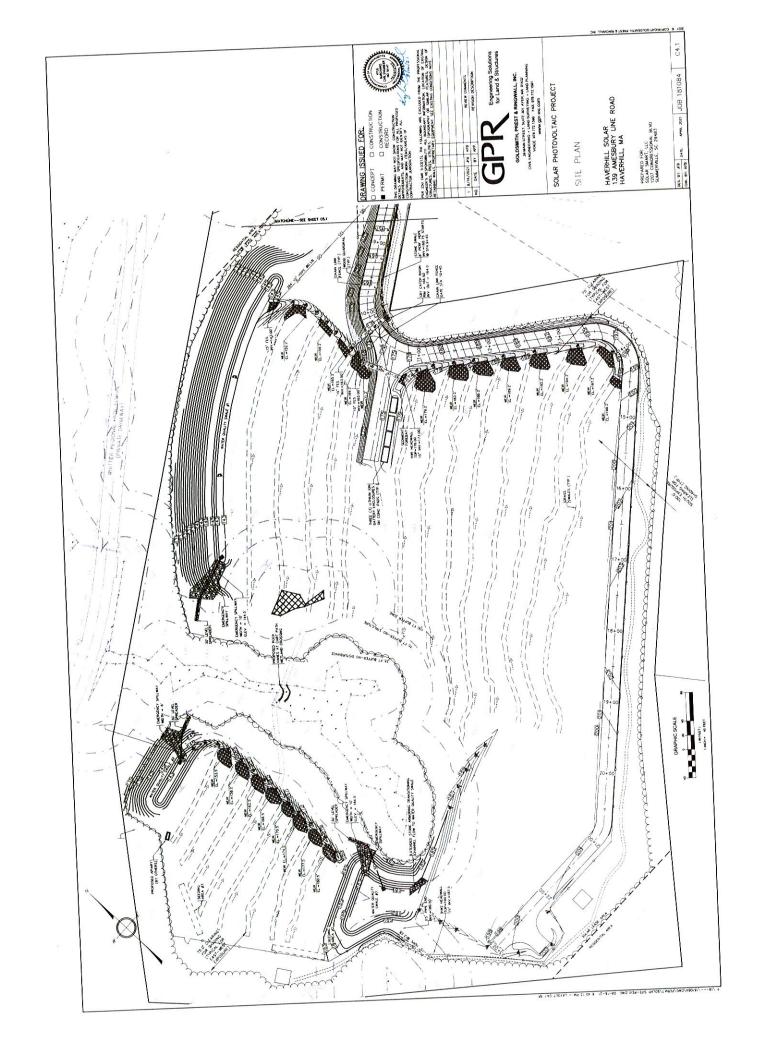


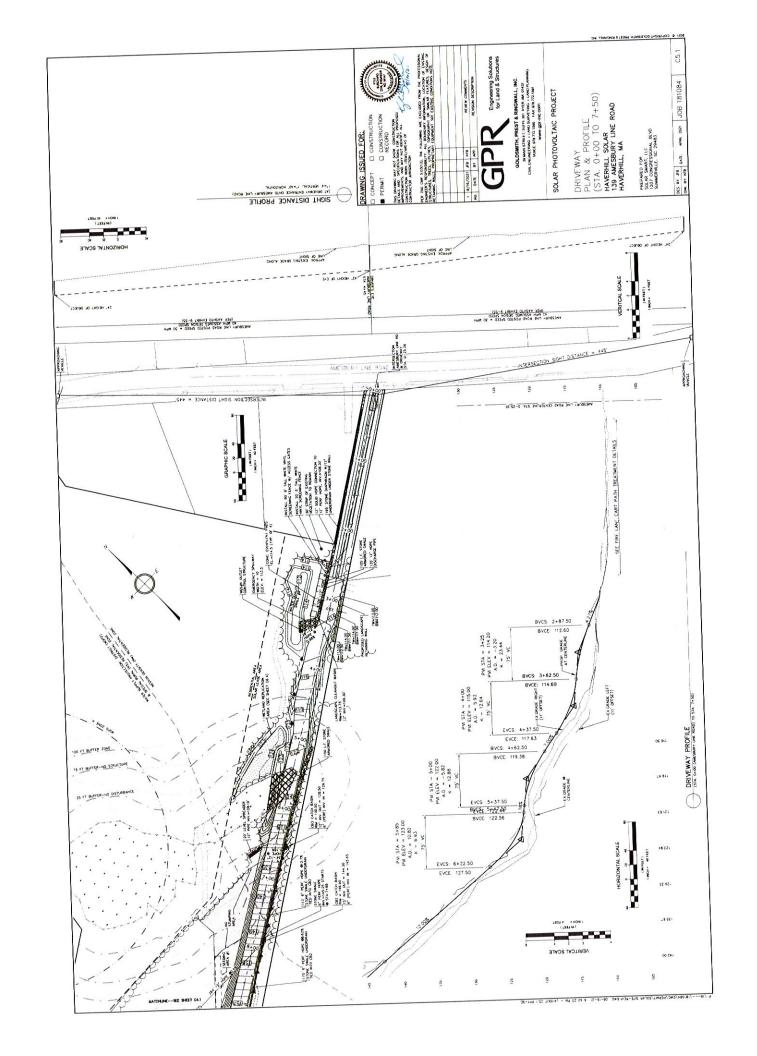


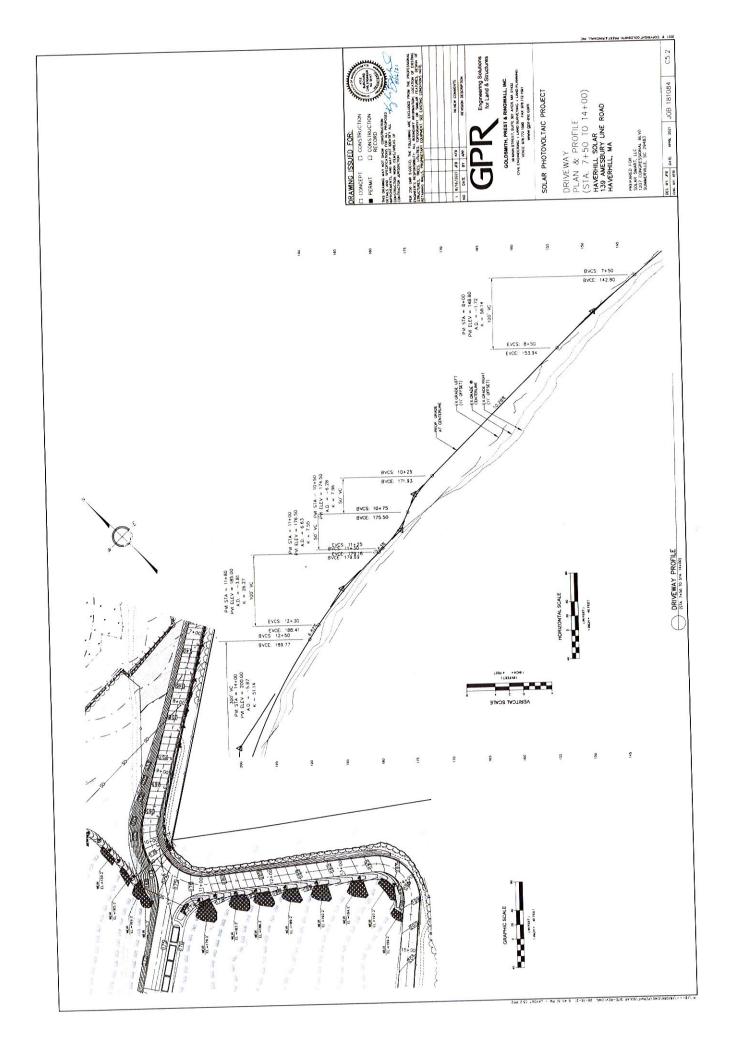


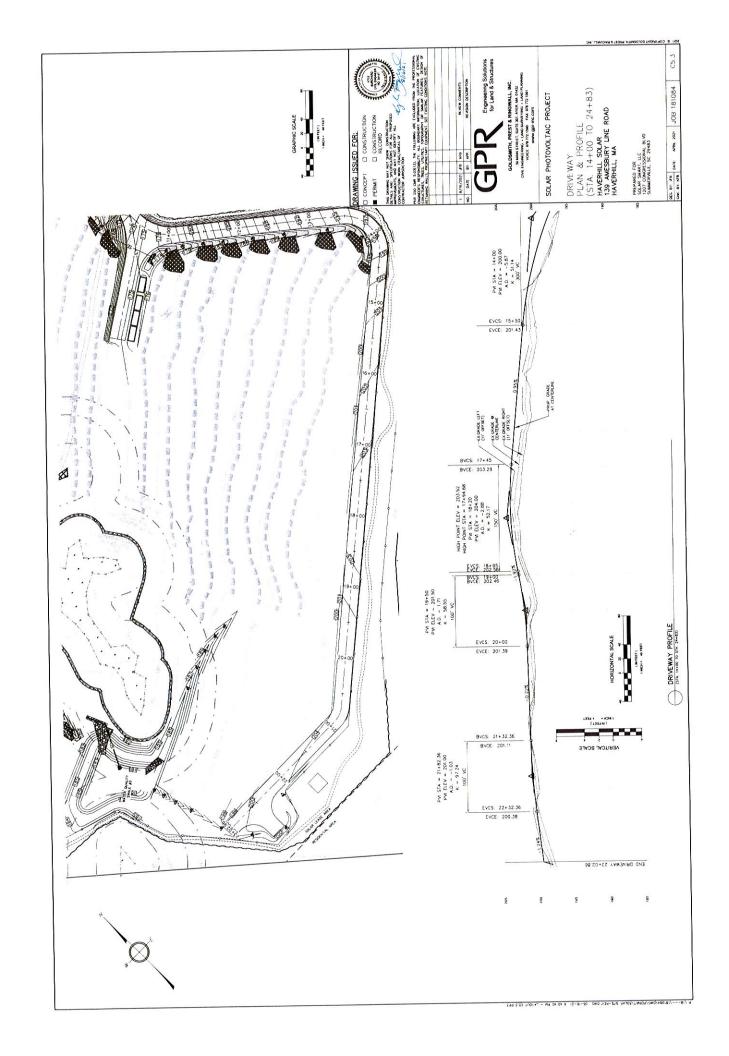


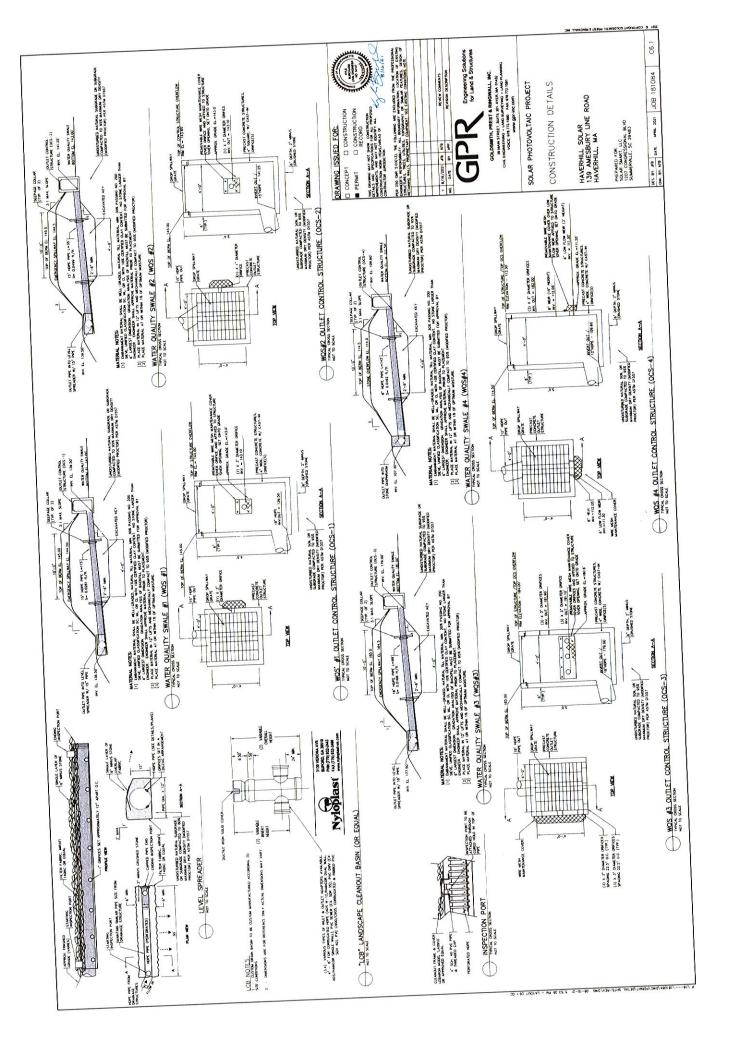


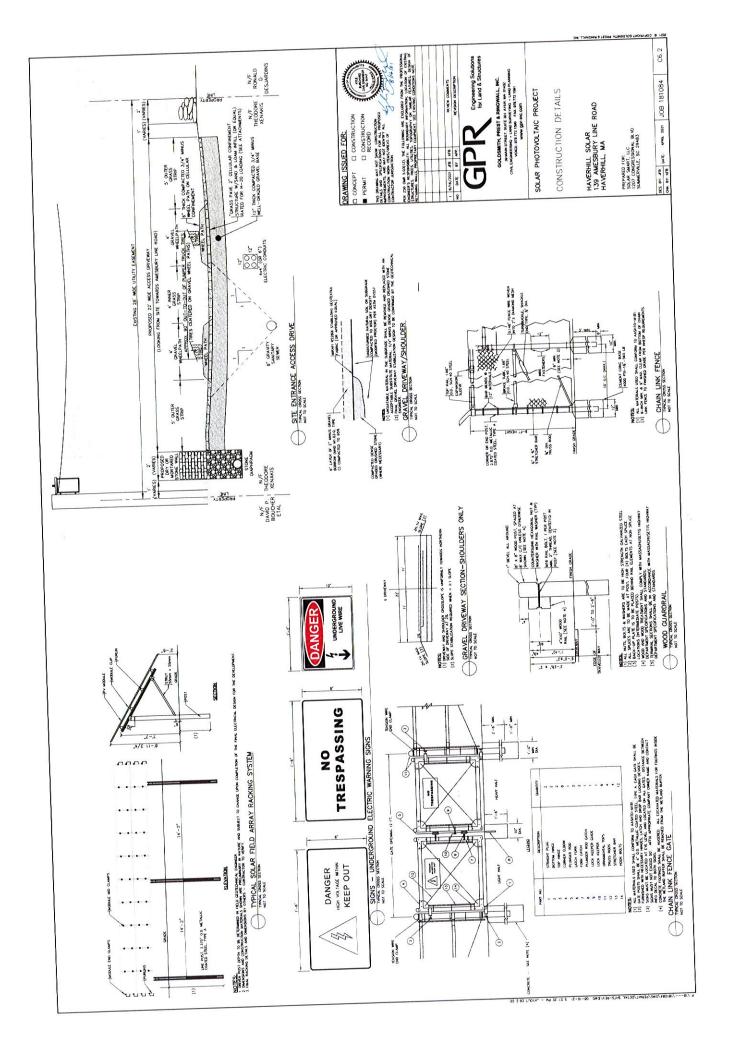


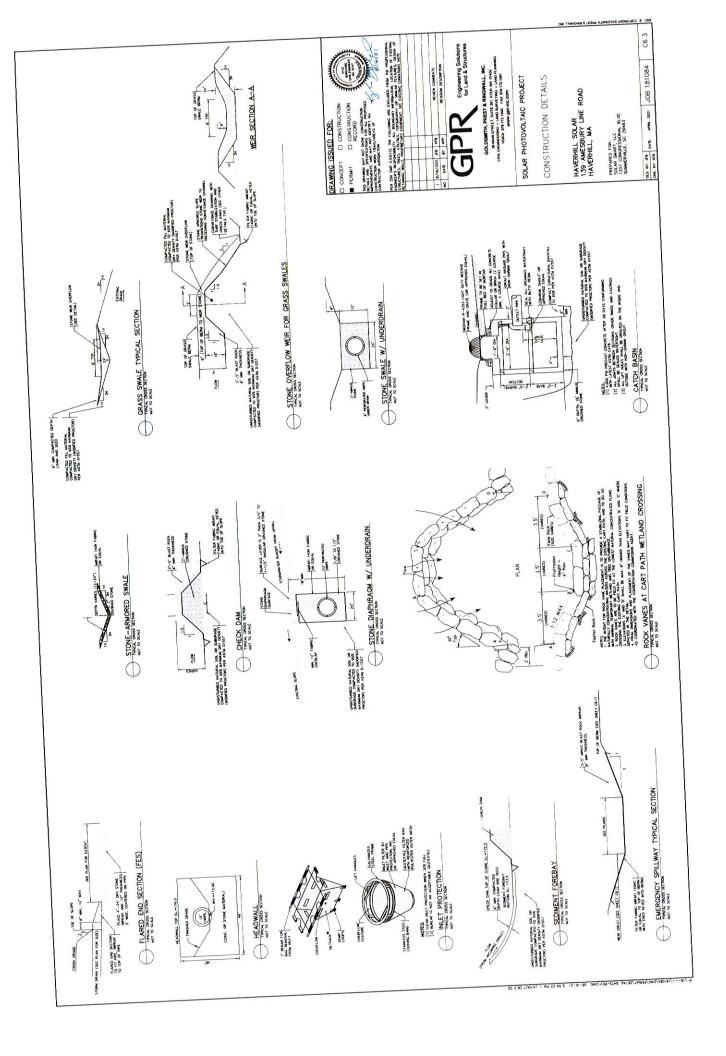


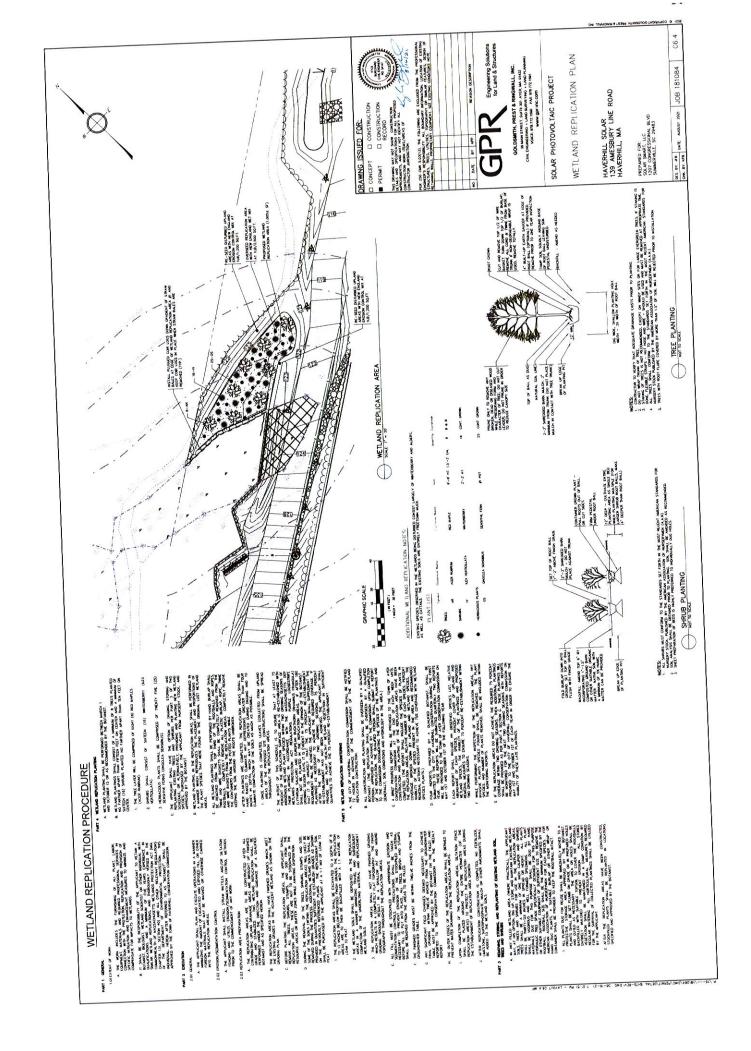


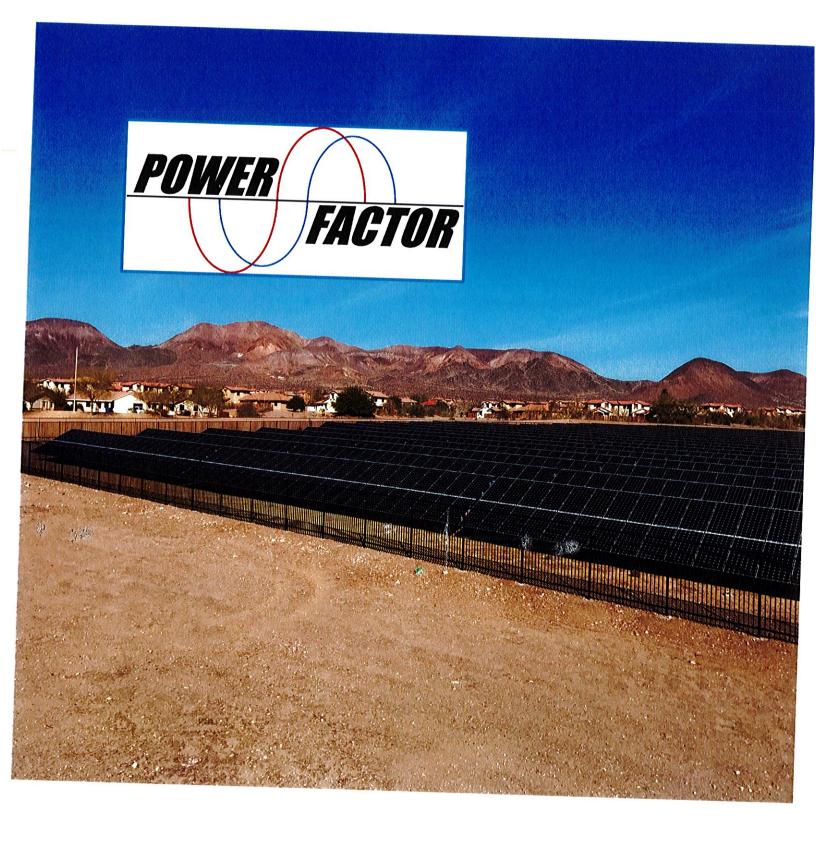












O&M PROPOSAL

George Lang IV

Andrew@powerfactorco.com

O&M Proposal



Part 1: Bidder Contact Information

Bidder Contact Information	
Corporate Name: Power Factor, LLC	
Corporate Address: 8240 Beachwood road, Dun	dalk MD 21222
	Tank HID LIZZZ
Parent's Corporate Name: Power Factor LLC	
Parent's Corporate Address: 8240 Beachwood ro	oad. Dundalk MD 21222
	and a surface with a surface s
Legally Authorized Representative	
Name: George Lang	
Title: Managing Director	
Phone: (443) 827 7543	
Fax:	
E-mail: george@powerfactorco.com	
Signature:	\$ 7 in
	A **
Primary Contact:	
Name: Andrew Streit	
Title: Director of Business Development	
Phone: (803) 665-6688	
-ax:	
-mail: andrew@powerfactorco.com	
or e powerfactor co.com	

Part 2: Executive Summary

Power Factor is honored to submit our qualifications for solar photovoltaic operations and maintenance services to Amesbury Line Solar LLC. Our company is ideally situated to deliver professionalism, excellence, efficiency and durability to Amesbury Line Solar in its efforts to successfully deploy solar projects on its properties. Due to a decade of involvement in developing customized renewable energy projects for public and private clients, Power Factor has an intimate understanding of the energy market in the southeastern United States. Our previous work with public entities has demonstrated that an elevated level of execution and delivery are the minimum standard for every government contract. We are prepared to meet and exceed those standards.

- Power Factor brings with it an experienced team of solar professionals that have successfully completed a large portfolio of projects ranging from rooftop solar arrays to solar parking canopies to utility scale solar farms.
- Power Factor has successfully deployed solar systems for a number of public entities, including various military and municipal installations.
- Power Factor has worked hand-in-hand with utilities, electric cooperatives, regulators, and private and public-sector entities to find economic, clean energy solutions that satisfy the aesthetic and sustainability goals of the client.
- Power Factor has amassed the professional capacity to manage projects on time and on budget even in the midst of challenging circumstances.
- Power Factor's reputation and history of successful solar project management should provide Amesbury Line Solar with the confidence it needs when selecting an experienced, knowledgeable operations and maintenance firm for this project.

Sustainability is not a catch phrase. It is the foundation of successful organizations. Power Factor recognizes that inventing and deploying the nation's utility grid was the single most important investment of the 20th century. Improving efficiency and eliminating waste will be primary drivers for the public and private sectors during the years to come. Given Power Factor's expertise and passion for the advancement of solar as a mainstream component of our country's energy portfolio, we are well prepared to lead in the realization and execution of these maintenance agreements. We are confident that our services will bring with them maximum value to Amesbury Line Solar and will result in a durable sustainability commitment. Power Factor is genuinely excited about our potential role in this process. We are proposing to provide all the preventative and corrective maintenance options requested, as well as providing training of any interested on-site personnel.

O&M Proposal



Preventive Maintenance Requirements and Costs

List of services:

Standard

Preventative Maintenance Work Scope	
Array Balance System	Yes/No
Array visual inspection-wire management, connector tightness, and insulation inspection	Ye
Array ground/racking debris removal and vegetation inspection	
Verify fence condition and grounding	Ye
Inspect system and site drainage	Ye
Module Visual Inspection	Ye
Inspect 100% of glass side for cleanliness and obvious defects	Yes/No
Inspect 100% of back-sheet a J-Boxes	Ye
Inspect 100% of module clamps for looseness	Ye
String Inverters (Central Inverters vary by Size/Band)	Ye
Inspect for corrosion, labelling and basic condition of housing	Yes/No
Verify functionality of display and operation of PV system	Ye:
Inspect base of inverter and conduit entry points	Yes
Clean inverter interior and inspect for moisture intrusion	Yes
Check string fuse functionality	Yes
Check ground straps and ensure all grounds are intact and tight to the enclosure	Yes
Clean heat sink and filters (replace filters if necessary)	Yes
Torque AC and DC conductors connections to manufacturers specs	Yes
IR scan all string terminations	Yes
AC/DC Disconnections & Panel Boards	Yes
Cycle all movable parts in AC/DC disconnect & Panel Boards	Yes/No
Torque all conductor connections to manufacturers specs	Yes
IR scan all string terminations	Yes
DAS & MET Stations	Yes
Inspect cabinet for labelling, corrosion, moisture intrusion and basic conditions of housing	Yes/No
Ensure all conductors and wires are routed in a neat and clean manner	Yes
Forque data terminations to manufacturers specs	Yes
Clean reference cell and/or purposes (2)	Yes
Clean reference cell and/or pyranometer (Replace desiccant)	Yes
/erify functionality of all DAS Components	Yes
Other Services (Please list below)	Yes/No

Corrective Maintenance Requirements and Costs

Corrective Maintenance (CM) Services are generally triggered by a monitoring alert reporting an issue at the site. Certain alerts can be corrected remotely, while more severe alerts can require an emergency response due to safety concerns, or (far more typically) permit the on-site service call to be scheduled.

Please indicate which services your company provides and the respective costs associated with typical corrective maintenance service visit in the O&M bid below. The preferred cost structure can be in terms of Hourly, Half Day, or Full Day Rate.

Standard

Corrective Maintenance Work Scope	
Common Corrective Maintenance Task	Yes/No
Inverter troubleshooting and warranty management String and Connector repairs	Ye
Panel Replacements	Y
Panel manufacturer defeated and	Y6
Panel manufacturer defect identification and tracking Monitoring troubleshooting and repair	Y
Fuse replacements	Ye
Breaker tightoning	Ye
Breaker tightening and replacement	Ye
Transformer Oil Sampling	Ye
Ground fault identification	
System wide IV Curve testing	Ye:
Aerial or customized IR thermal imaging	Yes
Power Quality Analysis	Yes
Additional Services May Include	Yes
Auditing/correcting sites installed by others	Yes/No
Commissioning of sites installed by others	Yes
Medium Voltage and Fiber Optic Services	Yes
Other Services (Please list below)	Yes
	Yes/No

Cost Structure for	Above Indicated Services (Fill in all that apply)
Hourly Rate	in all that apply)
Half Day Rate	\$75/hr
Full Day Rate	\$250
	\$500



O&M Proposal

Service	Service Levels and Rates	
Service	Description	Rate
Medium Voltage Electrician	location, site management	
Master Electrician Level 3 Datacom	engineering, transformers and modifications, field	\$100/hr \$75/hr
Electrician	2 capable Inverter and Datacom second level troubleshooting, panel	\$50/hr
Level 2 Technician	Images and Power Quality measurements. OEM repairs Inverter and Datacom resets. Primary trouble to	\$36/hr
Level 1 Technician	panels, and completes basic electrical and mechanical	\$25/hr
Professional Services	Performance engineering, integration services, system designs, commissioning review, project management and services oversight	
Travel Charges	For teams of 2: Labor + Mileage	\$47/hr
Per Diem	For teams of 2: Overnight Accommodations	
Overtime	Workdays exceeding 8 hours	\$250
Emergency Response	Deploy within 4 hours of notification	
	Specialized Site Services	W. Chilly Joseph Children
Service	Description	
Transformer Service	Sample of transformer fluid for DGA, refill nitrogen, includes all labor, laboratory and material costs	Rate
echnical Services	Diagnostics (IR Imaging), Module and String level I-V Characterization (IV Curves), DC/AC Power Quality Analysis (PQA)	
Comi	Other Services (Please list below)	
Service	Description	Rate

Onsite training for Amesbury Line Solar

Power Factor is happy to offer Amesbury Line Solar training services.

Training Services and Rates		
Training	Description	Rate
1-Day Training	Training to be held for Points of Contacts at a location provided by AMESBURY LINE SOLAR	\$25/hr
Customize in-class training	Half Day training(s) on specific topics of need for AMESBURY LINE SOLAR	\$50/hr
Field Shadowing	On-site, hands-on training	\$25/hr
Not Applicable	Our company does not provide specific training	725/III

Credibility

References:

- Maryland Management
 Christopher Dimario
 Rental Property Owner/Manager
 Cdimario@Marylandmgmt.com
- URI (Unlimited Restoration Inc) Rodney O'Neal Co-Owner
 ROneal@urinow.com
- Onyx renewable Partners Greg Cousoulas
 Sr VP of Construction
 On file
- Uhaul Jim Dickerson
 Owner Representative
 jim dickerson@uhaul.com



April 8, 2021 **AMENDED August 16, 2021**

City of Haverhill City Council 4 Summer Street, Haverhill, MA 01830

RE: 139 Amesbury Line Road Solar Farm

Application for Solar Energy Special Permit (§7.8.11) and Application for Water Supply Protection District (WSPD) Special Permit (§9.2.7)

Dear City Council:

On behalf of Solar Smart, LLC, the Applicant and Lessee, Goldsmith, Prest & Ringwall, Inc. (GPR) has compiled information below to support two special permit requests for the proposed 2 MW AC solar farm project at 139 Amesbury Line Road, City of Haverhill Assessors Property ID#430-11-12.

These special permit applications, including the plans and accompanying text, meet all the requirements to allow full evaluation of the proposed Large-Scale Ground-Mounted Solar Energy Use (hereinafter called the "Solar Lease Area") within the RS & RM Zoning Districts and within the City of Haverhill Water Supply Protection District (WSPD).

Introduction

The total land area of the subject property measures 26.81± acres, of which the proposed Solar Lease Area measures 18.40± 18.60± acres. Approximately 2,505 square feet of Jurisdictional wetlands present on the property shall not be altered and mitigated by wetland replication areas., and wWork within wetlands and wetland buffer zones shall be is documented in a Notice of Intent filing to the City of Haverhill Conservation Commission.

The Solar Lease Area partially straddles a natural drainage divide between the Merrimack River (to the east) and the Millvale Reservoir (to the west). This natural drainage divide also defines the limits of the City of Haverhill Water Supply Protection District (WSPD) for the Millvale Reservoir, as well as a zoning district line between the RS (Special Rural) and RM (Medium Density) residential zones. The WSPD and RS are one and the same over the Solar Lease Area. The WSPD also places a Zone 'A' Surface Water Supply Protection Area on the subject property, outside the Solar Lease Area. The remainder of the WSPD on the Solar Lease Area is considered Zone 'C' Surface Water Supply Protection Area, and all disturbances shall be documented in a Notice of Intent filling to the City of Haverhill Conservation Commission.

Goldsmith, Prest & Ringwall, Inc.

The solar energy facility is allowed in all districts by Special Permit, except the Waterfront District, as stipulated under City Ordinance Section 7.8.3.1. The project is not located in any

Solar Energy Special Permit Request

City Ordinance Section 7.8.11 Special Permit Criteria for the Large-Scale Ground-Mounted

"In addition to any other criteria set forth in this Ordinance for the grant of a special permit, the SPGA shall consider whether the grant of a special permit for a Large-Scale Ground-Mounted Solar Energy System will promote the highest and best use of the subject property, taking into account the characteristics of the subject property, including past land uses, possible presence of hazardous materials, and other

The proposed Solar Lease Area is currently forested, and slopes varying from 5% - 20% towards the Whittier School Driveway. The land is known to have been farmed in the past, and an old cart path and stone wall cuts generally east to west through the middle of the property, providing rough vehicular access and a scenic walking trail that has been used for

The current WSPD overlay is built upon state code provisions in 314 CMR 4.00 Massachusetts Surface Water Quality Standards and 310 CMR 22.00 Drinking Water, in which there are numerous limitations on the installation of septic systems, animal farming, and uses of herbicides and pesticides, in order to protect and promote surface water quality. Test holes for drainage were dug, spaced across the Solar Lease Area, that identified relatively consistently shallow seasonal high groundwater depths.

Development options for the property are somewhat limited by the forementioned regulatory, topographic and subsurface groundwater constraints. Possible development options could include moderate-intensity organic farming, and limited residential development. These options, as well as leaving the land undeveloped, could comply with regulations and conform to the constraints of the land.

The proposed solar energy farm represents a highest and best use of the land within the various regulatory and physical constraints. The solar energy farm consists of construction materials and methods that produce no hazardous or toxic wastes or byproducts. At this location, a cooperative educational relationship is in development with Paul Moskevitz, the Vocational Technical Director of the Whittier Regional Vocational Technical School. The plan is to supply the school with access to weather and solar output data, along with access to resources for emerging technologies in energy systems engineering. Raised observation areas are proposed, along with a perimeter trail to maintain the old cart path walking connection. In addition to a WSPD compliant design, pollinator seeding areas are proposed and bee hives are to be installed to promote future generations of fruitful habitat in the area.

In a broader sense, our modern society that has been built on electrical infrastructure fueled by the combustion of fossil fuels, coal and natural gas, is sourcing other fuels, including solar. Local solar energy sources provide local power grids and end users with better options from distributed power generation. Improved battery technology to be employed at 139 Amesbury Line Road will also help buffer periods of peak power usage to add resilience to the local power grid. Over time, solar installations will provide renewable, distributed, redundant, and clean energy sources serving local communities directly.

Harnessing solar energy is a highest and best use for the land at 139 Amesbury Line Road, today and into the future, with the installation of mature solar technology, accompanied by the other proposed elements for environment and education.

Water Supply Protection District (WSPD) Special Permit Request

City of Haverhill Ordinance Section 9.2 Water Supply Protection District (WSPD) lists in Section 9.2.7 Uses Permitted by Special Permit, nine (9) articles describing qualified use categories which may be granted special permit by the City Council. The proposed solar energy facility qualifies for special permit under the fourth article, (Ordinance Section 9.2.7.4) which states:

"Any use otherwise permitted as of right or by special permit that requires a permit under the National Pollutant Discharge Elimination System permit program established pursuant to 33 U.S.C § 1342, the Surface Water Discharge Permit Program established pursuant to M.G.L. c.21, s.43, or the Groundwater Discharge Permit Program established pursuant to M.G.L. c. 21, s.43."

As the solar energy facility is allowed by special permit in all but the WD District (§7.8.11), and greater than 1 acre of proposed land disturbance triggers a National Point Discharge Elimination System (NPDES) with the U.S. Environmental Protection Agency (EPA) under a Construction General Permit Notice of Intent (CGP-NOI), Ordinance Section 9.2.7.4 allows the City Council to grant a WSPD Special Permit. The following is complete in all regards, meeting all the requirements of the City of Haverhill Ordinance to allow full evaluation of the proposed use on the Water Supply Protection District. The information is provided in sequence according to the numbering listed in the City of Haverhill Ordinance.

§9.2.8.1. Application. This Application has a list of all state, local and federal permits, licenses and approvals required for the proposed activity, and the status of all such permits, licenses and approvals:

Permit Status Haverhill Solar Energy Special Permit **Applied** Haverhill WSPD Special Permit Applied Haverhill Conservation Commission NOI Not Yet Applied **EPA CGP-NOI** Apply for Construction General Contractor License Pending Selection **Building Permit** Apply for Construction **Electrical Permit** Apply for Construction

§9.2.8.2. This application is prepared in accordance with the data requirements and BMPs of the proposed development (e.g., including but not limited to erosion and sedimentation control plan, stormwater requirements, septic system designs).

An updated Stormwater Management Report, Long-Term Pollution Prevention Plan and Stormwater O&M Plan prepared in accordance with the Massachusetts Stormwater Management Handbook, and in response to Peer Review comments to the Notice of Intent application, describing all BMP's is provided as attachment to this application. A Solar Facility O&M Manual is also provided as attachment. A complete updated site plan set is provided as attachment, to depict geometric layouts, grading, drainage, and erosion and sedimentation control plans and details.

§9.2.8.3. This application is required to include a complete list of chemicals, pesticides, fuels and other potentially hazardous materials to be used or stored on the premises in any

quantity, however, there are none proposed with this project. The application shall include a Management Plan for the handling, storage and disposal of any materials identified.

Lithium-ion batteries used for energy storage and power transfer are proposed in fire-rated enclosures, with non-toxic fire suppression systems. Detailed technical information on these systems are included as attachment. No chemicals, pesticides, fuels or other potentially hazardous materials are proposed to be used or stored on the premises.

Electric transformers contain fluids for cooling. The transformers used on this project shall use Envirotemp™ 360 or FR3 fluid, which have the same general chemical composition as vegetable oil.

The proposed battery enclosures have a triple redundancy protection against failures. The modes of protection consist of:

- 1. The connex box itself is a sealed steel enclosure affixed to a concrete pad. The batteries are located inside the steel enclosure, protected from weather exposure.
- 2. An integrated cooling system and thermostat keeps the batteries from overheating.
- 3. The enclosure is equipped with a "FM-200™ Clean Agent Fire Suppression System" using the cleanest fire suppression technology available. A material safety data sheet for the active chemical, HFC-227ea is included in the appendix.

Should the cooling system fail, and the fire extinguishing system fail, any combustion of materials inside the steel connex container remains inside the container.

§9.2.8.4. This application includes an analysis by a professional Massachusetts licensed engineer experienced in groundwater evaluation to demonstrate that the proposed activity will not be detrimental to the purposes of this district as set forth in Section 9.2.1.

The proposed activity is not detrimental to the watershed to be protected.

The proposed solar panels, electrical equipment pads and gravel driveway do not generate TSS or other pollutants. The proposed drainage system provides stormwater recharge and peak flow attenuation in accordance with the standards of the Massachusetts Stormwater Management Handbook.

The site is within the watershed of the Millvale Reservoir. The existing ground surface within the project area is generally at a 15% slope draining towards the Whittier School driveway to the north. Roadside ditches along the Whittier School driveway capture runoff from the hillside and convey runoff under the road via three (3) concrete pipe culverts to a large wetland complex north of the driveway.

Two wetland areas on the subject property were flagged by wetland scientist Matthew S. Marro in September and October 2020. The third, larger wetland area on the north side of the Whittier School driveway was also flagged at this time. In July 2020, the Haverhill Conservation Commission hired a delineation consultant, Mary Rimmer of Rimmer Environmental Consulting, LTD who made changes and additions to the wetland delineation by Matthew Marro. The two consultants met and conferred on the delineation as shown on the Plan Amended 8/16/21, changing the shape of the two wetland areas and adding a third, isolated wetland area subject to the City of Haverhill Wetland Bylaw. Following the updated delineation, the project proposes wetland replication as mitigation for wetland impacts. The two primary wetland areas on the subject property form broad swales for conveyance of surface waters, and being at low points in the grade, these swales generally discharge into the drainage culverts under the Whittier School driveway. Some of the new delineated wetlands areas being impacted do not flow toward the Whittier driveway and are not in the

On 1/8/2021 soil investigation of the property was conducted by Kyle Burchard, P.E., registered Massachusetts Soil Evaluator #14048. A series of drainage test pits were dug in several locations across the proposed development in order to identify estimated seasonal high groundwater elevations and existing soil conditions. Test hole logs are included in the Stormwater Management Report attached to this application. The seasonal high water table was identified fairly consistently at 27" below the ground surface according to mottles in the soil. The chroma in the strata below the estimated seasonal high groundwater was not significantly gleyed, indicating that the soils were typically saturated without a large amount of seasonal variation in the groundwater elevation that would tend to wash more of the chroma away. The soil profile and characteristics were consistent across the whole project area, being relatively shallow groundwater and a composition of sandy loam and loam.

The relatively shallow groundwater condition on the site, and the indication of nearly constant saturation supports the proposed site stormwater BMP strategy of minimal surface grading and no impervious pavement. Long, shallow-depth, and minimally-sloped grassed swales with check dams will be incised along the hillside to capture, slow, and promote runoff recharge to groundwater. The proposed shallow manipulation of surface soils achieves the minimum Massachusetts Stormwater Management Handbook Standards of matching predevelopment to post-development peak flows, maintaining existing groundwater recharge, and promoting water quality.

The drainage calculations for the grassed swales, conveyance channels and detention basins in the Stormwater Management Report show appropriate compensation for the change in land cover from forested to grassed hillside and gravel driveway conditions.

The Massachusetts Stormwater Handbook targets a neutral stormwater impact with various BMP's and the assortment of measures proposed achieve that.

§9.2.9. Design and Performance Standards.

At the time of this application, the proposed Solar Lease Area area is wooded with a gravel cart path crossing through it from east to west, bounded on the south side by a stone wall. Other various stone walls mark some of the boundaries of the subject property. Two wetland fingers reach into the property from culverts under the adjacent Whittier School driveway to the north. The only known former use of the property was as farmland. There are no known septic fields, and no known hazardous materials on the property.

Access from Amesbury Line Road provides both temporary construction access, and permanent facility access for routine maintenance of the solar facility. This driveway access provides Fire and EMS access as well. The gravel access driveway will also be maintained as needed for stable passage. The first 280 feet of driveway from Amesbury Line Road will be treated in an alternative manner so as to appear like an old cart path, but with a stable construction meeting the approval of the Haverhill Fire Department. During construction a secondary construction access has been secured by agreement with the abutting property owner of 235 Amesbury Line Road. This secondary access will reduce construction traffic passage on the primary access driveway.

§9.2.9.1 Safeguards.

Three (3) pad-mounted and enclosed lithium-ion battery banks are proposed with the project. These three (3) large batteries are equipped with automatically deployed gaseous fire-suppression systems that suffocate any fire instantaneously without toxic residues.

Supports for the proposed solar panels consist of driven stainless-steel posts.

Buried wires and cabling are all waterproofed and insulated.

No toxic or hazardous materials or byproducts result from the solar farm installation.

§9.2.9.2. Location.

The WSPD boundary onsite has been delineated by the natural drainage divide.

Small deviations in the post-development drainage conditions are delineated on the drainage divide maps included with the Stormwater Management Report.

No toxic or hazardous discharges, nor septic discharges are proposed within the WSPD, or on the site.

§9.2.9.3. Disposal,

No onsite subsurface sewage disposal systems are proposed with this project.

§9.2.9.4. Stormwater.

The design of stormwater management measures conforms to the Massachusetts Stormwater Standards in all regards. See the Stormwater Management Report attached to this application.

The Applicant, based upon the testimony, plans and evidence submitted herewith and supplemented at the Public Hearing, respectfully requests that the City Council make a written determination and find that:

- 1. The proposed use or structure(s) shall not cause substantial detriment to the neighborhood or the City, taking into account the characteristics of the site and of the proposal in relation to that site.
- 2. There are Community energy needs which are served by this Project.
- 3. There is safe traffic and pedestrian flow provided by this Project.
- 4. There are adequate utilities and other public services for this Project.
- 5. The Natural Environment will not be impacted.
- 6. There is no impact on City services and this project will increase the city tax base.

In addition to meeting the above criteria set by Section 10.4.2, the Council can also find that the proposed use:

- 1. Satisfies the design and operations guidelines set forth in the Zoning Ordinance:
- 2. Is in harmony with the purposes and intent of this Section and will promote the purposes of the WSPD;
- 3. Is appropriate to the natural topography, soils, and other characteristics of the site to be developed;
- 4. Will not, during construction or thereafter, have an adverse environmental impact on any water body or watercourse in the district; and
- 5. Will not adversely affect the quality or quantity of an existing water supply.

The Applicant respectfully requests City Council approval of both the Solar Energy Special Permit and the Water Supply Protection District (WSPD) Special Permit.

Respectfully submitted,

Kyle Burchard, P.E.

Application Attachments:

Haverhill Solar Site Plan Set

Appendix 1- Solar Farm Components

Appendix 2- Stormwater Management Report and Operations & Maintenance Plan

Appendix 3- Solar Facility Operations & Maintenance Plan

Appendix 4- Construction Access Agreement

Appendix 5- Electrical One-Line Diagram

Appendix 6- Solar Site Illustratives

Appendix 7- Whittier School Sewer Plan

Copy to: Theodore Xenakis, Esq.

Solar Smart Development Robert D. Harb, Esq. GPR file 181084

SITE PLAN

HAVERHILL SOLAR PROJECT

HAVERHILL, MA

DATUM NAVO 1988

CLI EXISTING CONDITIONS
CLI EXISTING CONDITION
CLI EXISTING CONDITION
CLI SITE PLAN
CLI

ASSESSORS MAP 430, BLOCK 11, LOT 12

SUBMITTALS

REGULATORY NOTES

COPRINCING SHALL CONTACT DEC-SATE FOR UNGERGOOD UTILIT WIRENG AT 868 544 723 AT LLCST 72 HOUSE PHOLE PHOLE PHOLE WILL COMMUNICATION CONTINUED ON THE WIRE COMMUNICATION COMMUNICATION FOR THE PERIOD.

- CONTRACTOR SHALL COORDINATE, NO DELINE ALL CONSTRUCTION FORMETS RECORDED BY RECLATORY AND SOCIETY RESPECTION FILE.

 NATIONALES RECORDED.
 - CONTRACTOR SHALL BE ARMED OF ALL CONSTRUCTION RECOMMENTS, CONSTRUCT, AND LIMITAGES AMBORDS OF PERMITS AND APPROVALS. ISSUED BY RECULATORY AUTHORITIES PRICE TO COMMENCEDEST OF WATER WAY.
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- LIDGE REMOVAL VA BLASTING SHALL COMFORM TO 527 CAR 1.00 AND INCORPORATE THE HANDBHILL FIS DEPARTMENT LIDGE BLASTING SPECIFICATIONS.

SITE DATA

LOT AREA. OPEN SPACE. SOLAR LEASE AREA.

26.8 ±AC. (1.167.844 S.F.) 93% ± 18.6 ± AC (810,801 S.F.)

GENERAL NOTES

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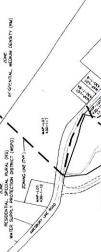
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212 & Zorang Map

Agends 6-18se 2 35 FY 23 FY 23 FY 24 FY 25 Panung Orleways and Entrances 787

430-11-1

430-11-12

SCHOOL SCHOOL

OVERALL MAP & ZONING SCALE: 1"= 250"



5. SABELT HOTICL OF HITLE TO OTT OF TAKENELL CHARGINATION COMMISSION FOR HOW THAT FALS UNCO. PICK MASSACHISTIS METANG PROTECTION OF THAT SALES UNCO. PICK MASSACHISTIS METANG PROTECTION OFGENERAL A SMBHT SEE PLAN TO DET OF HANDRIAL DENELOPHDET RENEW FOR CONSTRUCTION OF LANGE-SCALL GROUND SOLAR DIGGOS SYSTEM. 3. SPECIAL PETANT TO CITY COLANCY FOR CONSTRUCTION IN WATER SUPPLY PROTECTION DISTRICT (WARD

2. SPECIAL POINT TO GTY COUNCY FOR CONSTRUCTION OF LARGE-SCALE GROUND COORDINATE FOREN AND COMMUNICATIONS SERVICE WITH UTILITY COMPANES TO ENGINEER FOR ANY CONSTRUCTION.

PLAN REFERENCES

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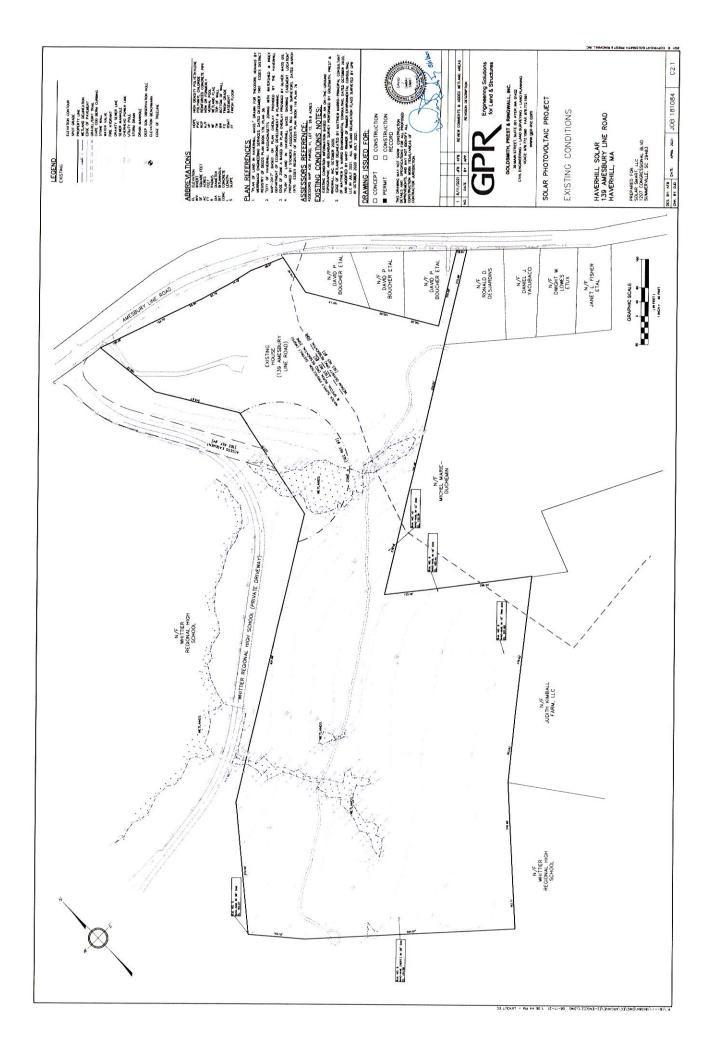
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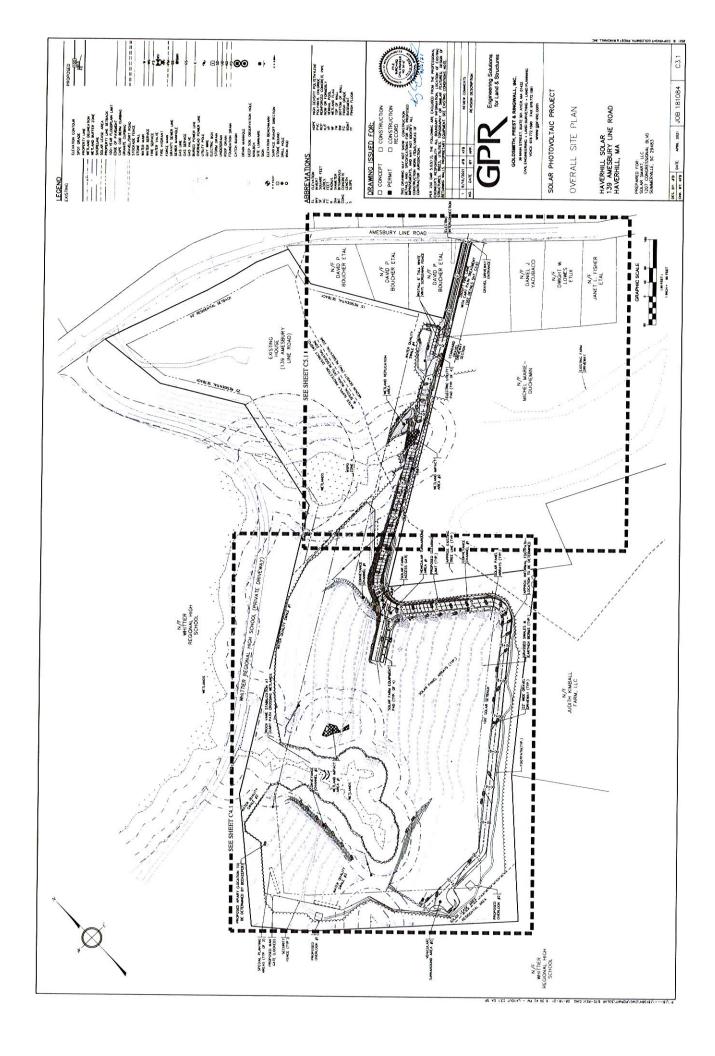
Engineering Solutions for Land & Structures

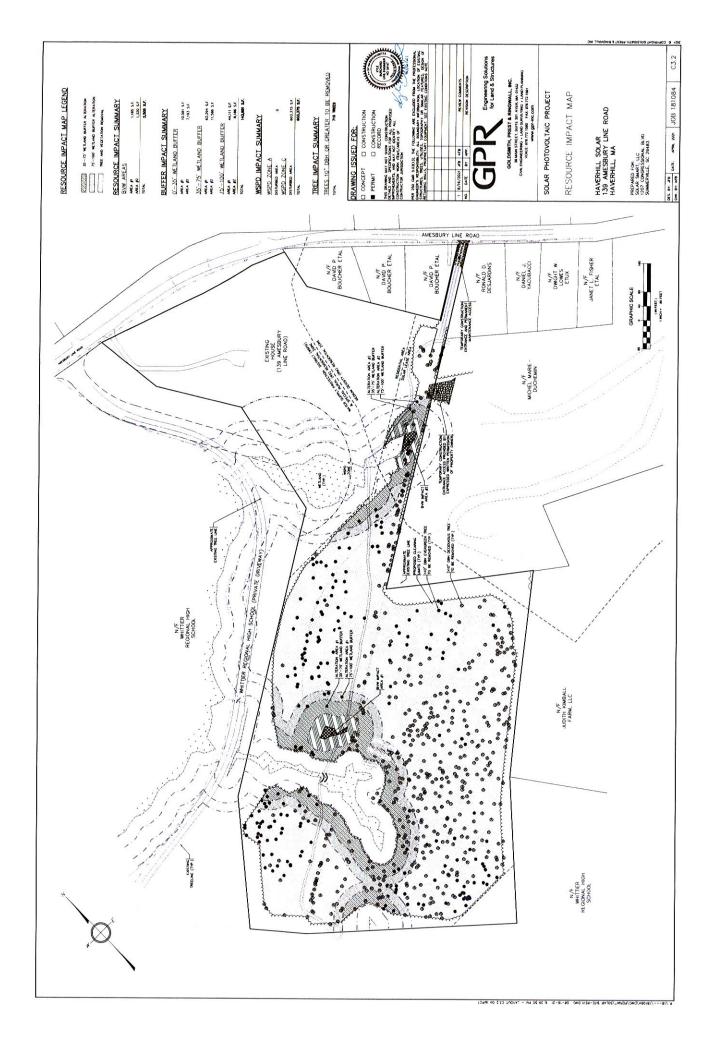
SOLAR PHOTOVOLTAIC PROJECT

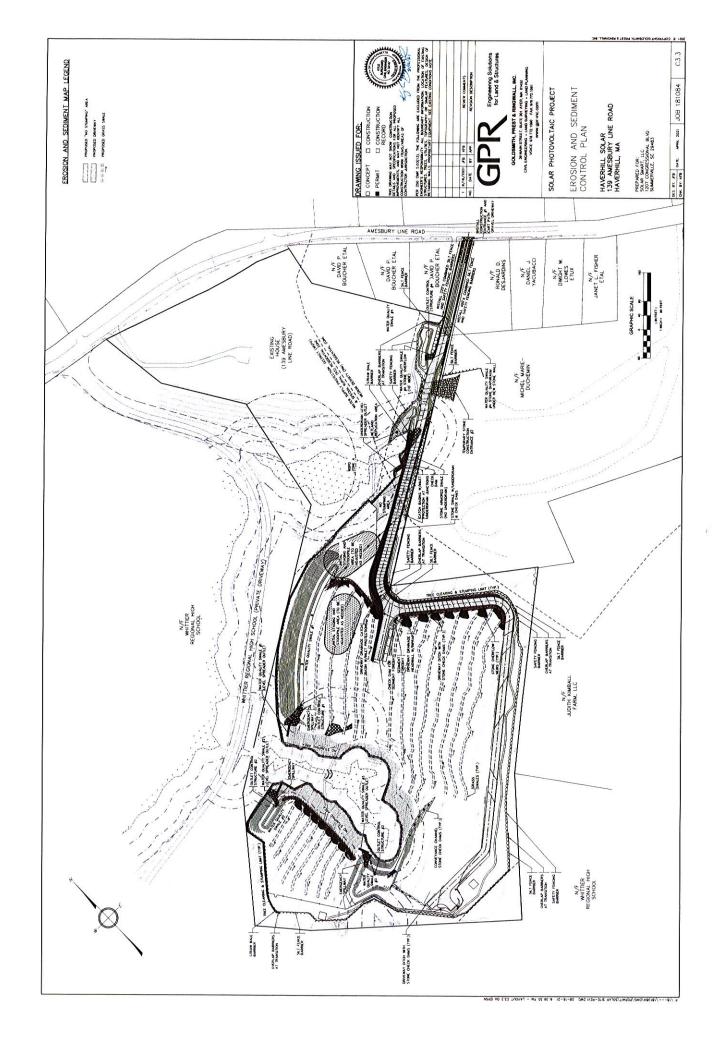
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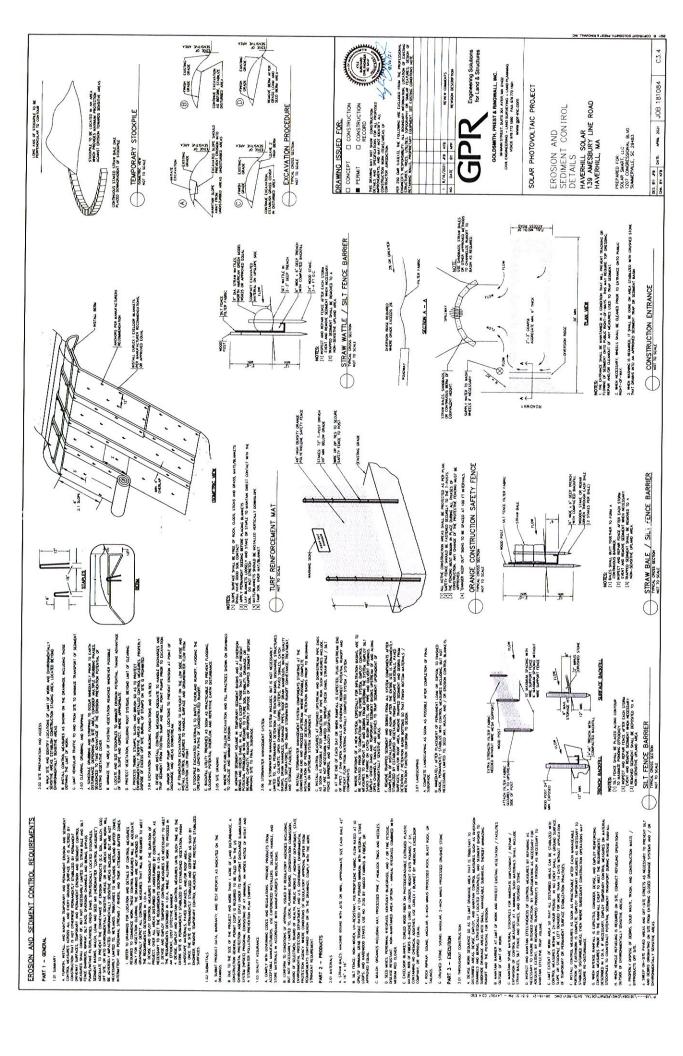
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June 2, 2021

Robert Moore, Conservation Agent Haverhill Conservation Commission 4 Summer Street, City Hall Room 300 Haverhill, MA 01830

Re: Peer Review Services

Haverhill Solar Project 139 Amesbury Line Road

Haverhill, MA

Dear Mr. Moore:

As requested by the City of Haverhill, CEI has completed a technical review of the materials and information listed below for the proposed Haverhill Solar Project at 139 Amesbury Line Road in Haverhill, MA. Our review focuses on design elements of the proposed project that pertain to the stormwater management design, based on the following information furnished to the Conservation Commission:

- 1. Notice of Intent Haverhill Solar Project, dated April, 2021, prepared by GPR Inc.;
- 2. Stormwater Management Report, dated April, 2021, prepared by GPR Inc.;
- 3. Site Plan Haverhill Solar Project, dated April, 2021, prepared by GPR Inc.

The proposed work includes construction of a large scale ground-mounted solar energy system, maintenance access road, walking trail, educational observation platforms and apiary with special seeding areas. The stormwater management design includes stone and grass swales with check dams, water quality swales with outlet control structures to collect and attenuate runoff, level spreaders at outlet pipes and stone diaphragms with underdrain pipes.

The project Site primarily wooded and includes two bordering vegetated wetlands (BVW) that are located along the northwest property boundary. A natural drainage divide at the Site is identified on the Site Plans with the majority of stormwater runoff flowing west, toward the wetlands and Whittier School driveway. This portion of the site is tributary to the City of Haverhill Water Supply Protection District (WSPD) for the Millvale Reservoir. Runoff from the remaining area of the Site flows to the east, toward Amesbury Line Road.

Proposed grading at the Site is limited due the nature of the proposed use and restrictions caused by shallow depth to groundwater throughout the project area. Site grading is primarily needed for

Mr. Robert Moore June 2, 2021 Page 2 of 6



construction of the maintenance road, turnaround areas and water quality swales. Proposed site work is located within the 100-foot wetland buffer area, with 14.6 acres of tree clearing outside of the 25-foot No Disturbance. A portion of the tree clearing area, between 35-feet and 75-feet, along the wetland area located on the western side of the site will not include stump removal to help maintain moisture retention and stabilize soils.

Soils at the Site are predominantly classified as HSG C, which have low infiltration rates. Soil test pit observations found shallow groundwater conditions that present a challenge for infiltrating and attenuating stormwater runoff.

CEI offers the following comments based on our review of the design drawings and NOI information listed above.

<u>Standard 1:</u> No new stormwater conveyances (e.g. outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

- 1. Proposed check dams along the stone and grass swales should be shown in bold, black lines to better identify the locations.
- 2. Elevations for all stone overflows should be indicted on the plans.
- 3. Widths for stone emergency spillways should be labelled.

<u>Standard 2:</u> Stormwater management systems shall be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates.

4. The HydroCAD model indicates post-development total runoff volume for the 2 year storm at AP1 (located at Amesbury Line Road) is greater than the pre-development volume. The Subcatchment (P2) area for AP1 includes the access driveway from Amesbury Line Road to the Vehicular Turnaround Area #1, wooded land to the northeast of the driveway, Water Quality Swale #4 (WQS4) and a Stone Diaphragm (a stone trench with an underdrain pipe).

The stormwater runoff from Subcatchment P2 is primarily collected by a swale on the north side of the access driveway and turnaround area, conveyed to WQS4 and discharged through an outlet control structure which then discharges to the Stone Diaphragm between the north edge of the driveway and abutting property (Lot 430-11-2A). The drainage system is designed to infiltrate runoff in WQS4 and the Stone Diaphragm. Promoting infiltration in this area may cause groundwater levels to rise above existing conditions during storm events and potentially impact abutting properties and existing on-site septic systems.

CEI recommends completing additional stormwater and groundwater evaluations, such as a mounding analysis and soil test pits, to better assess potential impacts to abutting

Mr. Robert Moore June 2, 2021 Page 3 of 6



properties. The Applicant's Engineer may also want to consider reducing stormwater flow toward Amesbury Line Road by grading the turnaround area to convey runoff to the west of the access driveway.

5. HydroCAD analysis points should be located at each of the school driveway culvert crossings to better isolate and compare each wetland drainage area under pre and post-development conditions.

<u>Standard 3:</u> Loss of annual recharge to groundwater shall be eliminated or minimized through the use of infiltration measures.

- 6. Calculations were provided to demonstrate the proposed Water Quality Swales are designed to provide infiltration for required recharge volumes below low flow orifices. The bottom elevations at Water Quality Swales 2, 3 and 4 do not appear to maintain a minimum 2-foot separation to estimated high groundwater elevations. The Applicant's Engineer may consider maintaining the existing grades at each water quality swale to establish a bottom elevation that would provide a 2-foot separation to groundwater.
- 7. Backup calculations should be provided to demonstrate all BMPs designed to provide stormwater storage completely drain within 72 hours. Calculations should include the grass swales that are proposed along the slopes leading down to the Water Quality Swales.
 - a. Consideration should be given to the potential for swales located on the upper slope to influence the groundwater elevation and dewatering capabilities of the swales located toward the bottom of the slope.
 - Construction of the grassed swales require a cut in the slope to form the swale which will further reduce depth to groundwater.
- 8. The City of Haverhill WSPD Ordinance (Section 9.2.9.4) includes a design standard that requires all increase in runoff generated on the site shall be recharged on-site in a manner demonstrated to assure full protection of the water quality and quantity in the WSPD". CEI recommends the City of Haverhill make a determination on the proposed drainage design for compliance with this design standard.

<u>Standard 4:</u> Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS).

The proposed stormwater management design provides the required TSS removal.

Mr. Robert Moore June 2, 2021 Page 4 of 6



Standard 5: For Land Uses with Higher Potential Pollutant Loads (LUHPPL), source control and pollution prevention shall be implemented.

The proposed project does not meet thresholds or characteristics of a LUHPPL.

Standard 6: Stormwater discharges near or to any critical area require the use of the specific source control and pollution prevention measures and the specific structural stormwater best management practices.

The proposed stormwater management system includes four discharge locations within the WSPD. Each location is located outside of the 25-foot No Disturbance zone and includes upstream BMPs that provide suitable treatment for managing discharges. The proposed land use does not appear to include equipment or activities that would pose a threat for an emergency spill or unexpected event which would require shutdown or containment.

<u>Standard 7:</u> Redevelopments projects are required to meet the Massachusetts Stormwater Management Standards only to the maximum extent practicable.

This project is not considered a redevelopment.

<u>Standard 8:</u> A plan to control construction-related impacts including erosion, sedimentation and other pollutant sources during construction and land disturbance activities.

- 9. A Turf Reinforcement Mat detail is included on the plans but the proposed installation areas are not shown. Plans should include labels and shaded areas where the Mat is being proposed.
- 10. The Construction Entrance detail should be revised to require a minimum length of 50 feet.
- 11. Catch basin inlet protection should be required for all proposed catch basins during the construction period and removed once the site has been fully stabilized.
- 12. Erosion and Sediment Control Notes (Sheet C3.4) should include silt sock installation, inspection and maintenance notes.
- 13. Erosion and Sediment Control should include inspection requirements with minimum weekly inspections and after every ½" storm event.
- 14. The Applicant has acknowledged a SWPPP will be submitted as part of the NPDES Construction General Permit filing with EPA. The site owner and the contractor are each



considered "operators" under that permit, and each will need to file an EPA Notice of Intent for coverage under that permit. Prior to filing a Notice of Intent, the applicant and its contractor must prepare a Stormwater Pollution Plan (SWPPP).

- a. The Applicant shall provide the Conservation Commission with a copy of the SWPPP before land disturbance commences.
- b. The Applicant shall provide the Commission with evidence that all "operators" (as defined in the NPDES Construction General Permit) have filed for coverage under the permit.

The Applicant shall obtain authorization from the Conservation Commission or its agent prior to filing a Notice of Termination under the EPA permit.

15. A phased Construction Plan is recommended to limit the area of disturbance, especially within the WSPD. Proposed water quality swales, outlet control structures and drainage swales should be stabilized and prepared to contain potential sediment runoff from upstream phased areas during the construction period. Any sediment that is collected in the BMPs shall be removed upon completion of work and re-stabilized as needed.

Standard 9: A long-term operation and maintenance plan shall be developed and implemented to ensure that stormwater management systems function as designed.

The Applicant has provided an Operation and Maintenance Plan for the Site and associated stormwater BMPs that are included in the facility design.

- 16. Designated snow storage and disposal requirements should be added in the O&M Plan and areas should be identified on the BMP Locus Plan.
- 17. Access driveway maintenance should be added in the O&M Plan to include requirements for regrading or repairing the gravel surface in order to maintain grading and properly convey runoff without causing channeling or erosion of slopes and drainage swales.
- 18. Long-term water resource pollution prevention strategies should strongly prohibit herbicide, pesticide and fertilizer application in any area of the property.

Standard 10: All illicit discharges to the stormwater management system are prohibited.

The Applicant has acknowledged an Illicit Discharge Compliance Statement is required and will be submitted prior to the discharge of any stormwater to post-construction BMPs.



General Comments:

- 19. Inspection and maintenance access ports should be included for all level spreader and underdrain pipes. Access ports should be indicated on the plans and details at both ends of each pipe.
- 20. Outlet Control Structures should include screens or cages for each orifice to help prevent clogging.
- 21. Typical Detail of the Solar Field Array Racking System should provide information for the proposed surface (i.e. grass) beneath the rows of panels and specifically alone the drip line.
- 22. Proposed check dams and stone overflow weirs should be shown as black, bold line type to better identify the proposed locations.
- 23. Spot elevations at each stone overflow weir should be labelled.
- 24. Design plans indicates a 195' stone diaphragm with a 6" underdrain pipe is proposed. The HydroCAD model includes a 100' long trench with an 8" underdrain pipe. Plans and model should be revised and consistent.
- 25. Staging area and stock pile locations are needed on the Erosion and Sediment Control Plan.
- 26. All proposed catch basins should require silt sack installation during the construction period. A silt sack detail should be added to the plans.
- 27. A proposed 22 foot wide access driveway may be excessive for the intended use. Decreasing the driveway width and replacing it with additional vegetated cover would help reduce stormwater runoff.

If you have any questions or comments regarding this report, please contact me at 508-281-5160.

Sincerely,

COMPREHENSIVE ENVIRONMENTAL, INC.

Curt Busto

Project Engineer

LEGAL DESCRIPTION OF PROPERTY

then bounders: A certain parcel of land, in Haverhill, Mass., located on the Southerly side of Amesbury Line Road, beginning at the Northeasterly corner thereof, at land of Richard Mackinion, thence running

```
along land of Mackinion and land of Henry Duchemin, along a stonewall, to a point, thence along land of Henry Duchemin, and along a stone
  S 74°-14'-50" W 523.81'
  s 74°-48'-11" W 194.48'
                                                                       wall, to a point, thence
along land of Henry Duchemin, and along a stone
wall, to a point, thence
along land of Henry Duchemin, and along a stone
wall, to a point, thence
   S.74°-16'-35" W 276.18'
   S 35°-20'-48" E 123.49'
                                                                       along land of Henry Duchemin, to an iron pipe at land of George Kimball, thence along land of George Kimball, along a stone wall, to a point thence alone land of Coorse Kimball.
  S 36°-22'-52" E 296.04'
  s 67°-52'-39" W 379.62"
                                                                        along land of George Kimball, along a stone
  s 66°-56'-38" W 203.83'
                                                                       wall, to an iron pipe, at the land of the Whittier
Regional Vocational Technical High School, thence
along land of the Whittier Regional Vocational
  S 58°-14'-52" W 246.96'
                                                                        Technical High School, along a stonewall, to a
                                                                        point, thence
along land of the Whittier Regional Vocational
Technical High School, along a stonewall, to a
   S 58°-11'-56" W 162.71'
                                                                        point, thence
along land of the Whittier Regional Vocational
   N 31°-47'-34" W 594.67'
                                                                        High School, to an iron rod at a stonewall, thence along land of the Whittier Regional Vocational
   N 24°-13'-18" W 160.10'
                                                                        Technical High School, along a stonewall, to an
                                                                        iron rod, themce
along land of the Whittier Regional Vocational
Technical High School, to a point, themce
along land of the Whittier Regional Vocational
   N 55°-42'-40" E 372.50'
   N 74°-24'-56" E 831.89'
                                                                        along Land of the Whittler Regional Vocational Technical High School, to a point, thence along Land of the Whittier Regional Vocational Technical High School, to an iron pipe, thence along Land of the Whittier Regional Vocational Technical High School, to an iron pipe, thence
   N 27°-47'-36" E 337.71'
   N 15°-20'-04" W 245.67'
N 09°-33'-06" E 198.32'

$ 54°-51'-26" E 105.49'

$ 54°-55'-26" E 153.70'

$ 53°-52'-44" E 60.90'
                                                                      to a point at Amesbury Line Road, thence
                                                                     along Amesbury Line Road to a point, thence
along Amesbury Line Road to a point, thence
along Amesbury Line Road to a point, thence
                                                                     along Amesbury Line Road to a point, thence
along Amesbury Line Road to a point, thence
along Amesbury Line Road to a point at land of
 S 57°-37'-52" E 82.76'
S 60°-39'-23" E 74.49'
S 51°-01'-34" E 98.07'
                                                                     Melvin Nelson, thence
along land of Melvin Nelson to a point, thence
along land of Melvin Nelson to a point, thence
$ 27°-40'-10" E 116.10'
$ 14°-47'-35" E 387.48'
N 74°-14*-50" E 219.00"
                                                                     along land of Melvin Nelson to a point at Amesbury
Line Road, thence
                                                                     along Amesbury Line Road, to a stonewall, at land of Richard MacKinion, being the point of beginning.
 S 30"-10'-10" E 28.91'
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Said parcel contains 26.813 Acres, and is subject to a 28' wide utility easement shown in more detail on the plan referenced below, and said parcel is subject to the benefit of a right-of-way to pass and repass over land of the Whittier Regional Vocational Technical High School, as shown on the referenced plan, and as noted in Book 5686, Page 428 in the Essex South District Registry of Deeds. Said parcel is more particularly shown on a "Plan of Land in Haverhill, Mass., drawn for Theodore Kenakis, December 1981, scale 1"=80', Merrimack Engineering Services, 66 Park Street, Andover, Mass".

For my title see deed recorded with Essex South District Registry of Deeds at Book 15605 , Page 19

NOTICE OF LEASE

LANDLORD:

Theodore Xenakis

139 Amesbury Line Road

Haverhill, Massachusetts 01830

TENANT:

Solar Smart, LLC

1605 Central Avenue

STE 6, #255

Summerville, South Carolina 29483

PREMISES:

139 Amesbury Line Road

Haverhill, Massachusetts 01830

TERM:

, 2021 through

, 2046

OPTIONS TO

EXTEND:

The lease also provides the Tenant with the option to extend

the lease for up to two (2) five (5) year extensions

Date of Lease:

, 2021

EXECUTED as a SEALED INSTRUMENT this guiday of March

....

, 2021

Witness

Theodore Xenakis- Landlord

Solar Smart, LLC

Witness

Peter Rundle CEO Tomont

COMMONWEALTH OF MASSACHUSETTS

Essex.	SS.

March 24,2021

On this 14 day of March , 2021, before me the undersigned notary public, personally appeared the above named Theodore Xenakis, as aforesaid, proved to me through satisfactory evidence of identification, which was a valid driver's license with photographic identification, to be the person whose name is signed on the preceding or attached document, and acknowledged to me that he signed it voluntarily for its stated purpose.

> Notary Public My Commission Expires: しつぎ ロンチ Notary Public

Commonwealth of Massachusetts
My Commission Expires

COMMONWEALTH OF SOUTH CAROLINA

Essex, ss.

March ZU, 2021

Delorah a Conner

On this 24 day of Morth , 2021, before me the undersigned notary public, personally appeared the above named Peter Rundle, as aforesaid, proved to me through satisfactory evidence of identification, which was a valid driver's license with photographic identification, which was SCDL 101505149, to be the person whose name is signed on the preceding or attached document, and acknowledged to me that he signed it voluntarily on behalf of Solar Smart, LLC for its stated purpose as Tenant.

Witness my hand and official seal:

JACKSON GILBERT Notary Public, State of 8C My Comm Exp 08/19/2030

Notary Public My Commission Expires:

Theodore Xenakis

Attorney at Law

139 Amesbury Line Road Haverhill, MA 01830 (978) 373-5493

Xenakislawoffice@gmail.com

March 31, 2021

Haverhill City Council City Hall Building Room 204 4 Summer Street Haverhill, MA 01830

Re:

139 Amesbury Line Road Solar Farm

Application for Solar Use Special Permit (§7.8.11) and

Application for Water Supply Protection District (WSPD) Special Permit (§9.2.7)

Dear City Council Members:

Please be advised that as owner of the real estate located at 139 Amesbury Line Road, Haverhill, Massachusetts 01830, I hereby give my consent to the above referenced applications by Solar Smart, LLC, the Applicant and Lessee.

I respectfully request that the aforesaid applications be granted.

Thank you for your kind consideration.

Sincerely yours,

Theodore Xenakis, Esquire

TX/bpm

Applicant Responses To City Department Comments

2021.04.14

LINDA KOUTOULAS commented on City Clerk Review - Hearing Dates Set for #CCSP-21-8

"Hearing scheduled for Jun 15"

RESPONSE: We have sought continuances as appropriate. Thank you for your response. 2021.05.12

John D'Aoust commented on Water Supply Review for #CCSP-21-9

"The Haverhill Water Department (HWD) has reviewed the proposed solar facility finds that the proposed use is not a prohibited under Chapter 255 Sec 9.2.6. The site storm water management plan and facility O&M plan have been reviewed and do not present any concerns in terms of water supply protection as all proposed activities are outside the delineated Zone A for surface water protection.

The Facility O&M does list a preventative activity related to sampling of transformer fluids. The HWD was unable to determine if any of the proposed equipment that contained hazardous liquids such as transformers and batteries were protected from accidental release with containment areas. The HWD recommends that the applicant describe what type of hazardous liquids or other materials may be in use on the site and how protective measures will be applied to prevent accidental releases."

RESPONSE: Electric transformers shall use EnvirotemeTM 360 or FR3 fluid, which have the same regeneral chemical composition as vegetable oil. Considered substantially inert to the environment, no secondary containment is proposed. MSDS are included in Appendix 1 of the AMENDED City Council Special Permit Application.

The proposed battery enclosures have a triple redundancy protection against failures. The modes of protection consist of:

- 1. The connex box itself is a sealed steel enclosure affixed to a concrete pad. The batteries are located inside the steel enclosure, protected from weather exposure.
- 2. An integrated cooling system and thermostat keeps the batteries from overheating.
- 3. The enclosure is equipped with a "FM-200™ Clean Agent Fire Suppression System" using the cleanest fire suppression technology available. A material safety data sheet for the active chemical, HFC-227ea is included in Appendix 1.

Should the cooling system fail, and the fire extinguishing system fail, any combustion of materials inside the steel connex container remains inside the container.

2021.05.18

Michael Picard commented on Fire2 Department Review for #CCSP-21-8 & #CCSP-21-9

"The planning, design and construction of new buildings, renovation of existing buildings and structures to provide egress facilities, fire protection and built-in fire protection equipment shall be in accordance with 780 CMR; and any alterations, additions or changes in buildings required by the provisions of 527 CMR which in the scope of 780 CMR, 9th edition, shall be made in accordance therewith. (527 CMR 1.04(4) and 780 CMR 101.2). Additionally, 780 CMR (901.2.1) Document Submittal Process will be required.

Plans approved by the fire department are approved with the intent they comply in all respects to MSBC, 780 CMR 527 CMR 1.00, MGL Chapter 148 and any City of Haverhill ordinance. Any omissions or errors on the plans do not relieve the applicant of complying with applicable requirements.

Project must comply with the City of Haverhill rules and regulations regarding zoning for solar fields

Required on site plan: Fire Department access Turnarounds Road width Grade of road

Special considerations:

Battery storage location
Suppression system for battery storage location Permitted
Remote shutoff locations
Key boxes
Emergency contact information"

RESPONSE: Fire Department access, turnarounds, road width and grades of the road are depicted on the Site Plan sheets. An Amended One-Line Diagram depicting the features of the electrical system is in Appendix 5, and considerations for final placements of all shutoff locations, key boxes, and emergency contact information shall be provided to the satisfaction of the City of Haverhill Fire Department on final electrical engineering drawings. Thank you for your response.

2021.05.20

4.30

Mark Tolman commented on Health Department Review for #CCSP-21-8

"No BOH approvals required."

2021.06.08

RESPONSE: We acknowledge your response. Thank you for your response.

Mark Tolman commented on Health Department Review for #CCSP-21-9

"BOH has no concern at this time."

RESPONSE: We acknowledge your response. Thank you for your response.

2021.05.27

Paul Jessel commented on Wastewater Review for #CCSP-21-9

City sewerage is not available

RESPONSE: We acknowledge your response, and no sewerage service is proposed or requested. Thank you for your response.

2021.06.01

John D'Aoust commented on Water Supply Review for #CCSP-21-8

"The Haverhill Water Department (HWD) has reviewed the provided information and finds that the proposed use is not prohibited by Chapter 255 Sec 9.2.6 of the City's zoning code. The proposed project lies in the public water supply watershed for the Millvale Reservoir. As indicated on the submitted plans the proposed work onsite is outside of the delineated water supply protection zone A.

The HWD reviewed the proposed facility storm water management and operations and maintenance plans. It is noted in the operations and maintenance plan that there is a maintenance item related to transformer fluids. It is unclear how the proposed facility will provide protection from an accidental release of hazardous fluids or liquids from transformers, batteries, or other equipment that may be used at the site. The HWD recommends that the applicant describe to what extent there may be hazardous fluids, liquids, or other materials used on the site and what means will be taken to prevent an accidental release."

RESPONSE: Electric transformers shall use EnvirotempTM 360 or FR3 fluid, which have the same general chemical composition as vegetable oil. Considered substantially inert to the environment, no secondary containment is proposed. MSDS are included in Appendix 1 of the AMENDED City Council Special Permit Application.

The proposed battery enclosures have a triple redundancy protection against failures. The modes of protection consist of:

- 1. The connex box itself is a sealed steel enclosure affixed to a concrete pad. The batteries are located inside the steel enclosure, protected from weather exposure.
- 2. An integrated cooling system and thermostat keeps the batteries from overheating.
- 3. The enclosure is equipped with a "FM-200TM Clean Agent Fire Suppression System" using the cleanest fire suppression technology available. A material safety data sheet for the active chemical, HFC-227ea is included in Appendix 1.

Should the cooling system fail, and the fire extinguishing system fail, any combustion of materials inside the steel connex container remains inside the container.

2021.06.01

Glenn Smith commented on Water Department Review for #CCSP-21-8 & #CCSP-21-9

"There is NO WATER INFRASTRUCTURE proposed for this project. The Water Distribution Division has NO COMMENT at this time."

RESPONSE: We acknowledge your response. Thank you for your response.

2021.06.07

Robert Ward commented on Wastewater Review for #CCSP-21-8

"The proposed solar energy facility does not require a sewer connection." RESPONSE: This comment is accurate. No sewer connection is needed. Thank you for your response.

2021.06.11

Robert Moore commented on Storm Water Review for #CCSP-21-9

"Applicant has filed a Notice of Intent application with the Conservation Commission. The hearing is currently ongoing. The next scheduled date for hearing discussion is June 24th. To date, concerns with the wetland boundaries represented on the plan have been identified. Additional concerns, pertaining to the stormwater management design, have also be identified through the Commission's peer review process. A copy of the initial stormwater peer review letter will be uploaded to this record for the Council. The applicant's consultants continue to work with the Commission to resolved the identified concerns." RESPONSE: Peer Review comments have been addressed and updated plans and reports provided for second review. Thank you for your response.

2021.07.07

Robert Ward commented on Water Department Review for #CCSP-21-8

"The project solar array which does not require water."

Robert Ward commented on Water Department Review for #CCSP-21-8

RESPONSE: We acknowledge your response, and this is correct. Thank you for your response.

"The Water Department does not object to approval of a special permit for this project." RESPONSE: Thank you for your response.

Kyle Burchard

From:

Lieutenant Michael Picard < MPicard@haverhillfire.com>

Sent:

July 22, 2021 3:16 PM

To:

Kyle Burchard

Subject:

Re: External Message Solar Smart Fire Lane Proposal

Hello.

After the Fire Department review of the lower road surface at 139 Amesbury Line Road, it was determined that the Fire Department will accept the proposal for the system listed. GRASSPAVE2 or equivalent, if it can support a Fire Department Engine at 39,620 pounds.

Lt. Michael Picard Haverhill Fire Department

Fire Prevention / Investigation Unit

Tel: 978-373-8460 Fax: 978-521-4441

Email: mpicard@haverhillfire.com

From: Kyle Burchard <KBurchard@gpr-inc.com>

Sent: Friday, July 16, 2021 5:23 PM

To: Lieutenant Michael Picard <MPicard@haverhillfire.com>; Deputy Chief Eric Tarpy <ETarpy@haverhillfire.com>

Subject: External Message Solar Smart Fire Lane Proposal

CAUTION: This email originated from outside the organization. Do not click links or open attachments unless you recognize the sender and know the content is safe.

Good afternoon.

Several weeks ago I had discussed with both of you at different times an alternative treatment of the proposed driveway entrance to the solar farm proposed at 139 Amesbury Line Road by Solar Smart LLC on the land of Ted Xenakis. I was supposed to send the attached proposal back then also, but resolving various other engineering issues needed to come first.

Please review the attached proposal letter, drawings and documents for the treatment of the initial part of the fire lane from Amesbury Line Road, and let me know if you have guestions.

I hope that the proposal is acceptable to the Fire Department for this unique access for the reasons stated within, or that we can resolve any concerns that you have.

Have a good weekend and I look forward to speaking with you next week. Thank you.

Kyle Burchard, P.E.

Goldsmith, Prest & Ringwall, Inc. 39 Main Street, Suite 301, Ayer, MA 01432 T 978-772-1590 F 978-772-1591

Licensed in MA, ME, NH & VA

Engineering Solutions for Land & Structures.

www.gpr-inc.com

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430-1-10 FEENSTRA BRAD MICHAEL-ETAL

114 AMESBURY LINE ROAD

HAVERHILL, MA 01830

430-1-7

FAY JAMES M 120 AMESBURY LINE RD

HAVERHILL, MA 01830

430-1-7A

WHITTIER REGIONAL HIGH SCH 115 AMESBURY LINE RD HAVERHILL, MA 01830

430-1-7B

LeBLANC-MEDEIROS MOLLY K-ETALI

9 VALLEY ST

MERRIMAC, MA 01860

430-1-8

BINKS JOSEPH A

180 AMESBURY LINE RD

HAVERHILL, MA 01830

430-1-8A

ANDREOTTOLA MICHAEL D 178 AMESBURY LINE RD

HAVERHILL, MA 01830

430-11-1

DUCHEMIN MICHEL MARIE-ETAL

235 AMESBURY LINE RD

HAVERHILL, MA 01830

430-11-12

XENAKIS THEODORE

139 AMESBURY LINE RD

HAVERHILL, MA 01830

430-11-17

BOUCHER GERARD

189 AMESBURY LINE RD

HAVERHILL, MA 01830

430-11-17-2

BOUCHER DAVID P ETAL

189 AMESBURY LINE RD

HAVERHILL, MA 01830

430-11-17-3

BOUCHER DAVID P ETAL

189 AMESBURY LINE RD

HAVERHILL, MA 01830

430-11-18A

WHITTIER REGIONAL HIGH SCH

115 AMESBURY LINE RD

HAVERHILL, MA 01830

430-11-2

YACUBACCI DANIEL J

205 AMESBURY LINE RD

HAVERHILL, MA 01830-1732

430-11-2A

PEPE WILLIAM C

32 GREENLEAF ST

BRADFORD, MA 01835

430-11-3

LOWES DWIGHT W ETUX

217 AMESBURY LINE RD

HAVERHILL, MA 01830

460-1-7

JUDITH KIMBALL FARM, LLC

272 NORTH EAST POND RD

MILTON, NH 03851

TO: Whom It May Concern

June 5, 2021

RE: Honey Bee colony installations on land to be leased by POWERFACTOR Company off Amesbury Line Road, Haverhill, MA (Theodore Xenakis, owner)

Dear Sirs/Madams:

Please be advised that I am developing a partnership with representatives of POWERFACTOR Company, to install an environmentally-friendly system of beehives on the above-noted property. I will be working directly with a professional full-time beekeeper from West Peabody,MA as well, in order to setup the hives in the most ergonomically/aesthetically- efficient manner for this property. It is my understanding that POWERFACTOR Company will coordinate wildflower plots in conjunction with suitable vegetation for the hives which should thrive as a result. Management of the hives will occur on a regular basis by myself and/or other beekeepers for the duration of the projected solar project.

As most know, honey bee pollination is essential for the growth of most local fruits and vegetables which we all consume. The proposed solar location is adjacent to several Haverhill farms, as well as numerous homes and waterways. This project should provide an inspiration for beautification of rural properties in Haverhill, and could provide a future site for school children educational projects as well!

Once established, it would be my pleasure to personally accommodate any Councilors who may be interested in viewing the beehive/solar project. Perhaps a jar of honey for sampling could be an enticement as well?

Respectfully,

Dr.Sam Amari, Jr

Haverhill, MA 978-373-9330



CCSP-21-9

Wastewater Review

City Council Special Permit

Status: Complete

Assignee: Paul Jessel

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Comments

Paul Jessel, May 27, 2021 at 10:29am City sewerage is not available 08/18/2021

Became Active: 05/18/2021

Completed: 05/27/2021

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE
139 AMESBURY LINE RD HAVERHILL, MA
201830



CCSP-21-9

Water Supply Review

City Council Special Permit

Status: Complete

Assignee: John D'Aoust

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611 **Became Active:** 05/18/2021

Completed: 05/27/2021

Location

139 AMESBURY LINE RD Haverhill. MA 01830

Owner:

XENAKIS THEODORE
139 AMESBURY LINE RD HAVERHILL, MA
01830

Comments

John D'Aoust, May 13, 2021 at 7:06am

The Haverhill Water Department (HWD) has reviewed the provided information and finds that the proposed use is not prohibited by Chapter 255 Sec 9.2.6 of the City's zoning code. The proposed project lies in the public water supply watershed for the Millvale Reservoir. As indicated on the submitted plans the proposed work onsite is outside of the delineated water supply protection zone A.

The HWD reviewed the proposed facility storm water management and operations and maintenance plans. It is noted in the operations and maintenance plan that there is a maintenance item related to transformer fluids. It is unclear how the proposed facility will provide protection from an accidental release of hazardous fluids or liquids from transformers, batteries, or other equipment that may be used at the site. The HWD recommends that the applicant describe to what extent there may be hazardous fluids, liquids, or other materials used on the site and what means will be taken to prevent an accidental release.



CCSP-21-9

Water Department Review

City Council Special Permit

Status: Complete

Assignee: Glenn Smith

Became Active: 05/18/2021

Completed: 06/01/2021

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Glenn Smith, Jun 1, 2021 at 4:41pm

There is NO WATER INFRASTRUCTURE proposed for this project. The Water Distribution Division has NO COMMENT at this time.



CCSP-21-9

Conservation Department Review

City Council Special Permit

Status: Complete

Assignee: Robert Moore

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611 **Became Active:** 05/18/2021

Completed: 06/11/2021

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Robert Moore, Jun 11, 2021 at 12:47pm

Applicant has filed a Notice of Intent application with the Conservation Commission. The hearing is currently ongoing. The next scheduled date for hearing discussion is June 24th. To date, concerns with the wetland boundaries represented on the plan have been identified. Additional concerns, pertaining to the stormwater management design, have also be identified through the Commission's peer review process. A copy of the initial stormwater peer review letter will be uploaded to this record for the Council. The applicant's consultants continue to work with the Commission to resolved the identified concerns.



CCSP-21-9

Storm Water Review

City Council Special Permit

Status: Complete

Assignee: Robert Moore

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611 **Became Active:** 05/18/2021

Completed: 06/11/2021

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Robert Moore, Jun 11, 2021 at 12:47pm

Applicant has filed a Notice of Intent application with the Conservation Commission. The hearing is currently ongoing. The next scheduled date for hearing discussion is June 24th. To date, concerns with the wetland boundaries represented on the plan have been identified. Additional concerns, pertaining to the stormwater management design, have also be identified through the Commission's peer review process. A copy of the initial stormwater peer review letter will be uploaded to this record for the Council. The applicant's consultants continue to work with the Commission to resolved the identified concerns.



CCSP-21-9

Planning Director Approval for Agenda

City Council Special Permit

Status: Pending

Assignee: William Pillsbury

Became Active:

Completed:

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE
139 AMESBURY LINE RD HAVERHILL, MA
01830

Comments

William Pillsbury, Jun 10, 2021 at 12:31pm

Recommend approval of the two requested special permits as presented



CCSP-21-9

Fire2 Department Review

City Council Special Permit

Status: Complete

Assignee: Michael Picard

Became Active: 05/18/2021

Completed: 05/18/2021

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Michael Picard, May 18, 2021 at 4:27pm

The planning, design and construction of new buildings, renovation of existing buildings and structures to provide egress facilities, fire protection and built-in fire protection equipment shall be in accordance with 780 CMR; and any alterations, additions or changes in buildings required by the provisions of 527 CMR which in the scope of 780 CMR, 9th edition, shall be made in accordance therewith. (527 CMR 1.04(4) and 780 CMR 101.2). Additionally, 780 CMR (901.2.1) Document Submittal Process will be required.

Plans approved by the fire department are approved with the intent they comply in all respects to MSBC, 780 CMR 527 CMR 1.00, MGL Chapter 148 and any City of Haverhill ordinance. Any omissions or errors on the plans do not relieve the applicant of complying with applicable requirements.

Project must comply with the City of Haverhill rules and regulations regarding zoning for solar fields

Required on site plan:

Fire Department access Turnarounds Road width Grade of road

Special considerations:

Battery storage location Suppression system for battery storage location Permitted Remote shutoff locations Key boxes Emergency contact information



CCSP-21-8

08/18/2021

Building Inspector Review

City Council Special Permit

Status: Complete

Assignee: Tom Bridgewater

Became Active: 04/13/2021

Completed: 05/09/2021

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Tom Bridgewater, May 9, 2021 at 8:48pm

This project will meet all zoning requirements, after reviewing I concur with the zoning opinion. This project went thru a PPR review before submitting to CC



CCSP-21-8

Fire2 Department Review

City Council Special Permit

Status: Complete

Assignee: Michael Picard

Became Active: 05/18/2021

Completed: 05/18/2021

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Michael Picard, May 18, 2021 at 12:14pm

The planning, design and construction of new buildings, renovation of existing buildings and structures to provide egress facilities, fire protection and built-in fire protection equipment shall be in accordance with 780 CMR; and any alterations, additions or changes in buildings required by the provisions of 527 CMR which in the scope of 780 CMR, 9th edition, shall be made in accordance therewith. (527 CMR 1.04(4) and 780 CMR 101.2). Additionally, 780 CMR (901.2.1) Document Submittal Process will be required.

Plans approved by the fire department are approved with the intent they comply in all respects to MSBC, 780 CMR 527 CMR 1.00, MGL Chapter 148 and any City of Haverhill ordinance. Any omissions or errors on the plans do not relieve the applicant of complying with applicable requirements.

Project must comply with the City of Haverhill rules and regulations regarding zoning for solar fields

Required on site plan: Fire Department access Turnarounds Road width 8/18/2021 OpenGov

Grade of road

Special considerations:

Battery storage location Suppression system for battery storage location Permitted Remote shutoff locations Key boxes Emergency contact information



CCSP-21-8

Water Department Review

City Council Special Permit

Status: Complete

Assignee: Robert Ward

Became Active: 05/18/2021

Completed: 06/07/2021

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Glenn Smith, Jun 1, 2021 at 4:32pm

There is NO WATER INFRASTRUCTURE proposed for this project. The Water Distribution Division has NO COMMENTS at this time.

Robert Ward, Jul 7, 2021 at 3:29pm

The Water Department does not object to approval of a special permit for this project.



08/18/2021

CCSP-21-8

Wastewater Review

City Council Special Permit

Status: Complete

Assignee: Robert Ward

Became Active: 05/18/2021

Completed: 06/07/2021

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Robert Ward, Jun 7, 2021 at 12:28pm

The proposed solar energy facility does not require a sewer connection.



08/18/2021

CCSP-21-8

Conservation Department Review

City Council Special Permit

Status: Complete

Assignee: Robert Moore

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611 **Became Active:** 05/18/2021

Completed: 06/11/2021

Location

139 AMESBURY LINE RD Haverhill. MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

Robert Moore, Jun 11, 2021 at 12:45pm

Applicant has filed a Notice of Intent application with the Conservation Commission. The hearing is currently ongoing. The next scheduled date for hearing discussion is June 24th. To date, concerns with the wetland boundaries represented on the plan have been identified. Additional concerns, pertaining to the stormwater management design, have also be identified through the Commission's peer review process. A copy of the initial stormwater peer review letter will be uploaded to this record for the Council. The applicant's consultants continue to work with the Commission to resolved the identified concerns.



CCSP-21-8

08/18/2021

Storm Water Review

City Council Special Permit

Status: Complete

Assignee: Robert Moore

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611 **Became Active:** 05/18/2021

Completed: 06/11/2021

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

à

Robert Moore, Jun 11, 2021 at 12:45pm

Applicant has filed a Notice of Intent application with the Conservation Commission. The hearing is currently ongoing. The next scheduled date for hearing discussion is June 24th. To date, concerns with the wetland boundaries represented on the plan have been identified. Additional concerns, pertaining to the stormwater management design, have also be identified through the Commission's peer review process. A copy of the initial stormwater peer review letter will be uploaded to this record for the Council. The applicant's consultants continue to work with the Commission to resolved the identified concerns.



CCSP-21-8

08/18/2021

Water Supply Review

City Council Special Permit

Status: Complete

Assignee: Robert Ward

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611 **Became Active:** 05/18/2021

Completed: 06/11/2021

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

John D'Aoust, Jun 1, 2021 at 2:54pm

The Haverhill Water Department (HWD) has reviewed the provided information and finds that the proposed use is not prohibited by Chapter 255 Sec 9.2.6 of the City's zoning code. The proposed project lies in the public water supply watershed for the Millvale Reservoir. As indicated on the submitted plans the proposed work onsite is outside of the delineated water supply protection zone A.

The HWD reviewed the proposed facility storm water management and operations and maintenance plans. It is noted in the operations and maintenance plan that there is a maintenance item related to transformer fluids. It is unclear how the proposed facility will provide protection from an accidental release of hazardous fluids or liquids from transformers, batteries, or other equipment that may be used at the site. The HWD recommends that the applicant describe to what extent there may be hazardous fluids, liquids, or other materials used on the site and what means will be taken to prevent an accidental release.



08/18/2021

CCSP-21-8

Planning Director Approval for Agenda

City Council Special Permit

Status: Pending

Assignee: William Pillsbury

Became Active:

Completed:

Applicant

Robert Harb bobharb@aol.com 17 West Street Haverhill, MA 01830 9783735611

Location

139 AMESBURY LINE RD Haverhill, MA 01830

Owner:

XENAKIS THEODORE 139 AMESBURY LINE RD HAVERHILL, MA 01830

Comments

William Pillsbury, Jun 10, 2021 at 12:32pm

Recommend approval of both special permits as presented





CITY HALL, ROOM 100
FOUR SUMMER STREET
HAVERHILL, MA 01830
PHONE 978-374-2300
FAX 978-373-7544
MAYOR@CITYOFHAVERHILL.COM
WWW.CI.HAVERHILL.MA.US

August 20, 2021

City Council President Melinda E. Barrett & Members of the City Council

Florentini (LTF)

RE: Mayor's Task Force on Public Health

Dear Madame President and Members of the City Council:

Please be advised that I hereby appoint the following to serve on the Mayor's Task Force on Public Health:

- Kevin McCarthy of Groundwork Lawrence
- Tony Slabacheski, Holy Family Hospital, Haverhill Campus, Administrator in Charge.

The Haverhill Task Force on Public Health's first mission will be to work to have the COVID-19 vaccine distributed to as many people as possible in the City of Haverhill. These are non-confirming appointments which will take effect immediately and expires on December 31, 2021.

Very truly yours,

James J. Fiorentim

Mayor

JJF/lyf

City of Haverhill

12.51511

Taxi Driver License - Ch.230 sec.20

pd. 50.00

Honorable President and i	Members of the Havernill	City Councili		
The undersigned respect	Illy asks that he/she may	receive a license to di	we a taxi in the City	of Haverhill
Name: Michael B				
Address: A High	LOT MANAGES	WIT BUILD		
Applicant phone number	603 937-72	35		
Any driver of vehicle(s) mi	st provide name addres	S.DOB, SS# and Drive	Ks lic ense # - fill out	on back.
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DOCUMENT

CITY OF HAVERHILL

In Municipal Council

ORDERED:

To the Honorable Members of the City Council:

By virtue of the authority vested in me, as Mayor, by the City Charter and Ordinances of the City of Haverhill, and the General Laws of the Commonwealth, I have this day appointed the following persons, as attached, to serve as Precinct Officers in the several wards of the City for the year 2021:

John R.	Buzzell
Linda	Hamel
Griselda	Garcia
Barbara	Dube
Guy	Berube
Alice	Tobiassen
Judith	Biewener
Tim	Biewener
Elise	Ashley
June	Brown
Lisa	Davis
Joyce	Thibodeau
Louis	Yarid
Ed	Brewster
Jessica	Brewster
Bryan	Waters
Eric	Guilfoyle
David	Decker
Kira	Yarid
Penelope	Guerrero
Charles	Mueller
Aileen	Swider
Joe	Hakim
Gail	Desmarais
Rosalind	McKeon
Marianne	Mueller
Jennifer	Doucette
Christena	Flynn
Maxine	Rock
Oleg	Rock
Gladys	Welles
Jane	Burgess
Lorraine	Lostimolo



Jane	Jeffers
Eric	Karlstad
Anna	Tschetter
Joann	Corthell
Sue	Brewster
Roxanne	Patroni
Kimberly	Hrubes
Linda	McCarthy
Carolyn	Hannagan
Pat	Ross
Donna	Malone
Anne	Dunn
Ismael	Matias
Mary	Harris
Leslie	Brown
Biagio	Bovenga
Herb	Bergh
Kathy	Bresnahan
Nancy	Perry
Virginia Virginia	Taylor
Maria	Lagual
David	Cue
Madelaine	Thompson-Judkins
Justine	Carrigan
Ajmain	Zahid
Ambriel	Mayhew
Dan	Beauregard
Joseph	Giampa
Margaret M.	Preston
Rene	Jungers
Lawrence	Hicks
Sheryl	Ross
Catherine	Hicks
Kathleen	Connor
Diana	Vencis
Janice -	
Carolyn	Keyser Layzer
Robert	Pombar
Anda	Adams
Sue	
	Hicks
Doug	Edison
Janet R	Senk
Steve	Arthur
Felipe	Hernandez
Cynthia	Floyd
Diane	Gurry
Rita	Gallo
Gary	Bradley

Carol	Read
Joe	Bolis
Roger	Begin
John	Woolf
Grace	Tumushabe
Richard	Klinger
Christine	Kwitchoff
Paula	Wentworth
Alice	Zujowski
Jane	Leach
Regino	DeAza
Dianne	Tarpy
Margaret	Pfifferling
Pam	Pfifferling
John	Brayton
Judith	Jewett
Pamela	Ross
Ernest	Anderson
Carol	DeOliveira
Frances	Poirier
Christina	Fabiano
Susan	Coppola
Carol	Carifio
Joe	LoGiudice
– Patricia	Hobitz
Maurice "Mo"	McGuire
Eric	Wortman
Patrick	Murphy
Irl	Clevesy
Gina	Marks
Lillian	Boutin
Shawna	Kelley
Lynda	Brown
Kevin	Bergin
Robert	Simard
Janice	Taylor
Katherine	Mulcahy .
Robert	Sahakian
Deryl	Santosuosso
Phil	Brown
Heidi	Blanchet
Manuel	Martines
Kevin	Parah
Jessica	Collins
Paula	Brooks
Robyanne	Cormier
Cheryl	Lupi
Frances	De Leon

Maryann	Mueller
Sandra	Finnigan
Bethel	Keller
Ed	Buckley
Kimberly	Cooper
John	Hassan
Leslie	Hassan
Denette	Abers
Tina	Morse
Walter	Gotham
Jessica	Shea
Jane	McNeal
Kathy	Welch
Susan	Gregory
Alvin	Hitchcock
Ann	Somma
Kara	Ferguson
Katelyn	Weber
Josh	Reynolds
David	McKenzie
Kathy	Renzi
Jessica	Shea

Mayor James J Fiorentini

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CITY OF HAVERHILL HAVERHILL, MASSACHUSETTS 01830-5843



CITY HALL, ROOM 204 4 SUMMER STREET TELEPHONE: 978 374-2328 FACSIMILE: 978 374-2329 www.cityofhaverhill.com

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August 18, 2021

To: President and Members of the City Council:

Councillor Daly O'Brien would like to discuss closing Washington Street and Wingate Street on Friday and Saturday evenings making them pedestrian only.

City Councillor Mary Ellen Daly O'Brien

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August 18, 2021

To: President and Members of the City Council:

Councillor Daly O'Brien would like to discuss a constituent's request to put an end to commercial truck traffic on Mill Street and the issue of truck traffic through residential neighborhoods throughout the city.

Mary Eller Daly D'Bren/lat City Councillor Mary Ellen Daly O'Brien

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August 19, 2021

TO: President and Members of the City Council:

Councillor Bevilacqua wishes to discuss the opportunity for additional senior citizen housing.

City Councillor Joseph Bevilacqua

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August 19, 2021

TO: President and Members of the City Council:

Councillor Bevilacqua wishes to recognize the upcoming 20th Anniversary Commemoration of the September 11, 2001 terrorist attacks that killed nearly 3,000 innocent people and injured thousands at The World Trade Center, The Pentagon, and a field in Somerset County, Pennsylvania.

Cut Councillor Joseph Bevilacqua

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August 19, 2021

TO: President and Members of the City Council:

Councillor Daly O'Brien and Councillor Bevilacqua requesting to discuss the continuing neighborhood concerns with NETTS tractor trailer traffic on Monument Street.

Mary Ellen Daly O'Brien/lav-City Councillor Mary Ellen Daly O'Brien

City Councillor Joseph Bevilacqua

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DOCUMENTS REFERRED TO COMMITTEE STUDY

38-W	Communication from Councillor Barrett requesting to give an update on response from Citizen MBTA/Keolis & US EPA about idling trains in Bradford	is Outreach	4/5/16 1/31/17
10-B	Communication from President Michitson asking to request from Mayor status of facility Citizen improvements to public buildings and parks to comply with American w/ Disabilities Act (ADA)		1/3/17
10- U	Communication from President Michitson requesting discussion on next steps to provide comprehong range plan for Haverhill Citizens	nensive S Outreach	8/15/17 1/31/17
38-D	Communication from Councillors Sullivan and Barrett requesting an update on City's emergency management plan and status of working generators in all public building in City Public Pub	8/15/17 lic Safety	, 4/23/18 3/20/18
79-F	Communication from Councillor Sullivan requesting to introduce Kathleen Fitts, Gale Park Assoc to request the city replace the Gale Park Fountain in fiscal year 20	. NRPP	1/23/19 6/25/19
79-T	Communication from Councillors Sullivan and Barrett re: discussion with VINFEN & Haverhill Police Dept. regarding incident in neighborhood of 20 Westland Ter. group home on 7/5 and steps being taken to better supervise residents and reduce police calls to residence	Public Safety	7/23/19
89-K	Communication from Councillor Macek requesting open discussion relative to the process for Establishing a Charter Commission to review the current City of Haverhill Charter	Citizens Outr	each 8/6/19
89-U	Communication from Councillor LePage re: applying for Community Compact Best Practices Program grant for benefit of city and its residents	Citizens Outro	each 9/17/19
89-V	Communication from Councillor McGonagle requesting a discussion about school bus safety	Public Safety	9/17/19
11	Communication from Councilor Jordan requesting to introduce Steve Costa of Citizens for Haverhill Fire to discuss Mayor's CIP and occupational cancer	Public Safety	1/7/20
34-P	Communication from Councillor Sullivan requesting a discussion regarding the disposal of cremated remains on public property	NRPP	3/17/20
58-M	Communication from Councillors LePage and Daly O'Brien re: the possible use of Hale Hospital Trust Funds for ongoing City health care programs and issues	A & F	4/21/20
69 - O	Communication from President Barrett and Councillor Sullivan requesting discussion on illegal fireworks in the City	Public Safety	7/28/20
86-D	Communication from Councillor Michitson requesting to address economic development ideas resulting from the pandemic	ning & Dev.	8/11/20
86-F	Communication from Council President Barrett and Councillor LePage requesting discussion pertaining to utilization of UV-C disinfection fixtures in public buildings	A & F	8/25/20
89-C	Mayor Fiorentini submits final recommendations of Matrix Company	NRPP	9/15/20

DOCUMENTS REFERRED TO COMMITTEE STUDY

91	Petition from Wady & Jewnifer Grullon requesting to purchase city property that abuts their property at 14 Silver Birch Ln; Assessor's Map 574, Block 1 Lot 7	NRPP	9/15/20
91-B	Petition from the Biggart Family requesting to purchase 2 parcels of land that abuts their proper at 30 Belvidere Rd., Assessor's Map 409, Block 114, Lot 9; and Map 409, Block 1A, Lot 1 that conservation land, but only the portion zone RMD (Residential Medium Density)	ty " includes	9/22/20
86-S	Communication from Councillors LePage, Sullivan and Macek to discuss process for approval of development projects within the Waterfront District Ch. 255, Article XVI	A & F	10/6/20
55-I	Communication from Council President Barrett and Councillor McGonagle requesting to introd Don Jarvis, Keith Gopsill and Mike Ingham to discuss becoming a Purple Heart Community	uce NRPP	12/15/20
91-C	Petition of Michael DeLuca requesting to purchase surplus city land on River St., Map 538, Block 419B, Lots 20, 21, 22, 23	NRPP	12/15/20
4 - I	Communication from Councillor Michitson requesting to address the rising inequities between high and low paid occupations in the United States	Citizens Outreach	1/12/21
4-Q	Communication from Councillor Macek requesting discussion on parking space requirements per zoning regulations throughout City	A & F	2/2/21
27-E	Communication from Councillor Sullivan requesting to introduce Debbie Lyons, to explain having legal permitting system as it relates to establishing permitting/licensing process to allow for "Bow Hunter Tree Stands" to be placed on trees on City properties when hunting is allowed	NRPP in season	3/2/21
27-Ј	Communication from Councillor Michitson requesting to re-start discussion on way ahead for residential zoning in Haverhill	Planning & Dev	. 3/9/21
50	Councillor Jordan requests on behalf of Tom Riley, 195 Kingsbury Ave., to have city surplus land that abuts his property, Map 768, Block 50, Lot 85A on Lincolnshire Ave.	NRPP	4/6/21
27-X	Councillor Daly O'Brien requests discussion re: cars parking on Concord St. sidewalks and possibility of city providing off-street parking	NRPP	4/6/21
50-U	President Barrett and Vice President LePage request discussion about composting options	Citizens	5/18/21
50-W	Councillor McGonagle requests to discuss an option to reward first responders and frontline workers to receive bonus for working through pandemic	Outreach Public Safety	5/18/21

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LONG TERM MATTERS STUDY LIST

- Communication from Councillors Barrett and LePage requesting to discuss double poles in the City A & F 3/15/16, 9/6/16, 11/3/16, 1/17/17, 5/11/17, 10/24/17, 3/6/19

 City of Haverhill Mayor's Recommendations, Capital Improvement Program 2016-2020 A & F 5/31/16, 11/3/16, 5/11/2017, 7/25/17, 2/15/18, 3/6/19, 4/17/19

 Gommunication from President Michitson requesting to introduce Dave Labrode to discuss street free plautings NRPP 8/7/18, 2/28/19, 2/27/20

 Communication from Councillor Macek requesting a discussion about reserve parking spaces at City Hall designated for Registry of Motor Vehicles NRPP 3/19/19, 2/27/20
- Communication from Councillor LePage to discuss accounting of revenue funds received from Licensed Marijuana establishments & their allocation to mitigate costs and impacts to city

 A & F 3/12/19, 8/5/19
- 89-D Communication from Councillors LePage, Michitson, Jordan requesting discussion on reducing exposure of persons under 21 yrs. of age to outdoor advertising (billboards) of marijuana productsand zoning regulations pertaining to smoke and/or vapor stores in Haverhill A & F 7/23,19, 8/16/19